INSTRUCTION MANUAL





THE NATIONAL SUPPLY COMPANY

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GENERAL ENGINE DATA

The Atlas Imperial Diesel Engine described herein is of the heavy duty, solid injection, full Diesel type, designed especially for the reliability and a long life of trouble-free operation. It operates on the four stroke cycle, the sequence of operation being as follows:

- lst Stroke On the downward or suction stroke of the piston, the inlet valve is open and pure air is drawn into the cylinder through the air inlet manifold.
- 2nd Stroke
 On the second or compression stroke, this air is compressed to about 400 lbs. per square inch, the heat of compression raising the air temperature to a point above the ignition temperature of the fuel. Just before the piston reaches top center fuel injection starts and is completed shortly after the piston has passed the top dead center.
- On the power stroke the injected fuel oil burns, increasing the pressure within the cylinder, which drives the piston down through its working stroke. Shortly before bottom center position is reached, the exhaust valve opens.
- As the piston returns toward the head, the burned gases are forced out through the exhaust valve port, and as the piston reaches top center the exhaust valve is closed, the inlet valve is opened, and the cycle is repeated.

The horsepower rating and the rated speed of the engines are stamped on the engine nameplate and these ratings should never be exceeded.

On the nameplate will also be found the engine serial number which should always be stated when ordering parts and in any correspondence with the factory or Sales agencies. The firing order, valve timing and the model designation will also be found on the engine nameplate. When corresponding or ordering parts it is desirable that the model number be stated also. The engine serial number is, however, more important and if the model number is not known the number of cylinders and the bore and stroke of the engine may be stated.

The number of orifices, the orifice diameter and the angle of the orifices in the spray valve tip are also stamped on the engine name-plate. The number of holes or orifices is stamped first, followed by the diameter of the holes in thousandths and in turn followed by the hole angle in degrees. For example, 5-10-20 indicates a spray valve tip which has five holes or orifices of .010" diameter. The axis of the holes or orifices are inclined 20 with the horizontal. If ordering spray valve tips the stamping on the nameplate should be stated.

Section A-1

The following data applies to the following six cylinder engines:

6HM2124 -- 6HM2124SC -- 6HMT2124 -- 6HMT2124SC Models 6HS2124 -- 6HST2124

BORE - - - - - 13"

STROKE - - - - - 16"

HORSEPOWER and OPERATING SPEED -- See engine name plate.

Firing Order -- The firing order may vary due to rotation or hand of engine and therefore this data should be taken from the engine name plate. No. 1 Cylinder is at forward or Governor end of engine.

WEIGHTS:

Cylinder Head Assem - - - - - - - 640 lbs. (Approx.)
Piston & Connecting Rod - - - - - 450 lbs. (Approx.)

PRESSURES:

Lubricating Oil Pressure- - - - - - 25 to 40 lbs./Sq.In. Cooling Water (at Pump discharge) - - - 20 lbs./Sq.In. MAX.

Note -- Applies to marine engines and only on stationary engines equipped with an Atlas inbuilt pump.

Fuel Oil (at Transfer Pump discharge) - - 10 lbs./Sq.In. MAX.

Fuel Oil (In Rail)- - - - - - - - - - - 1500 to 4500 lbs./

Sq.In.

Starting Air Pressure - - - - - - 125 to 250 lbs./
Sq.In.

TEMPERATURES:

Cooling Water - Engine Outlet

Direct Cooling (Raw Water) - - - - 125° F. Max.

Indirect Cooling (Closed System) - - 160° F. Max.

Lubricating Oil - Cooler Outlet - - - - 140° F. Max.

Exhaust Temperature (taken at Cylinder Head)

Full load and full speed - 750° F. Max.

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FUEL AND LUBRICATING OILS

1. RECOMMENDED FUEL OIL SPECIFICATION

Viscosity - - - - - - - - - 35 to 70 S.U. Seconds at 100° F. Gravity (A.P.I.) - - - - - - Minimum 24° Conradson Carbon (A.S.T.M.-D189) - Maximum 0.5% Ash - - - - - - - - - - - Maximum 0.05% B.S.&W. - - - - - - - - - - Maximum 0.1% Sulphur (A.S.T.M.-D129) - - - - Maximum 1.0% Ignition Quality - - - - - - 40 to 60 Cetane Number or equivalent in other ignition index.

2. EFFECT OF FUEL PROPERTIES ON PERFORMANCE

As adjusted at the factory the engine will operate satisfactorily on fuels with viscosities per above specification. It is possible to use thinner fuels but the operation is apt to be "snappy" and it may be difficult to maintain even cylinder load balance at varying loads. Fuels with viscosities less than 35 S.U.S. may also require special spray tips with smaller orifice holes than standard or the fuel pressure may have to be reduced. On the other hand fuels with high viscosities may require larger spray orifices than standard, increased fuel pressure and in extreme cases longer period of injection. To insure good operation it is recommended that the viscosity be held to the specification.

The gravity is of secondary importance. A minimum of 24° A.P.I. is merely given since heavier fuels generally require special treatment, such as heating and centrifuging, before they can be burned successfully.

The "Conradson Carbon" or "Carbon Residue" in the oil is an index to the amount of carbon which will form in the combustion chamber. Fuels with high "Conradson Carbon" may cause carbon to build up on the spray valve tips to such an extent that the fuel sprays are deflected causing poor operation and smoky exhaust. The higher the Conradson Carbon the more frequently will it be necessary to clean the spray, valve tips. Experience also indicates that maintenance costs will be higher when fuels with high "Carbon Residues" are used.

The Ash content of a fuel is a measure of the amount of mineral material it contains. After burning the mineral residues are abrasive and it is consequently important that the Ash content be limited to 0.05%. If the content is higher rapid wear of cylinder liners, pistons and rings will result.

The item <u>B.S.&W.</u> (Bottom Sediment and Water) is an index to the fuel's cleanliness. It is good economy to use clean fuel and store it in clean tanks. Cleanliness in handling the fuel is also important (See paragraph entitled "Importance of Cleanliness in Fuel Handling" in Section N).

When the fuel oil is consumed in the engine <u>Sulphur</u> burns to Sulphur-dioxide. Under normal operating conditions most of this gas is ejected with the exhaust gases. If, however, temperature conditions are low enough, that is, if the engine is idling at low speed and under cold conditions, the sulphur-dioxide gas combines with condensed water vapors to form a corrosive acid which will attack metals used in the engine and exhaust system. It is consequently particularly important to hold the sulphur content low in fuels used for engines subject to variable loads with long periods of idling and also for engines subject to frequent starting and stopping.

The <u>Cetane</u> number of a fuel is an index of the ignition quality. Low Cetane values produce excessive knocking. Excessively high Cetane fuels cause high exhaust temperatures and smokiness of the exhaust.

Although the <u>Flash Point</u> does not affect the suitability of a diesel fuel it is well to specify a <u>minimum of 150° F</u>, since state laws and Classification Societies generally require this minimum. The <u>Pour Point</u> of the fuel should be at least 15° F, below the lowest temperature to which the fuel storage tank is subjected.

3. LUBRICATING OIL

We recommend that a good grade of Marine type pure mineral oil be used in these engines. The oil should be stable under the temperature conditions encountered in the engine and should be resistant to oxidation and sludging. In general, regarding quality of lubricating oil we refer you to a Lubrication Instruction Book which will be sent to any customer or operator requesting it. This book contains some good pointers on the selection and care of lubricating oils.

It is not necessary to use compounded oils, i.e., oils containing additives, inhibitors, anti-oxidants, carbon removers, etc. in Atlas Engines. There are, however, many good compounded oils on the market and these may be used providing extreme caution is exercised and the action of the oil in the engine is observed closely.

When a pure or "straight" mineral oil is used some carbon or other deposits will generally be found in the crankcase and sump tank. The amount of these deposits depend greatly on the quality of the oil which has been used and for good grades of oil the deposits are not excessive and in any way harmful to the engine. The chemicals contained in the compounded oils enable these oils to carry the carbon and other constituents of the usual crankcase deposits in suspension. The compounded oils also have a strong tendency to break loose and carry away any existing crankcase deposits and since there is a limit to the amount that can be carried in suspension clogging of filters and oil lines may result. It is consequently of utmost importance to thoroughly clean out the crankcase, oil lines and sump tank before changing from a straight mineral oil to a compounded oil. As an added precaution we suggest that the first batch of compounded oil be used only for about 25 hours and then drained off. These precautions apply also when changing from one compounded oil to another compounded oil of different make or brand.

If a compounded oil is used the <u>non-corrosiveness</u> of this oil must be looked into very carefully. In this connection the Engineering Dept. of the Atlas Imperial Diesel Engine Co. is available for consultation and they will be glad to advise whether or not an oil is suitable for use in this engine.

With regard to viscosity grade our recommendations are that the viscosity at 130° F. be between 235 and 270 Secs. Saybolt Universal. This corresponds to an S.A.E. viscosity rating of 30 to 40. In other words, the oil to be used should be a heavy S.A.E. 30 or a light S.A.E. 40 oil.

In regard to drainage periods we suggest that the first batch of oil be drained after 100 hours of service. Thereafter the suggested drainage period is 200 to 250 hours. This period may be lengthened somewhat on engines which are equipped with waste packed filters. In that case if the filter cartridge is changed before the oil is badly discolored and loaded up with insolubles or foreign particles, drainage periods of 400 to 600 hours can be used. In the cases where no waste packed filters are used the oil will of course not be "worn out" after 200 hours of service if it is of a good grade. It will, however, be dirty and will contain insolubles which should be removed from the lubricating oil before it is re-used.

The same lubricating oil as used in the crankcase of the engine is also suitable for use in the <u>mechanical lubricator</u>. In the case of the mechanical lubricator, however, it is highly desirable that new oil be used.

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INSTALLATION INSTRUCTIONS

1. PREPARING THE ENGINE BED

The success of a Marine engine installation depends greatly upon the construction of the foundation and upon the care exercised in lining up the engine to the propeller shafting. Poor installations will result in excessive vibration and continual change in engine alignment. The result is poor performance and failure of vital parts. For this reason Atlas Imperial Diesel Engine Co. cannot guarantee an engine unless the engine foundation (engine bed) is strong and rigid enough to prevent vibration and changes in alignment.

The importance of rigidity in the engine foundation cannot be over-emphasized and it must be securely fastened to the hull of the vessel so as to be virtually a part of the hull construction. For installations in old hulls, where the rigidity of the hull is questionable, the foundation should be extended fore and aft as far as possible; twice the length of the engine is suggested. Stiffeners should be fitted to prevent the foundation from twisting and weaving. In twin screw installations it is advisable that both foundations be stiffly connected and braced to each other and to the hull. Steel foundations should be welded or riveted. Avoid bolts or screws which may work loose.

When preparing the engine foundation always obtain certified outline prints. Do not use figures or cuts in bulletins or sales literature. The top faces of the foundation must be straight and should be lined up so that they are parallel to the propeller shafting. Athwartships the two top faces should be level. The foundation should be constructed so as to allow 1" to $1\frac{1}{2}$ " thick shims or chocks between the engine supporting flanges and the top faces.

2. INSTALLING THE ENGINE

The engine should be lowered onto the foundation and allowed to rest on the leveling screws. For wooden foundations provide steel plates of sufficient area and thickness for the leveling screws to rest on. (Min. 4" x 4" x $\frac{1}{2}$ " to 3/4" thick.) Shift the engine sideways until the centerline of the crankshaft lines up with the centerline of the propeller shafting. Then by means of the leveling screws adjust the height until the centerline of the crankshaft exactly lines up with the centerline of the propeller shafting. Also level the base athwartships. When alignment in all planes is at hand the following check should be made.

- a. Turning over shaft there should be no binding between the centering spigot and recess of the two coupling halves.
- b. The faces of the coupling halves should be parallel regardless of the angle through which either or both shafts are turned. With the propeller coupling half held against the engine coupling half, but not bolted, it should not be possible to insert a 0.003 in. feeler at any point between them. Check at top and bottom and the two sides before bolting flanges together.

If engine has been installed before launching it is advisable to temporarily bolt it to the foundation at this time. It is not advisable to proceed any further before launching unless the hull is extremely rigid. When the vessel is afloat the alignment should again be checked and if found satisfactory a chock should be carefully fitted at each holding down bolt. This applies to steel foundations. In wooden foundations careful measurements should be taken of the distance between the bottom of the engine supporting flanges and the top of the foundation. A continuous wooden shim should then be prepared and this shim should exactly fit the space between the foundation and the engine supporting flanges. The shims should be at least as wide as the supporting flanges.

After the engine is resting on the chocks or wooden shims it is advisable to check that the foundation is supporting the engine evenly over the entire length. This is best done with a #696 Starrett Strain Gage. Check the distance between the inside faces of the crankwebs with the corresponding crank on upper and lower centers. (See figure in Section F for strain gage location.) Readings for any one crank should not differ more than .003". Distortion of the last two cranks only indicates that the crankshaft is out of line with the propeller shafting. (When making this check the engine and propeller shaft couplings should be bolted together.) Check the last two cranks in the two horizontal positions also. If misalignment or uneven support is indicated determine the cause and correct.

When the final alignment has been accomplished permanent foundation bolts should be fitted. For steel foundations drill and ream for fitted bolts. Spaces between the foundation bolt chocks can then be filled with type metal.

3. SERVICE PIPING

Plan all piping carefully and use as short and direct lines as possible. To improve the general appearance of the installation, piping should be laid below the engine room floor when it is possible to do so. Removable floor plates should be provided and care should be taken that all piping is accessible.

4. FUEL AND LUBRICATING OIL PIPING

See Section N for pipe sizes and arrangement of the fuel day tank. See Section T for lubricating oil day tank connections. Pipe sizes are stated in these Sections. Provide drain valves and vent valves where necessary and remove all scale and dirt from pipes and fittings before installing.

5. COOLING WATER PIPING

Locate the sea chest far enough below the water line to prevent uncovering when the vessel rolls. It should be provided with a coarse grating. Inside the hull a strainer of ample size should be provided with gate valves on each side so that it can be isolated for cleaning. For engines equipped with centrifugal circulating water pumps it is particularly important that the resistance in the sea chest, strainer and piping be as small as possible. Use as few bends as possible and do not make either suction or discharge piping longer than necessary. Locate the overboard discharge not more than 3' above the water line. All valves should be gate valves - not globe valves. Use pipe sizes called for on the outline drawing.

6. STARTING AIR PIPING

Air tanks should conform to A.S.M.E. specifications and should have ample strength for 250 lbs. per square inch pressure. Each tank should be equipped with a safety valve and a globe valve for isolation. A drain valve should also be provided at the lowest point and this valve should be accessible.

Tanks should be connected to the engine starting air header using the pipe size called for on the outline drawing. Provide a globe valve next to the engine. All valves and fittings should be of heavy pattern for at least 250 lbs. per sq. inch pressure. The air compressor on the engine should be connected to the tanks with pipe of the size called for on the outline drawing and valves and fittings of heavy pattern. The air compressor discharge pipe should preferably be run to the air tank. It should not be connected to the piping between the tank and the starting air header. Air compressor unloader should preferably be connected to the tank with its own piping or tubing. Under no circumstances should it be connected to the compressor discharge line.

7. EXHAUST SYSTEM

All exhaust piping should be installed in the shortest and most direct manner possible. When bends are necessary use long sweep fittings. Use the pipe size called for on the outline drawing for lengths up to 20' containing a maximum of three bends. For 3 to 6 bends increase the pipe to the next nominal size and for each additional 30' length increase by one pipe size.

In order to protect the engine and piping from undue strains a length of flexible metal tubing should be installed as near to the engine as possible. It is also recommended that flanged connections be used for ease of dismantling and cleaning. For twin screw installations it is recommended that separate exhaust lines be used. If exhaust lines are combined and only one engine is running, soot and carbon will be blown into the other engine through the open exhaust valve.

OPERATING INSTRUCTIONS

Before the operator attempts to run the engine, he should carefully study the chapters dealing with the mechanical details, especially those of the Control System. After familiarizing himself with the principles of the control mechanism, the operator will understand the significance of each movement of the control wheel and will be able to handle the engine intelligently. In the following only a brief description of the proper method of operating the engine and controls is given.

Observe the construction of the handwheel (1) and its locking device. Note how plunger (9) enters locking disc (8). Observe the positions of pointer (7) when the plunger enters the locking disc. These positions, "AHEAD" and "ASTERN", are the normal running positions.

TO GO AHEAD FROM STOP (see Fig. D-1)

- (a) In STOP position pointer (7) is vertical and indicates STOP position on telltale (10). Turn engine handwheel (1) in the AHEAD direction, so that pointer (7) moves in AHEAD direction, toward START position. At approximately 1-3/4 turns of the handwheel, the plunger (9) will enter locking disc hole. From this position the turning of the handwheel toward START should proceed more slowly for about 1/4 turn until motion is stopped by latch shaft "stop". (If handwheel is turned too quickly, control system may be damaged.) At this position the engine will begin to turn over on starting air.
- (b) As soon as the engine has reached maximum cranking speed, turn the handwheel back about 1/4 turn until the plunger enters the locking disc. This will be the "AHEAD" running position.

TO REVERSE THE ENGINE (see Fig. D-1)

(a) Turn handwheel in the ASTERN direction, causing pointer to move in the ASTERN direction. Continue to STOP position and after engine has stopped continue turning in the ASTERN direction until plunger enters locking disc. This will be about 3-1/2 turns from the AHEAD running position. From this position the same caution as above should be observed when approaching START position. In the START position the engine will begin to turn over on starting air.

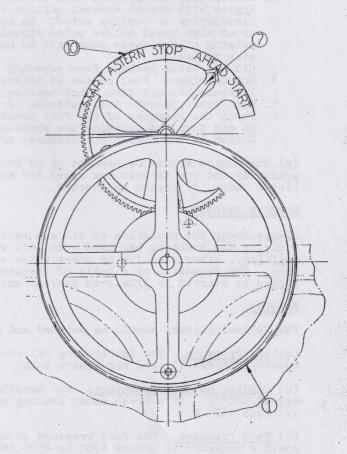


FIG. D-1

(b) As soon as the engine has reached maximum cranking speed turn the handwheel back about 1/4 turn until the plunger enters the locking disc. This will be the ASTERN running position.

INITIAL STARTING AND STARTING AFTER PROLONGED SHUTDOWN

- (a) A final check should be given all fuel, air, lubricating oil and water lines, giving attention to the location and position of shut-off valves, check valves, etc. It is well to trace each system through making sure that there are no short circuits or blockages.
- (b) For the initial starting it is well, although not absolutely necessary, to fill the pressure lines and passages of the lubricating oil system. For this purpose a small hand operated gear pump or piston pump can be used. When the pressure lines are full, a slight pressure will register on the pressure gauge. This procedure will insure lubricating oil pressure immediately upon starting.
- (c) Hand oil the engine at all the points listed under "4-HOUR ROUTINE" in the

"Maintenance & Inspection" section. Fill the mechanical lubricator and turn its crank several revolutions.

- (d) Open the two small vents on top of the outlet fittings of the high pressure fuel pump and operate the hand priming pump until fuel flows from both of these points. Then close these vents and pump up approximately 1000 lbs. fuel pressure.
- (e) See that valves in starting air piping between air receiver and engine are open and that there is sufficient air pressure available. With the spray valve isolating valves shut and with the "snifters" open crank the engine by air until any excess fuel in the combustion chambers has been blown out.
- (f) Start the engine by the method described on the preceding page and run it at a slow speed by setting the governor speed control handle. Then <u>immediately</u> check and watch the following.
 - 1. Lubricating oil pressure and circulation. Observe oil level in day tank. Engine will absorb several gallons when started up.
 - 2. Circulation of cooling water. Do not run the engine longer than 2 minutes or at high speed unless water circulation has started. In some instances priming of the water pump will be necessary but do not prime until the engine is cool.
 - 3. Oil and water leakage from external lines and fittings.
 - 4. Hot bearings. Feel covers at intervals to locate any hot areas which would indicate hot oil from a hot bearing.
 - 5. Feel water jackets and manifolds for even water circulation.
 - 6. Check the response of the fuel pressure relief valve by moving the handle up and down and watching the pressure gauge.
 - 7. Listen to the engine for evenness of firing and mechanical knocks.
- (g) The engine should be brought up to full speed and load slowly. Increase speed gradually and run at each new speed for at least one minute. At each speed the items listed under (f) should be checked.

ROUTINE STARTING

Always check the positions of oil and water shut-off valves and make certain that no tools or the cranking bar have been left where they can interfere with flywheel or shafting. After starting up check water circulation, lubricating oil level and pressure. The formation of a habit of checking these items automatically whenever the engine is started is likely to prevent accidents and serious damage.

RUNNING

The following items should be watched and regulated if necessary:

- (a) <u>Oil Pressure</u>. The lubricating oil pressure should be maintained between 30 lbs. per square inch and 40 lbs. per square inch.
- (b) <u>Cooling Water Temperature</u>. For Seawater Cooling the outlet temperature should not exceed 125° F. If a Fresh Water Cooling system is used the outlet temperature may safely reach 160° F.
- (c) <u>Fuel Pressure</u>. The fuel pressure should be varied with the engine speed. At full speed a pressure of around 4000 to 4500 lbs. per square inch will give the best results. However, as the speed is reduced the fuel pressure should also be lowered to prevent too great a withdrawal of the wedges. Too high a fuel pressure at low speeds causes very short injection periods resulting in roughness and uneven engine operation.
- (d) <u>Lubricating Oil Temperature:</u> At the outlet of the oil cooler should not exceed 140° F.
- (e) Mechanical Lubricator. The feed from the mechanical lubricator should be adjusted to 15 to 20 drops per minute per feed.
- (f) Exhaust Temperature. The normal full load and speed exhaust temperatures range from 700 to 750 degrees. If the temperatures for all cylinders are above these limits the propeller is overloading the engine and should be changed. If the exhaust temperature for any one cylinder is too high or too low the injection system is probably at fault. (See section on "Smoky Exhaust" under "Maintenance & Inspection".)
- (g) Exhaust Appearance. Observe the exhaust appearance. If it is smoky investigate the cause. In most cases the spray valves are responsible for smoke. (See section on "Smoky Exhaust" under "Maintenance & Inspection".)

OPERATING INSTRUCTIONS

Before the operator attempts to run the engine, he should carefully study the chapters dealing with the mechanical details, especially those of the Control System. After familiarizing himself with the principles of the control mechanism, the operator will understand the significance of each movement of the control lever and will be able to handle the engine intelligently. In the following only a brief description of the proper method of operating the engine and controls is given.

Observe the construction of the control lever noting the manner in which the latch engages the holes and slots in the latch plate. Depressing the latch button in the end of the handle disengages the latch so that the control handle may be moved. Depressing the button and twisting it holds the latch in the disengaged position. This locking out device is to be used only on that control lever, (engine or pilot house control stand), which is not used for maneuvering the engine. The latch on the control lever by which the engine is being operated should always be free and under control of the operator.

TO GO AHEAD FROM STOP (See Fig. D-1)

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- (a) Depress the latch button just long enough to release the control lever and move the lever "AHEAD". The latch will slip into the slot between points "A" & "B". As soon as the latch has entered this slot back the lever up until it is stopped at point "A" by the latch and hold it in this position until the reversing cylinder has shifted. (If the cylinder has not shifted the handle will be stopped at a point between "A" & "B".)
- (b) Without depressing the button move the lever ahead until it is automatically stopped in position "B" by the latch. The engine will begin to turn over on starting air.
- (c) As soon as the engine has reached maximum cranking speed, depress the button and quickly move the lever to "SLOW", position "C". The engine will start and run at its slowest speed ahead.
- (d) Depress the handle button and advance the lever until the desired engine speed is obtained. Then release the button so that the latch will engage one of the eight holes between "SLOW" (position "C") and "FAST" (position "D").

TO REVERSE THE ENGINE (See Fig. D-1)

- (a) Depress the latch button and return the lever to "STOP". Hold the lever in this position until the engine has stopped.
- (b) Depress the button and move the lever to "E" in the "ASTERN" direction. At the same time observe the indicator on the air ram.
- (c) As soon as the air ram has moved to its "ASTERN" position move the lever until it is stopped by the latch at "F". The engine will begin to turn over in the astern direction.
- (d) When the cranking speed is sufficient, depress the button and quickly move the lever to "SLOW" (position "G"). The engine will start and run at its slowest speed astern.

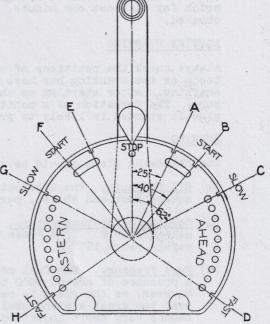


FIG. D-1

(e) Depress the handle button and move the lever toward "FAST" astern (Position "H") until the desired speed is attained and then release the button.

INITIAL STARTING AND STARTING AFTER PROLONGED SHUTDOWN

- (a) A final check should be given all fuel, air, lubricating oil and water lines, giving attention to the location and position of shut-off valves, check valves, etc. It is well to trace each system through making sure that there are no short circuits or blockages.
- (b) For the initial starting it is well, although not absolutely necessary, to fill the pressure lines and passages of the lubricating oil system. For this purpose a small hand operated gear pump or piston pump can be used. When the pressure lines are full, a slight pressure will register on the pressure gauge. This procedure will insure lubricating oil pressure immediately upon starting.
- (c) Hand oil the engine at all the points listed under "4-HOUR ROUTINE" in the

"Maintenance & Inspection" Section. Fill the mechanical lubricator and turn its crank several revolutions.

- (d) Open the two small vents on top of the outlet fittings of the high pressure fuel pump and operate the hand priming pump until fuel flows from both of these points. Then close these vents and pump up approximately 1000 lbs. fuel pressure.
- (e) See that valves in starting air piping between air receiver and engine are open and that there is sufficient air pressure available. With the spray valve isolating valves shut and with the "snifters" open crank the engine by air until any excess fuel in the combustion chambers has been blown out.
- (f) Start the engine by the method described in the preceding sections and run it at "SLOW" ahead (position "C" on Fig. 3). Then immediately check and watch the following:
 - 1. Lubricating oil pressure and circulation. Observe oil level in day tank. Engine will absorb several gallons when started up.
 - 2. Circulation of cooling water. Do not run the engine longer than 2 minutes or at high speed unless water circulation has started. In some instances priming of the water pump will be necessary but do not prime until the engine is cool.
 3. Oil and water leakage from external lines and fittings.

 - 4. Hot bearings. Feel covers at intervals to locate any hot areas which would indicate hot oil from a hot bearing.
 - 5. Feel water jackets and manifolds for even water circulation.
 - 6. Check the response of the fuel pressure relief valve by moving the handle up and down and watching the pressure gauge.
 - 7. Listen to the engine for evenness of firing and mechanical knocks.
- (g) The engine should be brought up to full speed and load slowly. Run at each control notch for at least one minute. At each speed the items listed under (f) should be checked.

ROUTINE STARTING

Always check the positions of oil and water shut-off valves and make certain that no tools or the cranking bar have been left where they can interfere with flywheel or shafting. After starting up check water circulation, lubricating oil level and pressure. The formation of a habit of checking these items automatically whenever the engine is started is likely to prevent accidents and serious damage.

RUNNING

The following items should be watched and regulated if necessary:

- (a) Oil Pressure. The lubricating oil pressure should be maintained between 30 lbs. per square inch and 40 lbs. per square inch.
- (b) <u>Cooling Water Temperature</u>. For Seawater cooling the outlet temperature should not exceed 125° F. If a Fresh Water cooling system is used the outlet temperature may safely reach 160° F.
- (c) <u>Fuel Pressure</u>. The fuel pressure should be varied with the engine speed. At "FAST" a pressure of around 4000 to 4500 lbs. per square inch will give the best results. However, as the speed is reduced the fuel pressure should also be lowered to prevent too great a withdrawal of the wedges. Too high a fuel pressure at low speeds causes very short injection periods resulting in roughness and uneven engine operation.
- (d) Lubricating Oil Temperature at the outlet of the oil cooler should not exceed 140° F.
- (e) Mechanical Lubricator. The feed from the mechanical lubricator should be adjusted to 15 to 20 drops per minute per feed.
- (f) Exhaust Temperature. The normal full load and speed exhaust temperatures range from 700 to 750 degrees. If the temperatures for all cylinders are above these limits the propeller is overloading the engine and should be changed. If the exhaust temperature for any one cylinder is too high or too low the injection system is probably at fault. (See section on "Smoky Exhaust" under "Maintenance & Inspection".)
- (g) Exhaust Appearance. Observe the exhaust appearance. If it is smoky investigate the cause. In most cases the spray valves are responsible for smoke. (See section on "Smoky Exhaust" under "Maintenance & Inspection".)

SUPPLEMENTARY OPERATING INSTRUCTIONS TURBOCHARGED 13 X 16 ENGINE

The points discussed in these instructions are the differences from the standard engine. The turbocharged engine is the standard engine adapted to turbocharging by the addition of a Buchi Elliott type of turbocharger with whatever changes in details are necessary to accommodate the application of the turbocharger and accomplish the overall result of increasing the horsepower approximately 40 to 45 % over the rating of the standard non-turbocharged engine. Thus the attached text for the standard engine applies except for the special items discussed here.

The Buchi Elliott turbocharger is a gas turbine driven centrifugal type blower mounted at one end of the engine. The exhaust gases from the cylinders pass through the exhaust manifold into the turbocharger for driving the turbine. The exhaust gases pass out from the top of the turbocharger up through the exhaust pipe and muffler as usual. Intake air for the engine passes through the inlet silencer, mounted on the turbocharger, through the centrifugal blower and is delivered to the air inlet manifold. Parts List and Instructions covering the turbocharger will be found at the end of this book under auxiliary equipment. The exhaust manifold consists really of two manifolds inside of a single jacket. Three cylinders discharge into each manifold and are alternate cylinders according to the firing order. This is in order to give proper spacing between exhaust gas impulses. The jacket around the two individual exhaust manifolds provides for water cooling of them.

WORKING PISTON

The working piston for the turbocharged engine has two pockets cut into the top in order to provide mechanical clearance for the inlet and exhaust valves when they are open at the end of the exhaust stroke and at the beginning of the inlet stroke. This is the scavenging period in the Buchi turbocharger cycle and as you will see by reference to the valve timing, there is considerable overlap between the opening of the inlet valves and the closing of the exhaust valves during this period. It is important when installing a piston in the engine to make sure that the pockets in the piston top correspond to the location of the valves in the cylinder head. Otherwise there will be interference between the valves and the piston.

Also note that the distance from the top of the liner to the top of the piston is greater on the turbocharged engine than on the standard engine. The figure for the turbocharged engine is 1-3/32. This greater distance between piston and cylinder heads provides a little larger combustion space for the turbocharged engine. Thus the compression ratio is a little lower on the turbocharged engine than on the standard engine. This is to allow for the effect of the action of the turbocharger which delivers more air to the cylinders than in the standard engine.

VALVE TIMING

The correct valve timing for this engine is given in the following table:

Starting Air Valve Opens	-	5° B.T.C.
Starting Air Valve Closes	-	50° B.B.C.
Inlet Valve Opens	-	80° B.T.C.
Inlet Valve Closes	-	300 A.B.C.
Exhaust Valve Opens		450 B.B.C.
Exhaust Valve Closes	-	65° A.T.C.

The fuel spray valve is designed to open 6° B.T.C. and close 22° A.T.C. but the exact timing for each individual engine is given on the engine name plate and the figures on the name plate should be followed when making any adjustments.

INLET AND EXHAUST MANIFOLDS

The air inlet manifold has a separate sleeve with a floating flange and if it ever becomes necessary to replace the manifold on the engine, the new manifold should first be applied in place with the sleeve loose, and when the right adjustment is found between position of sleeve and manifold when both are bolted in place, tack welding will hold the flange temporarily. Then the manifold can be removed for firmly welding the flange to the manifold sleeve.

Section E-1

Similarly, the exhaust manifold has the end flange loose and will require locating and welding at assembly.

Care should be taken when assemblying the turbocharger on its bracket that sufficient shims are used under the support feet to prevent any possibility of the turbocharger weight hanging on the exhaust and inlet connection capscrews. These capscrews are used purely for making tight gas joints and are not intended in any way to help support the weight of the turbocharger.

FUEL SYSTEM

The main high pressure fuel oil header or rail on this engine is larger than on the standard engine and is of sufficient capacity so that no separate accumulator is used. Also, the individual cylinder isolating valves are of larger size and capacity than on the standard engine.

The high pressure fuel pumps need to be of larger size and capacity than on the standard engine in order to supply the increased amount of fuel required for the larger horse-power developed by the turbocharged engine. Thus the diameter of these plungers is 3/4" on the turbocharged engine against 21/32" on the standard engine.

(2)

The standard spray tips for the turbocharged engine have seven holes 1.013" diameter at an angle of 25° from the horizontal. This tip is subject to variation under certain conditions, and the tip actually used will be noted on the engine name plate.

OPERATION

The operation of the turbocharged engine is no different from the operation of the standard engine. The turbocharger itself is entirely automatic and requires no attention except for maintenance. Instructions in the Buchi Elliott turbocharger pamphlet should be followed.

The speed of the turbocharger varies with the load on the engine, thus the quantity of the air delivered to the cylinders varies with the engine load requirements. You will note that the pressure in the air inlet manifold varies with the load on the engine. It is about three pounds per square inch at full load.

The compression pressure in the cylinders varies according to the load on the engine, because of the action of the turbocharger just described. There is also a slight variation between hot and cold engine conditions. Thus, if you measure compression pressure, make sure that you take these factors into account.

Under normal full load rated power conditions, the exhaust gas temperature in the exhaust manifold to the turbocharger is about 750°. Any temperature above this figure represents an overload on the engine, and it is not good practice to operate the engine at overload ratings except for brief periods. The engine should always be kept in first class mechanical condition and in good operating adjustment.

LOWER BASE, CRANKSHAFT AND BEARINGS

1. BASE AND CRANKSHAFT

The cast iron base carries the main bearing saddles and the main lubricating oil manifold from which oil is piped to each main bearing and to the intermediate gear bearings. The crankshaft turns in babbitt lined steel backed bearing shells, held in place in the base by the main bearing caps. Adjustment is by shims, and running clearances should be .0008" to .00095" per inch of shaft diameter when bearings are fitted.

2. MAIN BEARING ADJUSTMENT

Bearing clearances can be accurately measured with two pieces of lead wire of about .025" diameter and one inch long, which are compressed between shell and journal about 1" from each end of the bearing by tightening the cap bolts. The thickness, measured with a micrometer, is the running clearance. Clearances should be checked annually, and should not be allowed to exceed .0015" per inch of shaft diameter. Keep shims even on both sides.

3. MAIN BEARING SHELLS

The bearing shells are prevented from rotating in the base by the shims, and are located fore and aft by a square head dowel pin in the bottom of the bearing saddles which engages a circumferential groove around the outside of the shell. As fitted the shells project above the base and face of the caps from .002" to .003" on each side, but are squeezed down flush when the capnuts are pulled up. There should not be any appreciable clearance between the base, shim, and cap after final tightening. The bearing shells and caps are all numbered and must always be replaced in the bearing from which they were removed. Never interchange them, either from one bearing to another, or from top to bottom.

4. REMOVAL AND ASSEMBLY OF MAIN BEARINGS

After removing the cotter pins and main bearing nuts, the cap, upper shell and shims may be lifted out. As this operation is performed the positions of the numbers stamped on each of these parts should be noted so that the parts can be reassembled in their proper positions. Unless the bearing is considerably worn it may not be possible to remove the lower shell by hand and it is usually necessary to turn it out of the base by barring the engine over after inserting a capscrew in the oil hole in the journal. The head of the capscrew will contact the edge of the bearing shell and roll the bearing out with the journal.

When assembling the main bearing shells care must be taken to keep all parts absolutely clean. It is of utmost importance that any dirt be prevented from lodging between the shell and the saddle. Extreme care must be exercised in locating the bottom shell in a fore and aft direction before turning it into the base. Misalignment will cause the groove to miss the dowel pin in the base and trouble will then be encountered in backing the shell out again for another try.

5. CRANKSHAFT ALIGNMENT

The crankshaft should be checked at annual overhauls, or at intervals not greater than 7000 service hours, for misalignment due to uneven wear of the bearings. When the engine was erected at the factory the bearings were carefully scraped in, so as to bring the bearing surface of all shells in line. If one of these surfaces, due to uneven wear, becomes lower than the adjacent shells, it is evident that the crankshaft will be bent each time the adjacent cylinders fire and the connecting rods force the journal down against this low bearing. This condition must be guarded against, as neglect or ignorance of it will ultimately result in a broken shaft.

The simplest way to check crankshaft alignment is by means of a bridge gauge, which can be supplied with the engine as extra equipment. If a bridge gauge is desired it must, however, be ordered when the order for the engine is placed. It can not be supplied rater.

With the bridge gauge straddling the journal and resting firmly and squarely on the bearing cap seats in the lower base the distance between the top of the main bearing journal and the machined face on the bridge gauge is measured by means of a feeler gauge. At the time the engine was erected these measurements were taken and were stamped on the bridge gauge. As the age of the engine increases the bearing surfaces will wear, with the result that these measurements will gradually increase. As long as they all increase by the same amount the shaft will still be in line

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however, and there need be no worry, even though they do not agree with the original readings stamped on the bridge gauge. But if at any time the reading for one bearing is found to be more than .004" greater than those for the adjacent bearings, this low shell should be replaced at once and the crankshaft re-aligned, a job that should be undertaken only by an experienced mechanic. A careful record should be kept of all bridge gauge readings taken from time to time.

The bridge gauge measurements described above should be made successively, removing one bearing cap at a time and replacing it before proceeding to the next bearing. When making measurements the crankshaft journal must be forced down against the shell by means of a jack bearing against the centerframe. Protect the shaft journal with a piece of wood or sheet copper. An indication of low bearing shells will usually be given by looseness of the shell in the saddle. If it is possible to freely rotate one of the lower shells by hand when adjacent bearing caps are bolted down, it is quite probable that this shell is unduly worn and it should be checked with the bridge gauge at once.

If a bridge gauge is not available, crankshaft alignment may be checked with a gap or strain gage as follows: Stamp two center punch marks as shown in Fig. F-1 on all cranks. Starting with No. 1 cylinder crank remove adjacent main bearing caps and locate the crank as near lower center as gap gage will permit. Using jack screws between bearing journal and center frame force shaft against lower bearing half (protect shaft with a piece of wood or sheet copper) and record the gap gauge reading. Then loosen jackscrews and bar over until crank is on upper dead center. Again tighten jack screws and record the gauge reading. Repeat on all other cranks.

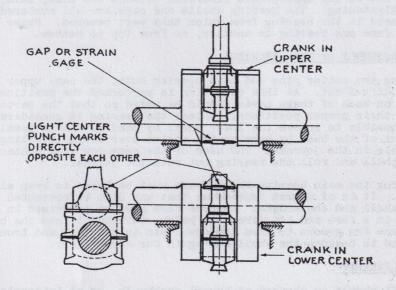


FIG. F-1

Comparison of gauge measurements in upper and lower centers will indicate crankshaft alignment conditions. Normally the measurements for the cranks in top position are slightly larger than measurements for the same cranks in the bottom position. However, the difference in measurement for any one crank should not exceed .0005" per inch of shaft diameter. If this is the case, realignment of the crankshaft bearings is indicated.

1. MULTI-COLLAR TYPE

All loads in a fore and aft direction resulting from propeller thrust are carried by the thrust bearing. This bearing is located aft of the flywheel on pads at the end of the lower base. Water jackets are provided in the bearing castings and a small supply of cold water is bled from the main water inlet manifold to the bearing. A positive supply of cil is fed to the bearing from the mechanical lubricator located at the forward end of the engine.

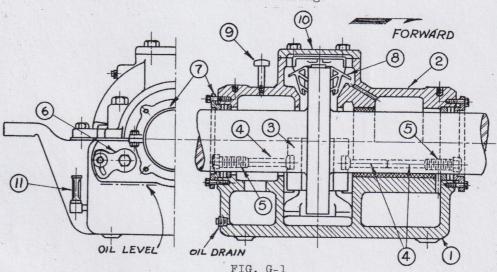
In general the thrust bearing assembly consists of three parts: the bearing, the cap and the thrust shaft. Both the bearing and the cap are water jacketed. Each contains dovetailed circumferential grooves which when lined with babbitt about ¼" thick form grooves for the thrust shaft collars. Between the grooves the cylindrical areas are also lined with babbitt so that sufficient journal area to carry a substantial radial load is incorporated in the bearing.

In the erection of the engine at the factory the thrust bearing is treated as if it were an additional main bearing. After all the lower main bearing shells have been scraped into alignment the thrust shaft is bolted to the crankshaft and tested for trueness. It is required that the total run out of the thrust shaft at the aft end does not exceed .002". In the meantime the thrust bearing (lower half) is installed temporarily on the base. The thrust shaft is then coated with blueing and the whole shaft assembly is lowered into position. The bearing is then shimmed up or down, moved forward or backward, to one side or the other and scraped until the bearing is satisfactorily located. The finished bearing must be in line with the main bearings. The thrust shoulders on the shaft must be a close fit in the grooves but at the same time have clearance. An end play of approximately .005" to .010" is desirable. The location of the bearing should be such that the crankshaft is slightly aft of its central position in the base since the normal wear on the thrust bearing will allow the crankshaft to move forward slightly.

When the foregoing conditions have been met the thrust bearing (lower half) is doweled to the base. The thrust bearing cap is then scraped in and adjusted for clearance with shims.

2. KINGSBURY TYPE

Referring to Fig. G-1 the standard style GH Kingsbury thrust bearing is equipped with two pairs of thrust shoes (3) (two shoes for ahead and two for astern thrust). These shoes are individually adjustable fore and aft by jackscrews (5) which are locked by lock wrench (6). A journal bearing, babbitted directly in lower thrust bearing housing (1) and upper housing (2) is also incorporated. The journal bearing is located on the flywheel end of the thrust bearing.



There is only one thrust collar which is forged integrally with the thrust shaft. Lubrication is self-contained and automatic. The lower housing contains the lubricating oil supply, the oil level being of such height that the lower part of the thrust collar dips into it. The oil is then carried to the top where scraper (8) distributes it over the collar thrust surfaces and takes off some oil for lubrication of the journal bearing. Oil is retained in the bearing by stuffing boxes at

Section G

both ends. Do not take up hard on stuffing box glands (7), as this will cause unnecessary heating of the shaft.

To allow for oil films between thrust bearing surfaces, and for expansion by heat, it is strictly necessary to provide longitudinal end play in accordance with the following table:

Engine Bore 14½ and 15" 13" 11½" 10"

End Play .017" .015" 0 635014" .012"

Using the jackscrews, adjust for end play as follows: Keeping thrust collar in desired fore and aft position, set up firmly on forward-end jackscrews so ahead shoes will bear equally against collar. Lock the screws. Next set up on after-end jackscrews, using a "feeler" gauge, with thickness equal to end play, back of the pivotal support of each shoe. Lock the jackscrews and remove the "feelers".

For average installation of propeller thrust bearings, a heavy turbine or engine oil should be used. The oil should be chosen with due regard to viscosity. If it is too light, the lubricating film may be dangerously thin. If it is too heavy, the friction is needlessly high. Specific advice as to proper viscosity for any definite installation is regularly marked on bearing nameplate. As a rule the viscosity should be about 200 seconds Saybolt at operating temperature of the oil bath. The oil must be clean and free from grit and other injurious substances. Fine grit has a scouring action and may gradually wear down the bearing surfaces. Poor oil may cause corrosion. Oil of good quality does not "wear out" by use in these bearings, but lasts indefinitely if not contaminated.

It is vitally important to maintain the oil at a suitable level. Oil level plates are attached to both sides of housing, with "High" and "Low" oil levels noted. If necessary fill housing with oil to "High" mark when not running. A slight draw down of oil level will be noted when bearing is running. Occasionally oil should be added to make up for leakage and evaporation. Be sure the make up oil is clean. The air vent holes (9) should be kept open. Oil gauge (11) may be placed on either side of housing.

CYLINDER AND LINER, CYLINDER HEAD AND VALVES

1. CYLINDER

The individual cast iron cylinders are secured to the centerframe and base by four studs which are screwed into the base adjacent to the main bearing saddles. The cylinders are located transversely and are aligned to the centerframe by machined pads along one side which register with a step on the top of the centerframe. Crankcase sealer is used between the cylinders and the centerframe. If this joint is disturbed the old sealer must be scraped off and replaced by fresh sealer before tightening the cylinder nuts. Glyptal Lacquer is recommended for sealer. On later engines a gasket is used between the cylinder and centerframe. These gaskets can also be used on engines not originally so equipped.

2. CYLINDER LINER

The cylinder liners are special alloy iron castings, heat treated to relieve stresses and secure correct hardness. They are accurately machined to close tolerances and should be handled carefully and care taken not to damage the fits at top and bottom. Spare liners should always be stored in a vertical position and should be securely fastened down if stored on board ship. The water seal at the bottom of the liner consists of two rubber grommets which should always be replaced with new ones whenever a liner is pulled. When lowering a liner into place, grease the grommets into the cylinder fit or they may be pinched and damaged. The liner has from .004" to .007" clearance in the cylinder at both top and bottom fits and no difficulty should be encountered in installing a new liner. A paper gasket .010" thick is used for the upper water seal between the liner and cylinder and a new gasket should always be used when replacing a liner. The fits and shoulders on both liner and cylinder should be carefully scraped and wiped clean to assure a water tight joint. Care must be taken not to damage these shoulders, as a water leak will result.

A copper gasket, 1/32" thick, forms the gas seal between the liner and the head. The gasket and both sealing surfaces must be carefully wiped free of all dirt when assembling.

3. CYLINDER HEAD

The individual cast iron cylinder heads are carefully designed to assure uniform cooling and accessibility of the water jackets. Depending on the engine model two or three large cleanout covers are provided.

On engines with $ll\frac{1}{2}$ " bore or larger positive cooling of the spray valve bosses is assured by nozzles projecting into the water jackets and discharging cool water directly against them. Water is supplied from a manifold located close to the exhaust manifold and fed at the center from the water inlet manifold.

The cylinder head is centered by means of a spigot which engages the bore at the top of the cylinder liner. The face of this spigot bears upon the copper gasket forming the gas seal. Brass bushings screwed into the cylinder and extending up into the head carry the cooling water. They are sealed by rubber grommets.

When a cylinder head is removed it should be placed on wooden blocks, never on concrete floor or steel deck. The rubber grommets should always be replaced by new ones and all dirt should be wiped from the bottom of the head before it is lowered onto the cylinder.

4. INLET AND EXHAUST VALVES

Two types of intake and exhaust valves are used on Atlas Imperial Diesel engines. One may be termed one-piece forged type and the other two-piece cast head type.

The two-piece cast head type consists of a valve head cast of special heat resisting alloy iron and a steel stem which is screwed and riveted to the head. Inlet and exhaust valves of the two-piece construction are interchangeable and the same valve may be used for either intake or exhaust.

On engines where valves of the one-piece forged type are used the exhaust valves are of a special heat resistant alloy steel and may be distinguished from the inlet valves by the "EXH." and "INL." stamped on the valve heads. The inlet valves are forged of chrome nickel steel and are not suitable for exhaust valves. The one-piece valves should never be used interchangeably except in an emergency.

In engines with $10\frac{1}{2}$ " or smaller bore the valves seat directly in the head. Renewable guides are pressed into the head. Engines with $11\frac{1}{2}$ " or larger bore have

both inlet and exhaust valves mounted in cages, bushed with renewable guides. The exhaust valve cage is water jacketed. Connections in the cooling water pipes must be broken when the exhaust cage is pulled. Exhaust cages must be pulled and water jackets emptied if engine is permitted to stand for any length of time in freezing weather as they will not empty from the main engine drain.

The cages are secured to the head with studs and are provided with jacking holes to facilitate their removal. Two jack screws are furnished with the tool equipment for this purpose. The cages are sealed against the head with copper gaskets at the bottom and cast iron piston rings installed in grooves above the port openings seal the cages at the top.

Depending on the engine model one or two concentric springs are used per valve. On the larger engine models the springs are held in place by a retainer which is secured to the valve stem by means of a split taper collar. Depressing the spring retainer against the springs permits the removal of the split collar and the disassembly of the valve and cage. On engines with 10" bore the upper end of the valve stem is threaded and spring retainers are held in place by a nut and locknut. On this engine model the length of the spring in place, with the valve closed, should be 4-3/16".

If the renewable valve stem guides are replaced they should be reamed after pressing in place with a standard reamer which produces a hole with a diameter to size or .0005" oversize. For instance, the 13" bore engine uses a valve with a stem diameter of 7/8". A standard 7/8" diameter reamer should then be used after the guides have been pressed into place in the cages. This reamer should then produce a hole with a diameter of .875" to .8755".

When grinding valves mounted in cages it is recommended that the cages be bolted into place in a cylinder head. A spare head may be used, or if a machine shop is available a sturdy fixture can be made up duplicating the cage bore in the head. The clamping nuts holding the cage to the head or fixture should be pulled up to approximately the same tension as when assembling in the engine. In this way any distortion of the cage and seat due to the clamping when the cage is in place will be duplicated while the valve is being ground, and a perfect seat will be assured. It will be found that this practice will practically double the interval between valve grindings. Always finish the grinding with fine compound, and take perticular care not to get any grinding compound into the guide. Thoroughly clean all traces of the grinding compound from valve and seat before reassembling.

Lubricate valve stem with clean engine oil before placing in guide. If valve faces are badly pitted they should be refaced in a lathe, as excessive grinding to remove pits will wear down the seats unnecessarily and will also cut a groove in the valve face. Badly pitted seats should also be refaced before grinding. Care must be taken to keep the seat concentric and square with the bore of the guide.

5. AIR STARTING VALVE (Engines with 13" to 15" bore)

The poppet type starting air valve, illustrated in Fig. H-1, is actuated from the camshaft by means of a lifter, pushrod and rocker, and is rendered inoperative while the engine is running by a pneumatic piston arrangement between the top of the valve stem and rocker. Fig. H-1 shows the device in the inoperative or cutout position, as it is when the engine is running. Valve (2) is held closed against its seat by spring (4), and piston (6) is down against cylinder (5), held so by a spring under the lifter. This spring holds the lifter and its latch up clear of the camshaft, so that as the cam rotates it does not contact the latch roller. (See description of latches under paragraph 28.) The pushrod is raised, rotating the rocker and holding piston (6) down against the cylinder as shown.

When the engine is to be started, starting air from the manifold enters port (10) and passes up through the drilled hole (9) in the valve stem to cylinder (5) where it raises piston (6) up against stop (7), collapsing the spring under the lifter, and forcing the lifter and latch roller down against the cam. As the camshaft then rotates piston (6) remains up against stop (7), the air force against the bottom of the piston being greater than that of valve spring (4) and the spring under the lifter,

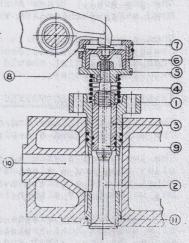


FIG. H-1

and the valve follows the motion of the cam, admitting starting air to the cylinder at the proper intervals. When the master valve in the starting air manifold closes and the pressure in the manifold drops, piston (6) is returned to its position against cylinder (5) by the lifter spring, and the valve remains closed.

Referring to Fig. H-1 the valve assembly is contained in cage (1) which is sealed to the head by copper gasket (11) at the bottom and by piston rings at the top and is held in place by two studs. Bronze bushing (3) works in the cage and is sealed against the starting air pressure by two piston rings. Stop (7) is threaded onto cylinder (5) and is locked in place by snap ring (8), the end of which is bent in and projects into a drilled hole in the cylinder. If either stop or cylinder are replaced this hole must be drilled in the cylinder, in line with the hole in the stop when the two parts are screwed tightly together. Use a 13/64" drill. The piston travel should be from .300" to .330", and may be adjusted by facing off the top of either the cylinder or the piston.

If the engine has been running or has been shut down for a considerable period of time and a period of maneuvering is anticipated, it is advisable to give the automatic air starting valves in the cylinder head a few drops of penetrating oil. Make sure that they are not stuck and squirt a little penetrating oil between the spring coils so that it will follow the stem down and lubricate bushing (3).

AIR STARTING VALVE (Engines with 10" to 112" bore)

On the smaller bore engines the starting air rocker is mounted eccentrically on the rocker shaft. When starting the engine an air ram described in Section R turns the rocker shaft and lowers the air start rocker until contact is made with the air start cam. Consequently on these engines the pneumatic piston arrengement described in paragraph 5 is not needed and is omitted, the rocker bearing directly on the valve stem. On ll½" bore engines the valve is mounted in a cage similar to that shown in Fig./H-1, while on the 10" bore engine the valve is guided and seated directly in the head. Hand oil the air start valves occasionally as described in paragraph 5.

7. PRESSURE RELIEF VALVES

Either two or three pressure relief valves are provided for each cylinder, located near the bottom of the head on the operating side of the engine. These include a manually operated relief or "snifter valve", a spring loaded safety valve, and on engines equipped with the automatic control system a pneumatically operated relief valve. If used, this valve is described in detail under the "Control System", Section R.

The valves are mounted in a tee screwed into the cylinder head. On standard engines without the pneumatic valve the snifter valve is in the top of the tee pointing up and the safety valve in the bottom. When the pneumatic valve is used it points down, the safety valve up and the snifter valve projects out from the end of the tee.

8. SNIFTER VALVE

The hand operated relief or "snifter" valves are small needle valves for release of the compression when barring over the engine. They are also used as shut-off valves when indicating or taking compression pressures.

9. SAFETY VALVE

The safety valves are spring loaded relief valves for the purpose of relieving excessive cylinder pressures. They act as telltales to indicate that the pressure is too high, and the popping of these valves is a definite indication that something is wrong and should be investigated at once. The valves are adjustable by tightening the spring retaining cover, and should be set to relieve at 800 lbs. per square inch. A setscrew locks the cover to maintain the setting. They should be tried out occasionally by prying up the lower spring washer with a screw driver to assure that they are in operating condition.

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PISTON AND CONNECTING ROD

1. PISTON

The pistons which are of the one-piece, solid-skirt type are made of high grade cast iron and are heat treated to relieve stresses and to obtain proper hardness. The piston is ground straight, that is without taper, from the bottom up to the ring belt. The clearance in the liner is .001" per inch of bore diameter. Due to manufacturing tolerances the total clearance of the piston skirt may vary .001" up or down from the above value. For example: the piston skirt clearance in a 13" bore engine should be between .012" and .014". The head of the piston being exposed to high temperatures is given a larger clearance, approximately .0055" to .006" per inch of bore diameter.

PISTON PIN -- (Tight in Piston)

The case hardened and ground piston pin is stepped, with differential fits in the piston pin bosses. The fits are about .0005" to .0015" press on the small end and metal to metal to .0015" loose on the large end. Rotation of the pin in the piston is prevented by the engagement of a dowel which projects radially from the large end of the pin with a groove in the bottom of the boss. A setscrew threaded into the smaller pin boss enters an indentation in the pin to act as a retainer. The setscrew is in turn secured by a locknut.

PISTON PIN -- (Floating in both Piston and Rod)

Floating type piston pins are retained in the piston by means of cast iron plugs which are pressed into a counterbore in the piston. A tapped hele is provided in each plug to permit removal. After one plug is removed the other one may be removed by inserting a rod or bar thru the piston pin and tapping lightly with a hammer. When replacing these plugs always be sure to line up the dowel pin with the slot in the piston. It is advisable to replace the plugs in the same counterbore from which they were removed. This type of pin should be fitted with a clearance of .0015" to .0025" in the piston.

3. PISTON RINGS

In engines with $10\frac{1}{2}$ " or smaller bore there are 6 rings per piston. In engines with larger bores seven rings are used per piston, an oil ring above and below the piston pin and five compression rings. Always assemble the oil rings with the bevel up, to slide over the oil film on the upstroke and scrape it down on the return. When overhauling pistons, thoroughly clean all carbon from rings and grooves and top of piston. Fuel deposit on the piston skirt can best be dissolved with cleaning solvent or paint remover. Be sure oil drain holes below oil rings are open.

Check rings for side clearance in grooves and end clearance, as measured in place in the liner. Side clearance should be .003" to .005" with new pistons and rings and end or gap clearance .005" per inch of bore diameter for the two top rings. For the other rings the gap clearance should be .003" per inch of bore diameter.

Rings should be discarded when the side clearance exceeds .008" and the end clearance .007" to .008" per inch of bore diameter. It is also a good policy to discard any rings which have been stuck for any length of time as they are apt to be out of round and may not hold compression. Always check new rings, measuring the side clearance, in the groove in which the ring is to run, with feeler gauge, and the end clearance with the ring in the liner at the smallest diameter. Never install rings with less clearance than that given above. As the oil rings wear the width of the flat increases, with consequent decrease in width of bevel and oil scraping ability. Experience will determine permissible wear without excessive oil pumping.

4. CONNECTING ROD

The connecting rods are steel drop forgings, rifle drilled to carry oil to the piston pins. Shims between foot of rod and crankpin box provide adjustment to balance compression pressures in the cylinders to the desired value. The distance "X" (see Fig. K-1), between the top of the piston and the top of the liner should be in accordance with the tabulation below.

Engine	Dimension	Engine	Dimension
Bore and Stroke	"X"	Bore and Stroke	"X "
10 x 13	13/16"	13 x 16(Turbo.)	1 3/32"
10 x 13 262	13/16"	14½ x 18	1 7/16"
11½ x 15	15/16"	15 x 19	1 3/16"
13 x 16	1 1/32"	15 x 19(Turbo.)	1 9/32"

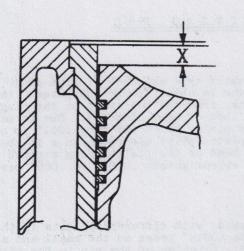


FIG. K-1

When taking measurement "X" the piston should be at top dead center and the cylinder liner must be securely clamped down into the cylinder. The cylinder stud nuts must also be tight when making this adjustment. Connecting rod shim adjustment in accordance with the above tabulation should be used for altitudes from sea-level to 1500' and will then produce compression pressures of 400 to 410 pounds per square inch. If the engine is located at higher altitudes than 1500 feet above sea-level dimension "X" should be smaller than the tabulated values. The Engineering Department of Atlas Imperial Diesel Engine Co. will advise the proper adjustment if the engine serial number and altitude is stated.

A bronze bushing for the piston pin is pressed in the upper end of the rod. If this bushing is replaced it must be reamed to allow a piston pin clearance of .002" to .003" on 10" bore engines and .0035" to .005" on engines with larger bore. Care must be taken to keep the reamed hole exactly

parallel with the foot of the rod. The oil grooving in the bushing is carefully designed for correct lubrication, and new bushings must be inserted in rod with the relief grooves on the horizontal axis of the pin. A ball check valve at the bottom of the rod prevents return of the column of oil in the rod.

Examine these valves at annual overhauls. The ball lift should not exceed 3/32".

5. CONNECTING ROD BEARINGS

The crankpin boxes are steel castings with babbitt lining centrifugally cast and accurately bored. No attempt should be made to rebabbitt these boxes in the field. New boxes may be obtained from A.I.D.E. Co. and a credit allowance will be made for old boxes returned. Bearing adjustment is by means of shims between halves of bearing. Bearing clearances when adjusted should be .0008" to .0009" per inch of bearing diameter.

Clearances are best measured with a lead wire compressed between bearing and journal, as described in Section F. Keep the shim thickness equal on the two sides. Inspect the bearing surfaces for even bearing. Areas which are not bearing on the shaft will be discolored, and such bearings as well as new ones should be carefully scraped to secure even bearing over at least 3/4 of the entire area. End clearance is .007" to .015" and should not be allowed to exceed .025"

The two crankpin box halves are held together by bolts so that the connecting rods and connecting rod bolts can be removed without disturbing the bearings. On some 13" bore engines the lower base is shallow and at its lowest point the connecting rod box passes close to the lubricating oil header. If the crankshaft in these engines is barred over with the crank pin bearings loose on the shaft be sure to keep the bearings in a vertical position as they approach and pass over bottom center as they will not clear the lubricating oil header below the crankshaft if they are turned appreciably from the vertical. The header may be severely damaged if struck by the crankpin bearing boxes.

NOTE: 15" bore engines built 1941 or later are equipped with loose bearing shells in the crankpin boxes. These shells are bronze backed and care should be taken that backs of shells and bores of boxes are absolutely clean when assembling. The shells project above the faces of the crankpin box halves .003" to .005" but are squeezed down flush when the connecting rod bolts are tightened up.

6. CONNECTING ROD BOLTS

The connecting rod bolts, fitting in reamed holes, hold the two halves of the crankpin boxes together and to the foot of the rod. The nuts should be kept pulled up tightly but not overstressed. They should not be sledged but should be pulled up by hand with a pipe about four feet long on the wrench. It is good practice to keep a record of the length of connecting rod bolts, measured with a micrometer at annual overhauls and to discard bolts that show more than .010" increase in length. It is further recommended that all connecting rod bolts be replaced every two years, assuming the engine to have had continuous service during that time, say 8000 hours or more. It is nearly always old bolts that have been in service for some time and have been overstressed by pulling up the nuts too tightly that fail. Replacing bolts as suggested above is cheap insurance against the possibility of wrecking an engine through connecting rod bolt failure. Replace cotter pins carefully, always using new cotter pins, Be sure that they are a close fit in the hole and bend the

ends back tightly against the sides of the nut. If this work is left to inexperienced mechanics it should be very carefully inspected at the completion of the job. Always replace rods, bearings and pistons in the cylinders from which they were removed. All parts are numbered.

K1 - Ed 4(3)

CAMSHAFT AND VALVE OPERATING GEAR

1. CAMSHAFT

The camshaft is made of 2" ground steel shafting. The keyways in the shaft are indexed for the firing sequence stamped on the engine nameplate when the engine is running in the "Ahead" direction of rotation. Number 1 cylinder is located at the forward end of the engine. The high pressure fuel pump crankshaft is part of the camshaft assembly and is bolted to a coupling flange which has been shrunk on and keyed to the aft. or pump end of the camshaft.

2. CAMSHAFT BEARINGS

The camshaft bearings are accurately machined cast iron blocks with pressed in bronze bushings. Bearing bore in bushing is reamed to 2.005" - 2.006" diameter which allows a running clearance of .005" to .007". If replaced the bushings must be reamed and oil and mounting holes drilled through after pressing in. A groove must be chipped to communicate with the oil hole if it does not intersect the groove in the bushing. The bearing blocks are held in machined seats cut in the webs of the centerframe and are secured by capscrews.

The camshaft thrust is carried by the two bearings adjacent to the fuel pump crankshaft. These two bearings differ from the other bearings in that the bushings have thrust faces. The face of the forward bearing contacts the forward face of the coupling shrunk on the end of the camshaft and the face of the after bearing engages the web on the after end of the fuel pump crankshaft. The two bearings are adjusted in a fore and aft direction to permit a camshaft end play of .015" to .020". All the bearings except the two thrust bearings and the bearing at the extreme forward end depend upon spray from the connecting rods and main bearings for lubrication. Catch basins in the top of the bearings collect the oil. The two thrust bearings and the forward bearing are supplied with oil from the force feed lubricating oil system.

3. CAMS

The cams are accurately ground to shape after being case hardened. The fuel valve cam consists of a case hardened steel disc in which a case hardened steel toe is inserted. This toe controls the action of the spray valve, the disc serving as a base circle. The cams are a sliding or light tap fit on the camshaft and are held in position by taper keys driven securely into place after the cams have been located to line up with the latch rollers properly. The ahead inlet and exhaust cams serve as hubs to which the astern inlet and exhaust cams, the ahead and astern air starting cams and the fuel cam disc are bolted. This cam sequence or arrangement may not apply to the 13 x 16 Turbo-charged engines, especially late model engines which use two loose cams for either inlet or exhaust. For correct cam sequence see the parts catalog plate facing the Camshaft Group. Elongated holes in the fuel cam disc allow angular adjustment with respect to the hub, permitting exact setting for timing.

4. CAMSHAFT REMOVAL

- (a) Disconnect the linkage between the governor and the wedge shaft, and disconnect the lubricator strap and the pump connecting rods on the forward end of the cam-
- (b) Remove the engine control parts, the latch shaft interlock (on lever controlled engines), and the pilot valves from the top of the latch box.
- (c) Remove the latch box.
- (d) Remove the latch shaft and latches.
- Remove all push-rods.
- (f) Pull the lifters upward away from the cams and secure them in this raised position with a hose clamp or some other suitable device.
- (g) Remove the rotary pump housing together with the three pumps.(h) Disconnect the fuel lines from the high pressure fuel pump and remove the pump housing assembly.
- (i) Remove the bearing caps of the high pressure fuel pump connecting rods and remove the crosshead plugs, oil guards, sleeves and guides.
- i) Take out the cam bearing retaining capscrews. (k) Loosen the cylinder nuts on the camshaft side of the engine.
- (1) Remove the camshaft. Sledge each bearing block out of its seat a little at a time using a timber inserted through the openings on the exhaust manifold side. The end of the timber should be placed against the camshaft as close to the bearing as possible. When the camshaft has been partially removed it will be possible to withdraw the connecting rods and crossheads of the fuel pump downward.

5. CAMSHAFT DISASSEMBLY

After the camshaft has been removed from the engine it should be disassembled as follows. The bilge pump crank is removed either by a suitable puller or by driving with a babbitt hammer. Then, after removing the first cam bearing the clamping bolts of the camshaft gear hub are loosened and the whole assembly slid off. Bearings and cams are then removed successively from the forward end of the camshaft. FOR ALL RIGHT HAND OR PORT ENGINE, ALSO FOR LEFT HAND OR STARBOARD ENGINES WITH 10". 10½" AND 11½" BORE, the cams are loosened by driving the keys forward with a drift. FOR LEFT HAND OR STARBOARD ENGINES WITH 13" BORE ONLY, the cams are loosened by driving the keys aft with a drift. The cams should slide on the shaft freely after the keys have been removed, but if it should be necessary to drive them off, only a babbitt hammer or brass drift should be used. Any burrs, particularly at keyways, must be dressed down with a file. If this precaution is not taken the cams may seize as they are removed and forcing the cams the remainder of the distance will

6. CAMSHAFT ASSEMBLY & INSTALLATION

When the camshaft is being reassembled the same precautions with regard to burrs apply. Coating the bores of the cams with white lead will aid materially in sliding the cams into place without scratching the shaft. The bores of either new or old cams should be inspected carefully for any defects likely to scratch the shaft. Bearings and cams are installed successively from the forward end but are not keyed to the shaft until later. The hub and cam gear are assembled on the shaft and clamped tightly. The camshaft gear should be located with its forward face a distance from the end of the shaft according to the following table:

10", $10\frac{1}{2}$ " and 13" bore engines - - - 6" $11\frac{1}{2}$ " bore engines - - - $6\frac{1}{4}$ "

The assembled camshaft is then installed in the engine. After starting each cam bearing in its seat the bearings are driven into place a little at a time with a heavy brass bar. Each bearing should be driven a little and then left until all the others have been knocked in the same amount so that the camshaft will not be bent. The cam bearings will seat more easily if the cylinder nuts are loose.

The connecting rods and crossheads of the high pressure fuel pump must be assembled as the camshaft is being driven into place. The crossheads should be inserted in the holes in the centerframe before the camshaft has been driven in any appreciable distance. When the camshaft has been partially installed it will be possible to place the connecting rods on their respective cranks. After this last step the connecting rods and crossheads need no further attention as the cam bearings are being seated.

After the cam bearings have been securely bolted, the latch shaft and latches should be installed. The cams are then ready for keying. Starting with Number 6 (flywheel end) cylinder place each set of cams directly under the proper latch rollers and secure the cams to the shaft by inserting the taper keys. FOR ALL RIGHT HAND OR PORT ENGINES ALSO FOR LEFT HAND OR STARBOARD ENGINES WITH 10", 10½" and 11½" BORE drive each key toward the after end of the engine (large end of key should be forward). FOR LEFT HAND OR STARBOARD ENGINES WITH 13" BORE ONLY, drive each key towards the forward end of the engine (large end of key should be aft). Complete this procedure with each set of cams before going to the next one and work forward from the after end of the engine.

The engine should next be timed, in accordance with the detailed instructions in Paragraphs 14 to 17 after which the latch box and control parts may be reassembled on engine. For Fuel Spray Valve timing see Section 0.

7. VALVE LIFTERS

The steel valve lifters work in cast iron guides bolted to the top of the center-frame and carry case hardened rollers on steel pins on their lower ends. (The air starting lifter does not have a roller.) Clearance between lifters and guides is .0015" to .0025", between rollers and pins is .001" to .002", and the pins are riveted into the lifter forks, with the ends flush, so that they may enter the guide bores. A hole in the lower end of the starting air lifter engages a pin carried in bosses on top of the latch, which serves to lift the latch clear of the cams when the engine is running.

8. PUSH-RODS

The engine may be equipped with either of two types of push-rods. One style connects to the valve rockers with forks which are screwed on to the end of the push-rod and

secured by a locknut. The forks are connected to the rockers with steel pins which are held in place by a ball check pressed into the rocker. This ball check engages in a circumferential groove around the center of the pin, and may be removed by tapping with a hammer and drift. The pins are fitted with a clearance in the rocker of .000" to .0025", and a clearance of .0005" to .0027" in the forks. Holes located near the top of the push-rod provide a means for turning the rod when making adjustments.

The other style of push-rod engages the rocker by means of a ball and socket, the socket being in the end of the push-rod. The ball screws into a tapped hole in the rocker and provides the means for adjusting the clearance between the rocker and valve. The ball studs are retained by a capscrew clamping the threads. These clamp screws should be kept tight so that there is no chance of the ball stud working loose and changing the clearance between rocker and valve, and also to prevent stripping of the thread due to the continued hammering action of the push-rods.

The steel pins which link the forks to the rockers have - .0005" to - .0027" clearance in the forks and .000" to .0025" clearance in the rocker ends. The pins are retained by ball checks which are pressed into the rocker ends and which engage circumferential grooves at the centers of the pins. The pins may be removed by tapping with a hammer and drift.

9. VALVE ROCKERS

The rockers for the inlet, exhaust and starting air valves are fulcrumed on a shaft which is supported by bearings at each end. The bearings are mounted on study screwed into the cylinder heads and are held between nuts on the study. By screwing the nuts up or down the rocker shaft can be raised or lowered.

The three rockers are bronze bushed at their fulcrums and the bushings are reamed for .001" to .003" clearance with the rocker shaft after pressing in. The case hardened rollers at the valve end of the exhaust and inlet rockers work directly on the valve stems and turn on steel pins riveted in the rocker forks. The clearance of the rollers on the pins is .0005" to .0015".

The fuel valve rocker is not carried on the shaft with the other three rockers. A support located on the manifold side of the cylinder head acts as a fulcrum. The steel fulcrum pin, retained by cotter pins at each end, has a clearance of .000" to .0017" in both pieces.

10. VALVE TIMING

The correct valve timing for the engine is given in the following table.

Starting Air Valve Opens 50 B.T.C 50 B.T.C. E. 7 W. " " Closes 450 B.B.C 500 B.B.C. E. 7 W. Inlet Valve Opens 100 B.T.C 800 B.T.C. E. X. W. " " Closes 350 A.B.C 300 A.B.C. 7 A.W. Exhaust Valve Opens 350 B.B.C 450 B.B.C. E. X. W. " " Closes 50 B.T.C 50 B.T.C. E. X. W. Exhaust Valve Opens 350 A.T.C 650 A.T.C. IX W. Fuel Spray Valve Opens see engine name plate " " " Closes see engine name plate		Non Turbocharged	13 x 16 Turbocharged
	" " Closes	50 B.T.C	- 50 B.F.C. E. Y. W 500 B.B.C. E. A. K 800 B.T.C. E. A. K 300 A.B.C. T. A. K 450 B.B.C. E. A. K 650 A.T.C. J. X. K. ate

11. SPOTTING THE PISTON

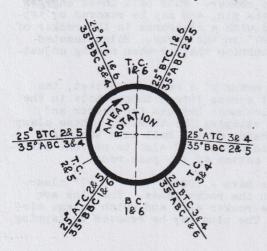
Before proceeding with the discussion on valve timing the following instructions regarding the correct method of spotting a piston should be considered. Whenever a piston is to be spotted for valve setting it should be brought into position by turning the engine in the direction of ahead rotation in order to take up all gear back-lash. If the engine is turned past the desired position, it should be turned well back in the opposite direction, and then again brought up to the required point.

12. FLYWHEEL MARKINGS

NOTE: The following data applies to Non-Turbo-charged engines and is intended for a general description of the markings only. For actual figures for valve timing see paragraph 10 above.

The 13 x 16 Turbo-charged engine flywheel is marked similarly except the degrees are marked completely around the full circumference due to the earlier opening and later closing of the valves. The description following may be applied to the turbo-charged engines providing the figures given paragraph 10 above are substituted.

The position of the piston may be determined from the flywheel pointer and the mark-



ings stamped on the flywheel rim. Top center of each piston is marked and stamped with the corresponding piston numbers, and degree marks are stamped for 25° on each side of top center. These markings are sufficient for all valve timings. The intake valves normally open 100 B.T.C. (Before Top Center) and the exhaust valves close 5 A.T.C. (After Top Center) and these points can of course be determined directly from the degree markings adjacent to the top center marking of the corresponding cylinder.

The intake valves normally close 35° A.B.C. and the exhaust valves open 35° B.B.C. Referring to Fig. L-1, these points may be obtained on the flywheel as follows. Since the crankshaft has three throws 120° apart the top centers of the three pairs of cylinders will be 120° apart. Bottom center of any pair of cylinders is 180° from top center. Therefore the bottom center of any pair of cylinders is 60° from the top centers of the other two pairs. As previously stated, each top center is marked for 25° in either direction.

FIG. L-1

Subtracting this 25° from the above 60° leaves
35°. Hence each 25° A.T.C. point is also the 35°

B.B.C. point for the preceding pair of cylinders and similarly each 25° B.T.C. point is also the 35° and similarly each 25° B.T.C. point

is also the 35° A.B.C. point for the following pair of cylinders.

13. POINTER LOCATION

The location of the flywheel pointer should be checked occasionally by "splitting the center". With one of the cylinder heads removed crank the engine to a point about 20° off top center. Measure the exact distance from the top of the liner down to the piston and observe the pointer reading on the flywheel. Then set the piston to the same distance below the top of the liner on the other side of top center and observe the flywheel pointer reading. If the readings do not agree adjust the pointer to give equal readings on each side. These readings should preferably be taken with an indicator and in each case the piston should be cranked upward into position.

14. CAMSHAFT TIMING

In order to time the engine it is necessary to determine the correct relation between the crankshaft and camshaft, which is done by positioning the camshaft gear on its hub, and then to adjust the push rods to open and close the valves at the correct points. Unless the crankshaft gear, camshaft gear or camshaft gear hub have been replaced, the camshaft can be correctly timed after overhauling as follows. Before breaking the gear train spot No. 1 piston exactly on firing top center. With a steel scale bearing firmly against the machined side of the centerframe scribe a line across the side of the camshaft gear parallel to the centerframe face. When re-assembling mesh the gears with the crankshaft and camshaft in the same relative positions, that is, with No. 1 piston on firing top center and the line on the camshaft gear in line with the centerframe face.

If the crankshaft gear, camshaft gear or the camshaft gear hub is replaced, the camshaft may be timed as follows:

- (a) Spot No. 1 piston $2\frac{10}{2}$ B.T.C. (13 x 16 Turbocharged $7\frac{10}{2}$ B.T.C.) in the AHEAD direction.
- (b) Set the camshaft gear relative to its hub so that clamping bolts are approximately in the center of the slots. Orient camshaft gear so that old dowel holes will not interfere with redowelling.
- Turn the latch shaft to the AHEAD position (latches out). (d) Turn the camshaft (with intermediate gear out of mesh) so that the inlet and exhaust lifters of No. 1 cylinder are each raised an equal distance. (NOTE: The piston was set at $2\frac{10}{2}$ B.T.C. (or $7\frac{10}{2}$) as this is the mean position between the opening of the inlet valve, and the closing of the exhaust valve, and at this position both valves should be open an equal distance.)
- (e) Holding crankshaft and camshaft in above positions and allowing the camshaft gear to slip on its hub as required, mesh the intermediate gear and tighten the clamp bolts between the camshaft gear and hub. After all valves have been timed and checked, drill 31/64" holes through gear in line with dowel holes in hub and ream to .497" - .498" for dowels.

After determining the correct relation between the camshaft and crankshaft the push rods must be adjusted as follows: (See Section O for timing of fuel spray valve.)

15. INLET & EXHAUST VALVE TIMING

(a) Non-Turbo-charged engines:
1. Spot piston at 100 B.T.C. at the end of the exhaust stroke.

Adjust inlet push-rod so that valve is just opening.
 Spot piston at 5° A.T.C. on the suction stroke.
 Adjust exhaust push-rod so that valve is just closing.

(b) 13 x 16 Turbo-charged engines only:

1. Spot piston at 80 B.T.C. near end of exhaust stroke.

2. Adjust inlet push-red so that the valve is just opening.

3. Spot piston at 650 A.R.C. on the suction stroke.

4. Adjust exhaust push-rod so that valve is just closing.

The following applies to both Non-Turbo-charged & Turbo-charged engines:

(c) Check clearances between valve stems and rocker rollers. The cams are designed for 1/32" clearance with the valves set as above and with the engine cold, but this will vary somewhat due to manufacturing tolerances. When making the adjustments aim at the opening and closing points but keep the clearances between .020" and .040", varying the opening and closing points slightly if necessary. Excessive clearances mean a noisy engine and increased wear on parts. Insufficient clearances prevent valves from seating properly, with consequent blowby and destruction of valves and

(d) Check and record closing point of inlet valve and opening point of exhaust valve. These points should fall within 5° of the position given in the timing table.

(e) Shift latch shaft to ASTERN and check opening and closing points of inlet and exhaust valves when running ASTERN. Discrepancies from the AHEAD timing up to 5° may occur due to manufacturing tolerances, but no attempt should be made to correct this condition, as any changes in the push-rod adjustments will upset the AHEAD timing.

(f) Adjust and record valve timing for the other cylinders as above.

16. STARTING AIR VALVE TIMING - ENGINES WITH 13" BORE

(a) Insert steel block 5/16" thick between the air starting rocker and the top of

the piston in the pneumatic tappet in the starting air valve.

(b) Spot piston at 5° B.T.C. at the end of the compression stroke (in the AHEAD direction and with latch shaft AHEAD) and adjust the pushrod so that the valve is just opening. Check the closing point, which should fall within 50 of the position given in the table. (See Paragraph 10) (c) Shift latch shaft to ASTERN and spot piston at 50 B.T.C. ASTERN.

(d) Adjust astern air starting cam relative to its hub so that starting air valve is just opening and clamp cam to hub. Check closing point.

(e) Adjust and record starting air valves for the other cylinders as above.

17. STARTING AIR VALVE TIMING - ENGINES WITH 111 OR SMALLER BORE

(a) Bar the valve rocker shaft by hand to its starting position (up against the

stop in the air cylinder).

(b) Spot piston at 50 B.T.C. at the end of the compression stroke (in the AHEAD) direction and with latch shaft AHEAD) and adjust the pushrod so that the valve is just opening. Check the closing point, which should fall within 5° of the position given in the table. (See Paragraph 10)

(c) Shift latch shaft to ASTERN and spot piston at 50 B.T.C. ASTERN.

(d) Adjust astern air starting cam relative to its hub so that starting air valve is just opening and clamp cam to hub. Check closing point.

(e) Adjust and record starting air valves for the other cylinders as above.

18. CAMSHAFT DRIVE GEARING - ENGINES WITH 13" BORE

The camshaft is driven from a gear on the crankshaft by means of an intermediate gear. The helical crankshaft gear is shrunk on the crankshaft between the two forward main bearings. If replaced the new gear should be heated to approximately 6000 F. and slipped over the shaft against a temporary spacer to locate the inner face of the gear 8-1/4" from the machined face of the first crank web. Do not overheat the gear, as this will damage the steel structure, and once it is started onto the shaft move it immediately to the final position, as it will be impossible to move it farther once it begins to cool and seize the shaft. If this should happen it would be necessary to destroy the gear in order to remove it. The intermediate gear has replaceable bronze bushings and rotates on a case hardened steel shaft. The intermediate gear bracket or bearing in which the gear and shaft are mounted is bolted and doweled to the top of the centerframe. Shims between the bearing and the centerframe and movement of the bearing transversely permit backlash adjustment of the gears, which should be set at .006" to .008". If the bushings in the intermediate gear are replaced they should be reamed to 2.937" to 2.938" diameter and faced to 3.002" to 2.998" in thickness after being pressed into the gear. The clearance between the gear bushings and the shaft should then be .002" to .004" and the total lateral clearance .005" to .012". Lubricating oil under pressure is supplied to the intermediate gear bearing from the header in the base.

The camshaft gear is bolted and doweled to a hub which is keyed and clamped to the forward end of the camshaft. It should be located fore and aft in line with the intermediate gear.

19. CAMSHAFT DRIVE GEARING - ENGINES WITH 112" BORE

The camshaft is driven from a gear on the crankshaft by means of a compound intermediate gear. The helical crankshaft gear is shrunk on the crankshaft in front of the last forward main bearing. It should be located 1/4" from the machined face of last crank web. Do not overheat the gear, as this will damage the steel structure, and once it is started onto the shaft move it immediately to the final position, as it will be impossible to move further once it begins to cool and seize the shaft.

The intermediate gear has replaceable bronze bushings and rotates on a case hardened steel shaft. The intermediate gear bracket or bearing in which the shaft is mounted is bolted and doweled to the end face of the centerframe. Shims between the gear bracket and the end main bearing cap permit alignment of the gear and adjustment of backlash which should be set at .006" to .008". If the bushings in the intermediate gear are replaced they should be reamed to 2.999 - 3.000 diameter and faced to 5.502 - 5.498 thickness after being pressed into the gear. Lubricating oil under pressure is supplied to the intermediate gear bracket from the lubricating oil pressure system.

The camshaft gear is bolted and doweled to a hub which is keyed and clamped to the forward end of the camshaft. It should be located fore and aft in line with the intermediate gear.

20. CAMSHAFT DRIVE GEARING - ENGINES WITH 10" AND 101 BORE

Paragraph 19 applies with the following exceptions. The intermediate gear bracket or bearing in which the shaft is mounted is bolted and doweled to the forward end centerframe cover. If gears are replaced backlash should be adjusted to .006" to .008". If bushings in the intermediate gear are replaced they should be reamed to 2.249" - 2.250" diameter and faced to 4.63/64" after being pressed into the gear. The crankshaft gear is in this case located against the machined face of the forward crank

FUEL SUPPLY SYSTEM

The complete fuel system may be conveniently divided into two parts, the fuel supply system and the fuel injection system. The fuel supply system is made up of the fuel transfer pump, the fuel day tank and the fuel filter, while the fuel injection system includes the high pressure fuel pump, the fuel rail, the accumulator, the fuel pressure regulating valve, the fuel spray valves, and the necessary connecting tubing.

1. IMPORTANCE OF CLEANLINESS IN FUEL HANDLING

The high pressure fuel pumps and fuel spray valves have been referred to as the heart of the Diesel engine and the proper functioning of these parts is necessary for the successful operation of the engine. These pumps depend upon lapped plungers working in cylinders with clearances measured in hundred thousandths of an inch and it is vital that the fuel entering these parts be kept free of any grit or foreign matter. The engine is equipped with filters for this purpose but it is also necessary for the operators to use every possible care in getting clean fuel oil and in keeping it clean until it is delivered to the engine. Fuel tanks and piping should be thoroughly cleaned when installed and should be kept covered at all times.

The fuel filter should be periodically cleaned and serviced according to the detail instructions given in paragraph #3. The best filters obtainable will be useless if dirt is introduced into the fuel after it has passed through them, and it is therefore of great importance that every effort be made to protect the fuel pipes after the filter during repairs and overhauls. Cleanliness in handling fuel, piping and injection equipment is of vital importance and will pay good dividends in trouble-free operation. Many times mysterious and expensive pump and fuel spray valve troubles have been traced to careless handling of fuel and carelessness in storing and installing spare parts.

2. FUEL TRANSFER PUMP

The fuel transfer pump, which is located in the rotary pump housing on the after end of the centerframe,

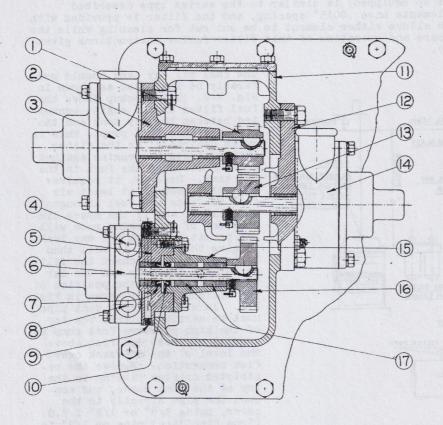


FIG. N-1

delivers a continuous supply of fuel to the engine from the main storage tank. It is a rotary type gear pump, identical in construction (but smaller in size) with the lubricating oil pumps described in Section S. The description will not be repeated here, nor the instructions regarding direction of rotation, which apply equally well to the transfer pump. (On direct reversible marine engines the rotary gear type fuel transier pump is reversible. Consequently fuel is delivered from the same port irrespective of direction of rotation.) The fuel transfer pump drive is shown on Fig. N-1. Transfer pump (6) is mounted in adapter (5) which is bolted and doweled to housing (11). If the adapter is replaced it must be positioned for .004" to .005" gear backlash before doweling. A cylindrical fit between pump and adapter permits replace-ment of the pump without disturbing the drive gear setting. The pump shaft and rotor is

carried in three bronze bushings one in the adapter and two in bearing (15) which is bolted to the adapter. If replaced these bushings must be line reamed to .6250"-.6255" dia. after pressing in and with the bearing bolted to the adapter.

The bushing in the adapter is lubricated by fuel oil from the pump, and the two in the bearing by lubricating oil, fed through drilled holes in the castings from a lubricating oil line connecting into the adapter. Oil seals (7) and (10) prevent contamination of the lubricating oil by the fuel oil and if replaced must be installed as shown, that is with the leather ends together and flush with the ends of the bores. Some engine models are equipped with one rotary type seal instead of the two seals shown in Fig. N-1. This type of seal rotates with the pump shaft and seals against the specially prepared faces of the adjacent bushings. Fuel leakage past the seal is drained off through connection (9), which should be piped back to the fuel tank. Under no circumstances should this opening be plugged, or the fuel will drain into the lubricating oil in the crankcase. Drive gear (16) is secured to the shaft with a Woodruff key and setscrew, which should be securely wired, as should all the internal bolts in the assembly.

3. FUEL OIL FILTER - (Series Type - Standard Equip.)

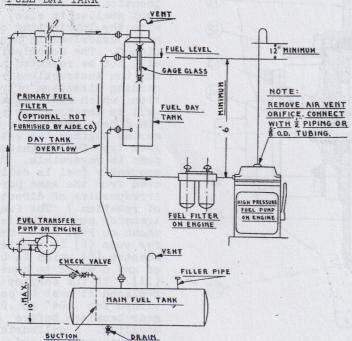
The fuel oil filter is a metal edge type filter, similar to the lubricating oil filter described in Section S and the detailed description will not be repeated here. There are two elements in series, with .002" and .003" spacing. The dirt may be scraped off the elements by turning the cleaning handles on the top, and this should preferably be done when the engine is not running so that the dirt can settle freely to the bottom of the sump tanks although there is no objection to cleaning with the engine running. The sumps should be drained before the dirt builds up to the level of the elements.

After draining refill the filter through the priming plug in the top, and leave the vent cocks slightly open when starting the engine to allow the trapped air to bleed out. The filter elements may be replaced by removing the handles and sump tanks and unscrewing the elements from the head. CAUTION: Element is attached to head with left hand thread. Assemble with .003" element on the inlet side.

4. FUEL OIL FILTER - (Duplex Type - Special Equip.)

This filter (if engine is so equipped) is similar to the series type described above, except that the elements have .0015" spacing, and the filter is provided with a switch-over valve which allows either element to be cut out for cleaning while the engine is running. For care and operation of this filter follow instructions given above for the series type.

5. FUEL DAY TANK



The fuel oil day tank should preferably be installed as shown in Fig. N-2. This hookup shows the fuel filter on the engine connected between the day tank and the high pressure fuel pump. This is quite desirable, as the filter then protects the engine against contamination of the fuel in the day tank. However, it requires a gravity head of at least six feet to force the fuel through the filter, and if the space limnot permit locating the day tank to give this head, it will then be necessary to connect the filter between the pump and the day tank, that is, in the position of the optional filter shown in Fig. N-2. In either case a vent pipe must be carried up from the top of the high pressure fuel pump to a point at least one foot above the level of the day tank overflow connection. Remove the restricted orifice fitting in the top of the pump cover, and con-nect the pipe directly to the cover, using 3/8" or 1/2" I.P.S. (Iron Pipe Size) pipe or 1/2" to

FIG. N-2 (Iron Pipe Size) pipe or 1/2" to 5/8" 0.D. copper tubing. The end of the pipe must be protected to prevent the entrance of dirt and moisture.

The suction pipe from the pump to the storage tank and the day tank overflow pipe should be 1/2" or preferably 3/4" I.P.S. and the pressure pipe from the pump to the engine should be 1/2" or 3/4" I.P.S. For long pipes use the larger of the sizes given.

While the installation with fuel day tank as shown in Fig. N-2 is recommended and the tank is furnished with the engine it is not absolutely necessary. If desired the tank may be omitted and the hookup made according to Fig. N-3. The advantage of the day tank is that fuel is always available under a gravity head for starting the engine and in case of failure or loss of prime of the transfer pump the engine will run for some time on the fuel in the day tank. If a day tank is not used the engine will stop almost immediately upon failure of the transfer pump.

If the hookup without the day tank is used, as shown in Fig. N-3 the vent connection in the top of the high pressure fuel pump must be piped back to the main storage tank as shown, and in this case the throttling orifice in the top of the pump should not be removed, but the fuel return pipe should be connected into this orifice.

This return line provides for a continuous flow of fuel through the top of the high pressure pump and insures the removal of any air trapped in the fuel. The restricted opening in the air vent orifice is proportioned to give

AIR VENT ORIFICE HIGH PRESSURE FUEL PUMP FUEL FILTER ON ENGINE PRIMARY FUEL FILTER RETURN PIPE (OPTIONAL- HOT B I.P.S. OR 2 0.0. FURHISHED BY A.I.D.E.CO.) COPPER TUBING FUEL TRANSFER PUMP ON ENGINE VENT FILLER PIPE TO-HXH-D MAIN FUEL TANK SUCTION DRAIN

FIG. N-3

ed opening in the air vent orifice is proportioned to give the desired pressure in the high pressure pump suction chamber. If the main fuel tank is above the engine room level, the return pipe should spill over into the top of the tank, and the pump suction should be taken from some distance above the bottom of the tank to prevent sucking sludge and the water into the engine. The fuel return line should be 3/8" I.P.S. or 1/2" 0.D. copper tubing, the pump suction pipe should be 3/4" I.P.S. pipe, and the pressure pipe 1/2" I.P.S. or larger.

While not absolutely necessary, it is suggested that a primary filter (not supplied by A.I.D.E. Co.) be employed in addition to the filter on the engine. This will collect the larger particles of dirt, and will thus materially increase the necessary cleaning interval of the engine filter. If used in connection with a day tank it should preferably be connected before the tank as shown in Fig. N-2 thus keeping the fuel in the tank clean. If a day tank is not used it should be connected in

the pump suction, as shown in Fig. N-3. In either case, but particularly in the latter, it should be of ample capacity and of duplex construction, with built-in switch valve for cutting either unit out of service for cleaning. A Purolator filter, Type Dll3JJ with .003" spacing is recommended.

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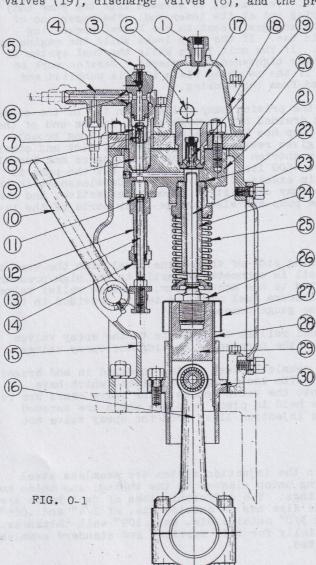
1. HIGH PRESSURE FUEL PUMP

The high pressure fuel pump is located on top of the centerframe between the fly-wheel and Number 6 cylinder on the operating side of the engine. The pump consists of two plungers actuated by crossheads and connecting rods from a crankshaft which is bolted to the after end of the camshaft. A small hand operated plunger is also built into the pump and is used for priming the fuel system and for building up fuel pressure when the spray valves are being timed or tested.

Referring to Fig. 0-1 cast iron guides (30), located in holes in the centerframe and secured by capscrews, carry crossheads (29), which are actuated by the crankshaft and connecting rods (16). The bronze connecting rods have a clearance of .0005" to .0025" on their crankpins and a side play of .005" to .009". Roller bearings in the upper end of the connecting rods constitute the wrist pin bearings, and the pins have .0005" to .0015" clearance in the crossheads. Each crosshead has a replaceable bronze sleeve (28), held in place by a shoulder on the lower end of the crosshead and by the oil guard (27) and plug (26) at the upper end. The clearance between this sleeve and the crosshead guide is .002" to .004" and if it becomes excessive new sleeves should be installed. Lubrication is by spray from the cranks.

Pump housing (15) supports mounting plate (20) and carries handle (10) and shaft of the priming pump. Mounting plate (20) which is bolted to the top of the housing carries the individual pump bodies (21) on its lower face. The pump bodies contain all the essential parts of the pump, namely, barrel (24) and plunger (23) suction valves (19), discharge valves (8), and the priming pump plunger assembly (12) and (13).

1.



The suction and discharge valve assemblies extend upward through holes in the mounting plate and a suction chamber (17) is formed by the mounting plate and its cover (18). A reservoir of fuel under low pressure is consequently located immediately above the suction valves.

Plunger and barrel assemblies (23) and (24) of the main pumps are installed in seats in the bottom of pump bodies (21). Retaining nuts hold the barrels in place and copper gaskets between the barrels and seats form the seals. Springs, retained at the lower ends of the plungers by special washers, force the plungers downward on the suction strokes. The plungers and barrels are lapped together in matched pairs and are not interchangeable. Always use care to prevent mixing them. If either piece becomes scored or damaged both must be replaced. Always wash parts thoroughly in clean solvent or fuel oil and lubricate with clean engine oil before replacing.

When dismantling the pump, mounting plate (20) together with the pump bodies and plunger barrel assemblies should be removed from the housing as a unit. Hold the plungers in place as the unit is lifted, as they will drop out when free of the crossheads.

Suction valves (19) are located in pockets in the top of the pump bodies immediately above the plungers. They are mounted in cages which form the guides and seats, and are held closed by

springs, which are retained by nuts on the valve stems. The cage assemblies are held in place by retaining plugs screwed into the pump bodies, and are sealed to the bodies by copper gaskets. The valve lift is determined by the clearance between the top of the cage and bottom of the spring retaining nut, and should be set at 1/16". The valves may be removed by unscrewing the retaining plugs, after first removing top cover (18).

Discharge valves (8) are mounted in cages (9) which are screwed into the tops of the pump bodies. Spherical seats make tight joints between cage & body without gaskets. Flutes on the valve stems work in hardened steel inserts (7) pressed into the cages. The valve lift is limited by retaining plugs which screw into the tops of the cages and secure discharge tees (5). The lift should be 3/32". Spherical surfaces between the tees and the cages and plugs form tight joints without gaskets. Bleeder valves (4) in the tops of the retaining plugs permit venting entrained air from the fuel. The above construction is identical for both pumps, two of the tee outlets being connected together, and the other two leading to the fuel rail and to the accumulator and regulating valve.

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4(10)

Leakage of the suction or discharge valves can usually be stopped by lapping lightly with very fine grinding compound, but if this is not successful new valve and cage assemblies should be installed. If the lower end of the retaining plug above discharge valve (8) shows signs of heavy hammering this is usually due to discharge valve seat (7) being loose in the cage. The cage and seat must then be replaced. Hammering may also be due to insufficient discharge valve lift which should never be less than 1/16".

Priming pump assembly (12) and (13) is threaded into the bottom of the forward pump body directly below the discharge valve. The barrel is screwed into the pump body against a copper gasket and has a packing nut at its lower end. The upper end of the plunger (11) has a valve head which engages a seat in the barrel preventing leakage when the priming pump is not in use. If the pump leaks while the engine is running the valve should be lapped in. If the unit leaks while the fuel system is being primed the packing should be either tightened or replaced. Service work on this pump will be greatly facilitated if the mounting plate (20) is unbolted and the whole fuel pump assembly is removed from the housing.

Fuel leakage from the main pumps and the priming pump collects on top of the center-frame inside the pump housing, and is drained off through a hole in the end of the centerframe. The high pressure fuel pump has been designed to give long trouble-free performance provided that it is given reasonable care. Water, dirt and other impurities in the fuel will materially shorten the life of the plungers and barrels. The normal working pressure is 4000 to 4500 lbs. per square inch but the pump is capable of building up pressures far in excess of this figure. Carelessness in the care of the pressure regulating valve, may cause it to become ineffective, and the resulting high pressure may injure the pump and also damage other parts of the injection system.

2. FUEL RAIL

The fuel rail is located on the operating side of the engine level with the tops of the cylinder heads. One end of the rail is connected directly to the high pressure fuel pump and the other end is connected to the accumulator, pressure relief valve, pressure gauge and back to the high pressure fuel pump. A tee is provided in the pressure gauge line for the pilot house gauge connection.

Isolating valves are built into the fuel rail at the outlets to the spray valves and an additional valve is provided for the purpose of testing the spray valves.

The fuel rail consists of a length of seamless steel tubing inserted in and brazed to the bodies of the isolating valves. The isolating valve stems, which have hardened conical ends, are threaded into the valve bodies. The valve seats are replaceable tobin bronze washers and are held in place by plugs which are screwed into the valve bodies and to which the injection lines from the spray valve are

3. INJECTION TUBING

All of the high pressure lines used in the injection system are seamless steel tubing. The ends are formed by brazing union sleeves to the tubing, and union nuts fasten these ends to the various fittings. Two different sizes of fuel tubes are used in the high pressure system. One size has an outside dia. of 1/4" and .065" wall thickness, and the other size is 3/8" outside dia. and .109" wall thickness. A high grade tubing is used, made especially for this service, and standard seamless steel tubing should never be substituted.

The importance of keeping the injection lines clean cannot be overemphasized. When an injection line is removed from the engine the open ends should be covered with clean paper which should not be removed until the tubing is to be placed on the engine again. If there is any doubt as to the cleanliness of an injection line it should be thoroughly cleaned before installing. To clean a line it should be washed repeatedly in cleaning solvent or gasoline and should be blown out with an air hose between each washing. This cleaning process should be carried on until there is no uncertainty as to the cleanliness of the tubing.

4. ACCUMULATOR

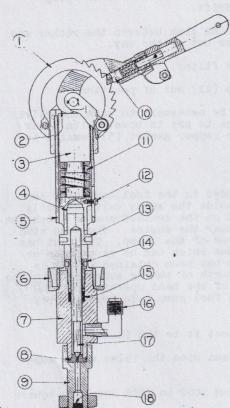
The accumulator is a welded steel bottle mounted on the centerframe, and connected to the fuel rail on certain sizes of engines or to both the rail and high-pressure pumps on other sizes. The function of the accumulator is to prevent large pressure fluctuations in the fuel system due to lowering of the pressure each time a spray valve opens, or to the increasing of pressure on each stroke of the fuel pump plungers. Therefore, due to the compressibility of the fuel oil, the accumulator helps to maintain an even pressure in the fuel system.

On the 13×16 Turbo-charged engine, the fuel rail has been increased considerably in diameter so that it performs the functions of both the rail and accumulator.

5. FUEL PRESSURE REGULATING VALVE

Fuel injection pressure is controlled by the adjustable pressure relief valve. This valve is of the by-pass type in which the opposing forces of a spring and the fuel pressure acting on the stem of a needle valve maintain constant fuel pressures. If the pressure starts to drop the spring closes the needle slightly reducing the amount of fuel by-passed with the result that the pressure is held constant.

Referring to Fig. 0-2 the regulating valve is built around valve body (7). The hardened steel valve seat (8) is held between the body and adapter stud (9) which screws on the bottom of the body, and through passage (18) allows the by-passed fuel to escape. Fuel inlet elbow (16) is threaded into the side of the body, supplying fuel to the annular space around the reduced section of the valve stem (17). The top of the body is bored to receive stem packing (15) and packing gland (14). Screwed to the top of the body is relief valve spring cage (5). This cage is screwed down upon the drain cup holding the latter in place against a shoulder on the body.



Cage (5) carries upper spring seat (3), Spring (11), and the lower spring seat. Valve spring adjusting screw (13) which is bored to receive the upper end of the valve is threaded into the bottom of the lower spring seat. A small machine screw in the lower spring seat engages a slot in the cage and prevents rotation of the seat when the adjusting screw is being turned. The bearing assembly which holds the control handle and sector (1) is threaded to the upper end of cage (5). The lower part of the control handle is shaped to form a cam which actuates the upper spring seat. A spring loaded pawl (10) in the handle engages teeth in sector (1) so that the handle will remain in position after it has been adjusted. A downward force on the end of the handle pulls the pawl away from the sector and allows the handle to be lowered.

The injection pressure is normally changed by moving the handle up or down. Moving the handle in an upward direction increases the pressure, downward movement lowers the pressure. The pressure increase or decrease per notch is approximately 600 to 800 lbs. However, the pressure in any notch may be changed by means of adjusting screw (13).

Packing (15) will need replacing when the fuel leakage around the valve stem (17) becomes excessive. Tighten the packing gland just enough to prevent leakage. Never attempt to stop leakage by tightening the gland severely when new packing is needed. A loss of fuel pressure can often be traced to dirt lodged between valve stem (17) and the seat (8). This condition can be remedied by removing adapter stud (9) and valve seat (8)

from the bottom of the relief valve and thoroughly cleaning the valve and its seat. Occasionally it may be necessary to lap the needle and its seat to prevent excessive by-passing and a low fuel pressure. After performing this operation all

traces of grinding compound should be carefully washed off before the valve is reassembled.

6. SPRAY VALVES

The purpose of the spray valve (or fuel injection valve) is to meter the fuel accurately, to deliver it precisely at a definite moment, in a definite time into the combustion chamber in the form of a finely atomized spray. It might be stated that the successful operation of the engine depends upon the proper functioning of the spray valves more than on any other item. If the engine does not perform properly and the exhaust is smoky, the functioning of the fuel valves should be checked first of all. In the great majority of cases servicing the fuel valves and making them function properly corrects the trouble.

Fundamentally, the spray valve is a heavily spring loaded needle valve. Referring to Fig. 0-3 the seat of the needle valve is incorporated in the tip or nozzle (1) just above the entrances to the spray orifices. The lower end of valve body (4) is counterbored to receive the end of the spray valve tip. A shoulder on the spray tip (1) which is centered in the counterbore, is held securely against the lower end of the body by nut (2). Valve assembly (3) is made up of two sections. The lower section has a conical end which is ground to the seat in the spray valve tip. This lower stem section is pressed into an extension (10) to which the spring loading is applied and by which the stem is lifted. A shoulder on the extension carries a small ball type thrust bearing (14) which acts as a lower spring retainer. Upper spring retainer (12) screws into the upper end of valve spring casing (13) which in turn is threaded to the upper end of valve body (4).

The flange used for clamping the valve is drilled and tapped to receive fuel elbow (6) which supports the small metal edge type filter (15). Fuel is carried from this point to the nozzle in the annular space surrounding stem (3). Leakage upward along the stem is prevented by packing (7) held between an upper and lower gland and secured by packing nut (8).

7. REMOVAL OF SPRAY VALVE FROM ENGINE (See Fig. 0-3)

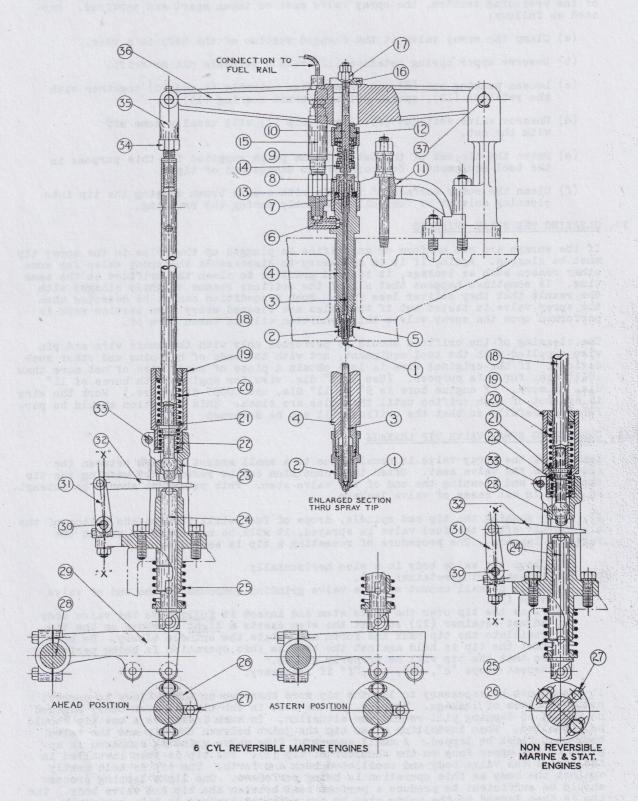
- (a) Remove the cotter pin from one end of pin (37) at the fulcrum end of spray valve rocker (36). Drive the pin out with a brass drift.
- (b) Remove horseshoe shaped collar (16) which forms the link between the rocker and the upper end of the spray valve and swing the rocker out of the way.
- (c) Disconnect the injection line at the spray valve filter.
- (d) Loosen the clamp nut and slide spray valve clamp (ll) out of position.
- (e) Remove the spray valve from the engine. It may be necessary to work the valve loose by rotating it back and forth and in some cases to pry it upward with a bar to remove it. As the valve is removed, note whether copper gasket (5) remains in the cylinder head or on the end of the valve.

8. TEST EQUIPMENT

All the parts for a spray valve test stand are included in the tool equipment supplied with the engine. The spray test clamp which holds the spray valve directly below the flanged section of the body can be mounted on the centerframe or latch box of the engine or at some other convenient location near the engine. The long stud supplied with this equipment screws into the outer end of the clamp. The test handle is supported on the upper end of the stud by a nut which can be screwed up or down on the stud until the desired height of fulcrum has been obtained. Fuel is supplied from the extra fuel rail valve through a length of tubing supplied with the tool equipment. Fuel pressure is obtained by means of the hand operated priming pump located at the forward end of the high pressure fuel pump. To test a spray valve proceed as follows:

- (a) Clamp the spray valve in the test stand and connect it to the fuel rail.
- (b) Close all the isolating valves on the fuel rail and open the valve which supplies the test stand.
- (c) With the priming pump build up a pressure of about 2000 to 4000 lbs. per square inch.
- (d) Open the valve quickly three or four times by hitting the end of the test handle sharp blows with the fist, watching as the valve operates to see if a fine fuel spray comes out of <u>each</u> hole in the tip.

(e) Wipe off the tip carefully, pump up the pressure to about 4000 lbs. per square inch again and operate the spray valve as described in step 4 until the pressure has dropped to about 2000 lbs. per square inch. Then watch the bottom of the tip for a period of time to see if drops of fuel form, indicating tip leakage.





9. DISASSEMBLY OF SPRAY VALVE (See Fig. 0-3)

If the sprays are not uniform, if one or more orifices are entirely plugged up, or if drops of fuel form on the end of the tip after testing as described in step (e) of the preceding section, the spray valve must be taken apart and serviced. Proceed as follows:

- (a) Clamp the spray valve at the flanged section of the body in a vise.
- (b) Unscrew upper spring retainer (12) with a suitable pin or drift.
- (c) Loosen packing nut (8) and remove stem assembly (3 and 10) together with the retainer (12), spring (9) and thrust bearing (14).
- (d) Unscrew valve seat nut (2). Spray tip (1) will usually come off with the nut.
- (e) Drive the tip out of the nut with the punch supplied for this purpose in the tool equipment. Use care not to damage end of tip.
- (f) Clean the outer surface of the tip with a wire brush dipping the tip into cleaning solvent or fuel oil frequently during the brushing.

10. CLEANING THE SPRAY ORIFICES

If the sprays are not uniform or an orifice is plugged up the holes in the spray tip must be cleaned. Again, if it is necessary to disassemble the spray valve for some other reason such as leakage, it is good practice to clean the orifices at the same time. It sometimes happens that all of the orifices become slightly clogged with the result that they deliver less fuel. Such a condition cannot be detected when the spray valve is tested but if the holes are cleaned every time service work is performed upon the spray valves this condition will be taken care of.

The cleaning of the orifices should be performed only with the music wire and pin vise supplied with the tool equipment, not with the ends of hat pins and other such devices. If the original wire is lost obtain a piece of music wire of not more than .011" dia. for this purpose. (Use .011" dia. wire for engines with bores of 11" dia. or more. If engine bore is 9" to 11" dia. use .009" dia. wire.) Work the wire in and out of each orifice until the holes are clean. This operation should be performed consciult so that the orifice will not be deferred. formed carefully so that the orifice will not be deformed.

11. CORRECTING SPRAY VALVE TIP LEAKAGE

Leakage of the spray valve is usually due to a small amount of dirt between the needle and the valve seat. Often this condition can be remedied by washing the tip thoroughly and cleaning the end of the valve stem. This procedure should be attempted first in all cases of valve leakage.

If, after washing the tip and spindle, drops of fuel still form on the bottom of the tip shortly after the fuel valve is sprayed, it will be necessary to reseat the valve by lapping. The procedure of reseating a tip is as follows:

- (a) Clamp the valve body in a vise horizontally.
- (b) Loosen spring retainer (12).
- (c) Apply a small amount of fine valve grinding compound to the end of valve stem (3).
- (d) Place the tip over the valve stem and insert it fully into the valve body.
- (e) Adjust retainer (12) so that the stem exerts a light pressure on the tip. (f) Oscillate the tip back and forth and rotate the spindle slowly. Be sure that the tip is held against the body as this operation is being performed so that the tip will be properly guided.

 (g) Repeat steps "c", "d", and "f" if necessary.

It should not be necessary to lap the tip more than two or three times to correct ordinary cases of leakage. However, if the seat in the tip has been badly damaged no amount of lapping will remedy the situation. In such instances a new tip should be installed. When installing a new tip the joint between the tip and the valve body must first be lapped. A small amount of fine valve grinding compound is applied to the upper face on the shoulder of tip (1). The tip is then installed in the end of the valve body and oscillated back and forth. The tip is held gently against the body as this operation is being performed. One light lapping process should be sufficient to produce a perfect seal between the tip and valve body. The tip is then lapped to the valve stem by the method described in this paragraph.

12. VALVE PACKING ADJUSTMENT

Packing nut (8) should never be appreciably more than finger-tight. A small amount of fuel leakage past the packing is necessary for proper lubrication of the spindle. Too tightly adjusted packing will prevent this lubrication and will result in a scored spindle and sluggish valve action. If a spray valve leaks excessively along the spindle after the packing has been lightly tightened up the need for new packing or a new spindle or both is indicated.

13. ASSEMBLY OF THE SPRAY VALVE - SPRAY VALVE "LIFT"

Referring to Fig. 0-3, spring (9) must be adjusted to a certain tension in order to assure proper functioning of the spray valve. It is further important that the adjustment of all the spray valve springs be the same or that the "lift" on all the spray valves be the same. With "lift" as used in the following instructions is understood the lift which spring (9) will allow before its coils touch each other and prevent further upward movement of the valve stem. (The actual lift when the spray valves are operating in the engine is of course determined by the position of fuel wedge (32), the adjustment on pushrod (18) and cam (27). This actual lift is less than the "lift" as defined in this paragraph.) Proceed as follows to assemble the valve and adjust for proper "Lift" (or opening tension):

(a) Wet spindle (3) with clean fuel oil and slip it into position in the valve body.

(b) Clean the spray valve tip and install it carefully on the valve body. Tighten valve seat nut (2) securely.

(c) Screw down on spring retainer (12) carefully until the coils of spring (9) just touch. Be careful not to screw down so hard that valve stem (3) bends, rendering it useless. It is best to have the valve in the test stand when performing this operation and determine when spring (9) becomes solid by means of the test handle. When it is not possible to lift the spray valve stem by means of the test handle the spring coils are touching. The "Lift" is then zero.

(d) Unscrew spring retainer (12) 3/4 to 7/8 turns which will make the "lift" 1/16". The "lift" on all the valves should be between 1/16" and 5/64".

Screw down on packing nut (8) until it is just finger-tight. (f) Test the functioning of the valve as described in paragraph 8.

14. ASSEMBLY OF SPRAY VALVE IN ENGINE.

The spray valve is installed in the engine in the reverse order of its removal. Again referring to Fig. 0-3, if copper gasket (5) is in the cylinder head merely lower the valve into position. If the copper gasket (5) was removed with the valve, the gasket can be held in position on the lower end of the valve by a thin coating of grease applied to the washer.

After installing the valve it will be necessary to reset the push rod as described in paragraph 18. After timing, in order to clear the cylinder of excess oil, always turn the engine over on air with the snifter valves open and with the fuel isolating valves closed.

15. SPRAY VALVE FUEL FILTERS

In addition to the fuel filter at the high pressure fuel pump an individual filter (15) is supplied at each spray valve. The spray valve filters are of the metal edge type and have a spacing of .0015". They are installed in housing (15) which screw into the fuel inlet elbows at the spray valves. The frequency at which these filters will need cleaning will depend upon the quality of the fuel and the condition of the filter located at the high pressure fuel pump. After disassembling the housings it will be possible to unscrew the filter unit. Wash each unit thoroughly in clean solvent or fuel and blow it clean with compressed air, being careful not to injure the windings when handling it.

16. SPRAY VALVE OPERATING MECHANISM (See Fig. 0-3)

The spray valve is actuated by cam (27), lifter or cam follower (24), pushrod (18), and rocker arm (36). In stationary engines the lifter follows the fuel cam directly. In direct reversible marine engines latch (29) is interposed between the lifter and the cam. Lifter (24) and latch (29) are held against the cam by spring (25).

Motion of the lifter is transmitted to the pushrod through wedge (32). As can readily be seen in Fig. 0-3, moving the wedge inward will decrease the gap between the lifter and the pushrod. Consequently the spray valve will open sooner, will lift higher, and will close later. Moving the wedge outward produces the opposite results. The outer end of the wedge is pinned to lever (31) which is clamped to the wedge shaft, which in turn is connected to the governor. Accordingly the governor, by rotating the wedge shaft, completely controls the action of the spray valves.

When the engine was tested at the factory, wedge levers (31) were adjusted to be parallel to each other and in line on wedge shaft (30) and were then clamped and pinned to the shaft. If new levers or a new wedge shaft are installed it is important that they be lined up in accordance with the above. The position of the fulcrum of wedges (32) for the full load full speed position (wedges fully in) should be about 1/4" inside the vertical line X-X through the center of the wedge shaft. The position of the wedge fulcrum for idling at low speed should be as shown in Fig. 11, that is, about 1/4" outside line X-X. In other words, line X-X should approximately divide the total movement of the wedge fulcrum in two equal parts.

Levers (36) should be approximately horizontal and should be approximately parallel for all the spray valves. This is accomplished by means of adjusting nut (17) which bears down on horseshoe collar (16) which in turn bears down on lever (36). With the lever disconnected from push rod fork (35) hold it up against collar (16) and nut (17) without opening the spray valve. Then adjust nut (17) for the proper lever position and lock by means of the lock nut on top.

Buffer spring assembly (19), positions the pushrod relative to the lifter and assists spray valve spring (9) in returning the valve mechanism (rocker, pushrod, etc.) as the spray valve is being closed. The weak spring (22) below buffer spring (20) merely holds the pushrod against washer (21). As buffer spring assembly (19) is screwed down buffer spring (20) and washer (21) force the pushrod downward against the weaker spring and bring the end of the pushrod closer to the wedge and lifter. Proper adjustment of the buffer spring assembly is as follows:

- (a) Bar the engine until the fuel cam follower is on the base circle of the cam.
- (b) Set the wedge shaft and wedges in <u>full load position</u> (wedges "fully in" as determined by the governor weights being fully in) and unscrew cage (19) until there is clearance between the lower end of the pushrod and the upper face of the wedge.
- (c) Slowly screw down cage (19) and at the same time move the wedge back and forth sideways with fingers.
- (d) As soon as the wedge is felt to tighten unscrew the cage one-half turn and lock it in this position with the clamping screw.

NOTE: When timing the spray valves as described in the following the buffer spring assembly should always be unscrewed about one or two turns. When timing is completed adjust the buffer spring in accordance with instructions in this paragraph.

17. SPRAY VALVE TIMING (See Fig. 0-3)

The timing procedure described in the following is for a spray valve opening of 8° B.T.C. (Before Top Center) and a spray valve closing of 18° A.T.C. (After Top Center). The proper spray valve timing to use is stamped in the engine name plate and should always be followed. If the timing in the name plate differs from 8° - 18° opening and closing the following instructions should be modified accordingly. Proceed as follows:

- (a) Turn the latch shaft to the AHEAD position and unscrew all Buffer Spring Cages one or two turns. Shut off all the isolating valves in the fuel rail except for Number 1 cylinder.
- (b) Be sure that wedges are in the full load position ("fully in") as determined by the governor weights being against their inner stops. (Normally the wedges will be "fully in" when the engine is shut down but it is well to check this point.)
- (c) Spot Number 1 cylinder at 5° A.T.C. on the power stroke. (Half way point between 8° B.T.C. opening point and 18° A.T.C. closing point). Then unbolt and turn the fuel cam until the center of the toe is directly in line with the axis of the lifter. Clamp the fuel cam temporarily.
- (d) Set the crankshaft 8° B.T.C. on the compression stroke. Bar the engine up to this point in the ahead direction of rotation.
- (e) Pump up a fuel pressure of about 1500 lbs. per sq. inch with the hand pump.
- (f) Slowly lengthen the spray valve pushrod until the needle of the pressure

gauge drops indicating that the spray valve has opened. Check this adjustment by backing the engine up a few degrees, pumping the fuel pressure up again and barring the engine slowly in the ahead direction until the pressure again drops. If the flywheel pointer is not at 8° B.T.C. readjust the pushrod and check again.

To adjust the length of pushrod (18) loosen locknut (34) and turn the pushrod, using a pin or drift in the holes provided at its upper end. Then tighten the locknut.

If the push-rods use the ball and socket connection to the rocker, then loosen the clamp screw in the rocker and screw the ball stud up or down until the proper adjustment is reached. Be sure that the clamp screw is tightened after the ball stud is adjusted.

- (g) Bar the engine over to 25° A.T.C. and again pump up the fuel pressure. Then bar the engine backwards slowly until the pressure drops. This point, which is the closing of the spray valve, should be 18° A.T.C.
- (h) If this point is past 18° A.T.C. too long a spray period is at hand. It will be necessary to advance the fuel cam slightly and repeat steps "d", "e", "f", and "g". If on the other hand the spray valve closes before 18° A.T.C., retard the cam slightly and repeat steps "d", "e", "f", and "g".
- (1) Repeat steps "c" to "g" on the remaining cylinders. Check and record the spray valve timings for ASTERN. The timing going Astern may be slightly different than the ahead timing. However, the ahead timing is the more important and no changes should be made to favor the astern timing.
- (j) Adjust the buffer springs as per instructions in paragraph 16. Note that buffer spring cages should always be unscrewed when spray valves are timed.

18. BALANCING THE ENGINE FOR EQUAL LOAD ON ALL CYLINDERS

Theoretically, if the spray valves have been timed exactly and correctly (as outlined in the preceding paragraph) the amount of fuel injected in each cylinder should be the same. Consequently, the total engine load should also be equally divided between all the cylinders. Practically however, it is impossible to time all the spray valves exactly alike, and even if that could be accomplished manufacturing tolerances on such items as orifices in the spray valve tips, fuel cams, wedges, etc. are apt to affect the cylinder balance. The division of load between the various cylinders should consequently be checked after the engine is running, preferably at full load. Since the exhaust temperatures are proportional to the loads that the various cylinders are carrying the amount of fuel injected should be adjusted so that the exhaust temperatures for the various cylinders are alike, or nearly alike.

The amount of fuel injected and consequently the load carrying capacity of a cylinder may be changed by adjusting the length of pushrod (18). It should be noted, however, that readjusting the pushrod length will affect the spray valve timing. Therefore, this adjustment should not be appreciable and should not exceed one-half turn of the pushrod or ball stud from the position obtained when timing the spray valve.

The proper procedure for balancing the engine can be summarized as follows:

- (a) Assuming that all the spray valves have been correctly timed it should be possible to balance the engine by merely lengthening or shortening the pushrods by one-half turn or less. Lengthening a pushrod will increase the exhaust temperature of the cylinder and vice versa.
- (b) If a pushrod adjustment of one-half turn is not sufficient, the timing of all the spray valves should be checked and, if necessary, readjusted to the proper timing as indicated on the engine name plate.
- (c) If the valve timing is found to be satisfactory or if, after making any necessary correction in the spray valve timing, a correction of one-half turn of the pushrod is still insufficient, defective combustion is indicated. This may be due to one or more spray tip orifices being plugged or to any of the defects dealt with under the heading "Smoky Exhaust" in the "Maintenance and Inspection" section.

When the engine was tested at the factory spray valves were carefully timed and adjusted to equalize the exhaust temperatures in the various cylinders and while the operator should not continually change adjustments in an effort to improve an engine that is operating satisfactorily he should keep the balance of the various cylinders fairly even. The cylinder balance should be checked whenever a spray valve has been changed. If the exhaust temperatures are kept within a total range of 20° the balance will be excellent, while a range of 50° may not be considered excessive and will give fairly satisfactory operation. However, do not allow the cylinder unbalance to exceed the last mentioned value.

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CONTROL SYSTEM

The Control System includes all of the parts necessary for reversing the engine and operating it in the desired direction of rotation, starting and stopping the engine, and controlling its speed of rotation. According to the specific functions of the component parts, it may be subdivided as follows:

The Reversing Mechanism consisting of the Latches, Latch Shaft, Control Wheel and the interconnecting gearing between this control wheel and latch shaft.

The Starting Mechanism which consists of the individual starting air valves in each cylinder head (described in detail in Section H), the Master Starting Air Valve in the starting air manifold, and the Pilot Valve for operating the master valve. In some engine models, as described later, the pilot valve actuates an Air Ram which in turn operates the air starting valves in the cylinder heads and the master valve.

The Fuel Cut-Out Mechanism which operates to stop the engine by taking the wedge shaft out of control of the governor, rotating it to pull out the fuel wedges thereby cutting off the fuel to the engine.

The Flywheel Air Brake which assists in stopping the engine between reversals and is therefore closely related to the reversing mechanism. It is also controlled by a pilot valve.

The Governor which maintains the desired speed of rotation and the Speed Control Lever (or Throttle Lever) by means of which this speed may be changed.

1. LATCHES AND LATCH SHAFT

For a given direction of rotation all the valves must be actuated in a definite sequence and with a definite timing. For direct reversible engines it is consequently necessary to provide dual sets of cams, one set for operation in the AHEAD direction of rotation, the other set for operation when running ASTERN. At the same time means must be provided for throwing one set of cams into operation, while at the same time the other set must be made inoperative.

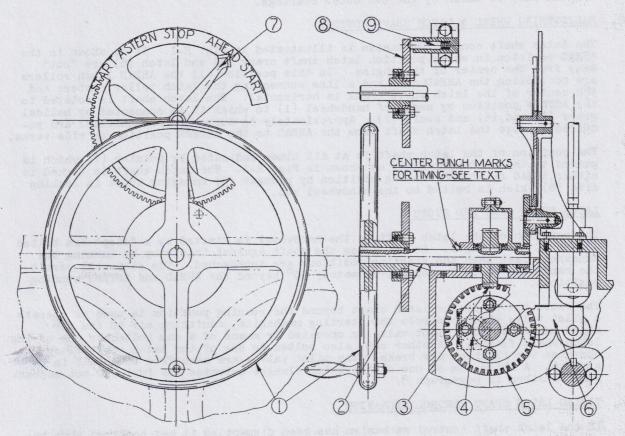


FIG. R-1

In Atlas engines the AHEAD and ASTERN cams are mounted side by side on the camshaft. Referring to Fig. R-1 it will be noted that latches equipped with two rollers are interposed between the cams and the valve lifter rollers. The two latch rollers are offset and lined up relative to the cams in such a manner that in the AHEAD position of the latches one set of rollers contact the AHEAD cams while at the same time the other set of rollers are free of the ASTERN cams. (Astern cam not shown in Fig. R-1) Thus in the position shown in Fig. R-1 the AHEAD cams actuate the latches which in turn actuate the valves by means of the lifters, pushrods and rockers.

By rotating the latch shaft 180° the latch fulcrum points are moved inward (toward the center of the engine) to a point where the ASTERN cams contact the other set of latch rollers. This inward movement frees the AHEAD latch rollers of the AHEAD cams and consequently the ASTERN cams now control the actuation of the valves.

The fuel valve timing is very nearly the same for both directions of rotation. For example, in one direction of rotation the fuel valve may open 8° before top center and close 18° after top center. Then if the rotation was reversed and the latch kept in the same position the fuel valve would open 18° before top center and close 8° after top center. In other words, the timing would be 10° early. It is possible to compensate for this slight difference in timing by properly positioning the ASTERN roller on the fuel valve latch. Consequently only one fuel cam is provided which serves for both AHEAD and ASTERN running and the fuel latch rollers are in line, not offset as on the other latches.

The case hardened steel latch rollers turn on steel pins carried in the bodies of the latches and riveted in place. In the inlet, exhaust and starting air latches, spacers between the walls of the latches and the sides of the rollers establish the positions of the rollers in line with the cams. The fuel valve latch does not require any spacers since only one cam is used and both rollers are in line. The rollers all have a clearance of .001" to .002" on the pins and a side clearance of 1/64".

The latch shaft is built up of six sections, each section comprising the crankshaft for the four latches of a single cylinder. The shaft is mounted on cast iron bearings which are bolted to the side of the centerframe. Journals are turned on the shaft at each end of each crank, and flanges at the ends of each section provide means of bolting the sections together. Bearing clearance is .001" to .0025" and end play is taken by the two outer bearings.

2. MANEUVERING WHEEL & LATCH SHAFT CONTROL

The latch shaft control mechanism is illustrated in Fig. R-1. It is shown in the AHEAD position in which position latch shaft crank (4) and latch (6) are "out" away from the center of the engine. In this position all the AHEAD latch rollers are contacting the AHEAD cams and a line connecting the latch roller centers and the center of the latch shaft crank is horizontal. The latch shaft is rotated to the ASTERN position by means of handwheel (1) to which it is connected by helical gears (3) and (5) and shaft (2). Approximately $3\frac{1}{2}$ turns of the handwheel are required to move the latch shaft from the AHEAD to the ASTERN position or vice versa.

The position of the latch shaft is at all times indicated by pointer (7) which is geared to the handwheel shaft as shown in Fig. R-1. The latch shaft is locked in either AHEAD or ASTERN running position by plunger (9) engaging holes in locking disc (8) which is bolted to the handwheel hub.

3. LATCH SHAFT CAMS AND STOPS

The rotation of the latch shaft by the handwheel is limited by a "stop" cam bolted to one of the flanges. Do not force the shaft against this stop by turning the handwheel fast when the starting positions are approached. The stop will permit the handwheel to be turned approximately 90° beyond the AHEAD and ASTERN running positions.

The extra travel of the latch shart beyond the running position is used to operate a pilot valve which controls the starting mechanism, admitting air to the air start manifold. The pilot valve is operated by means of a cam bolted to one of the latch shaft flanges. Another cam, also bolted to one of the latch shaft flanges operates the flywheel air brake. The pilot valves are described in detail in paragraph 6. A third cam on one of the latch flanges actuates the fuel cut-out mechanism described in paragraph 8.

4. TIMING LATCH SHAFT CONTROL MECHANISM

If the latch shaft control mechanism has been dismantled it may be timed when reassembling as follows. Place the latch shaft in AHEAD position (crank out). A

pointer is mounted on one of the latch shaft bearings for this purpose, and the shaft should be spotted so that the line scribed on the corresponding shaft flange exactly registers with this pointer. Then, with the handwheel in the AHEAD position, as indicated by the register of center punch marks on the handwheel shaft and the end of the bearing housing (See Fig. R-1) mesh helical gears (4) & (5). NOTE: Before dismantling the handwheel assembly observe whether or not these parts have been marked. If not, mark them as indicated, with the latch shaft in the AHEAD running position. The handwheel and gear assembly may then be bolted in place and the indicator assembled, meshing the gears with the pointer midway between AHEAD and START.

5. STARTING MECHANISM - ENGINES WITH 13" BORE

The starting mechanism used on engines with 13" bore differs from that used on engines with smaller bore and the two systems will be described separately.

Fig. R-2 illustrates the master starting air manifold valve. It is pneumatically operated by means of a pilot valve located on top of the latch box. (Pilot valve described in Paragraph 6). The pilot valve is connected by means of tube (7) and for the position of the master valve shown in Fig. R-2 the pilot valve is venting tube (7) and the space above plunger (1) to atmosphere. Consequently spring (4) will hold plunger (1) against its upper stop and in this position the reduced diameter at the middle of the plunger will form a passage through which tube (8) and the starting air manifold is vented to atmosphere. Valve (5) is held closed against its seat by spring (11) and also by the air pressure in chamber (6) which is connected to the air tank.

When the engine is to be started the pilot valve is opened by the cam on the latch shaft as described in paragraph 6, admitting air through tube (7) to the top of plunger (1). The plunger is thus forced down, closing the starting air manifold vent passage and opening the main operating valve (5). As this valve is opened starting air is admitted to manifold (12), leading to the indidual starting air valves in the cylinder heads. By-pass valve (10), which is first opened by plunger (1) and pin (4) admits air pressure to chamber (9) above the main operating valve, balancing the air forces acting thereon and permitting it to open under the downward force of plunger (1).

For the operation of the air start valves in the cylinder head refer to Section H.

6. PILOT VALVES

All the pilot valves for operation of the starting air valve, flywheel brake, etc. are identical and are illustrated in Fig. R-3. They are mounted on top of the latch box between cylinders No. 5 & 6. The operation of all valves is exactly the same, their function being to control the supply of air to the device to which they are connected.

Two valves are provided, pilot valve (3) and vent valve (4). The housing is provided with three pipe tapped connections. Hole (2) is connected to the source of air supply, (1) to the device to be operated, and (9), the vent, is open to the atmosphere.

The valve as shown in Fig. R-3 is in the normal position assumed when the engine is running. Plunger (7) is then held down

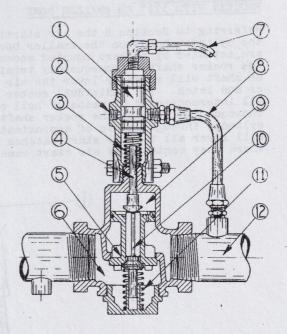
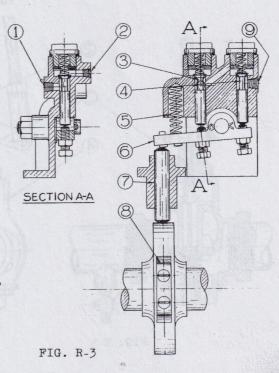


FIG. R-2



against the latch shaft flange by spring (5) acting on rocker (6). The vent valve is open and the pilot valve is closed under the action of the spring. Connection (1), to which the device to be operated is connected is thus vented through the diagonal hole connecting the two valves.

When the latch shaft is rotated so that cam (8) contacts plunger (7) it raises rocker (6) closing the vent valve and opening the pilot valve, admitting air to the device to which the valve is connected. The adjusting screws in the rocker should be set to allow approximately 1/16" clearance between the ends of the screws and the ends of the valve stems when the valves are seated.

7. STARTING MECHANISM ENGINES WITH 112 OR SMALLER BORE

Referring to Section H the air starting valves in the cylinder heads on the smaller bore engines are actuated by rockers mounted eccentrically on the rocker shaft. Consequently turning the rocker shaft will raise or lower the air start lifter and latch. The individual rocker shafts are all interconnected by means of bell cranks and consequently turning the rocker shaft on No. 1 cylinder through an arc of approximately 110° will lower all the air start latches to a point where they contact the air start cams, throwing

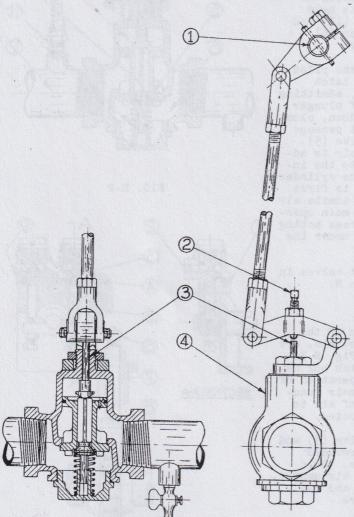


FIG. R-5

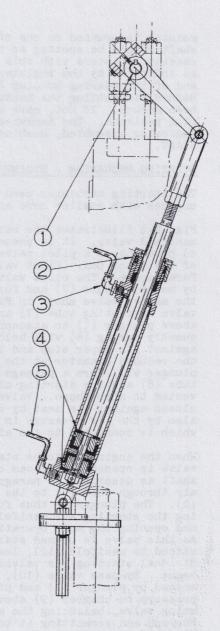


FIG. R-4

the starting air valves into operation.

The rocker shaft is shifted from one position to the other by means of a pneumatic cylinder mounted forward of cylinder No. 1 and illustrated in Fig. R-4. The pilot valve controlling this cylinder and the manner in which it is operated from the latch shaft are identical with the pilot valve, described in Paragraph 6. As shown in Fig. R-4, it is in the inoperative position, with the plunger down. Air pressure admitted above the piston through connection (3), which is permanently connected to the source of air supply normally holds it in this position. The pilot valve is piped to connection (5), and when in the RUN position vents the

lower end of the cylinder. When the latch shaft is shifted to the START position the pilot valve opens, admitting air below the piston. Since the area below the piston is considerably larger than that above the piston it is forced up, shifting rocker shaft (1) to the START position. As soon as the pilot valve closes the space below the piston is vented and the air pressure above immediately returns the piston to the RUN position.

The travel of the piston is limited by contact of thrust washers (4) with the upper and lower heads of the cylinder and the stroke is 9-5/8" for the $ll\frac{1}{2}$ " bore engine and $7\frac{1}{2}$ " for engines with 10" or $10\frac{1}{2}$ " bore. Packing gland (2) should be kept sufficiently tight to prevent air leakage, but should not be tightened more than necessary.

The position of the rocker shaft relative to the air ram can be adjusted by means of the threaded end of the air ram piston, turning it in the clevis connecting to the rocker shaft lever. The rocker shaft position should be adjusted so that the bell cranks connecting the various rocker shafts point straight up when air ram piston is in the RUN position.

The master starting air manifold valve used on the smaller bore engines is illustrated in Fig. R-5. Valve (4) is essentially the same as that used on the 13" bore engines and described in Paragraph 5. It is mechanically operated however, by linkage connecting to the valve rocker shaft (1), this linkage replacing the pneumatic piston construction used on the 13" bore engines. When the rocker shaft shifts to the "START" position, adjusting screw (2) contacts pin (3) and opens the valve. Screw (2) should be set so that the valve is opened about ½" when the rocker shaft is in the "START" position.

8. FUEL CUT-OUT MECHANISM

The fuel cut-out plunger is illustrated in Fig. R-6. As shown in Fig. R-6 the latch shaft is in or near the "STOP" position, with plunger (3) up on cam (4), which is mounted on one of the latch shaft webs. The upper end of the plunger has engaged the adjusting screw in lever (1), rotating the lever and the fuel wedge shaft (2) to pull out the fuel wedges and cut off fuel from the engine. The adjusting screw in lever (1) should be set to allow 1/8" clearance with the top of the plunger when the latter is down off the cam and the fuel wedges are in at the full load position.

9. FLYWHEEL BRAKE

The flywheel brake assembly is shown in Fig. R-7. Brake shoe (1) which is faced with brake lining, is carried by the horizontal arm of crank shaped lever (2). This lever is mounted on shaft (3), and carries the brake cylinder (4) in trunnions on its vertical arm. Shaft (3 is supported by bracket (5) which is bolted to the after end of the centerframe. The projecting end of the piston rod (6) bears against the compressor cylinder and therefore the piston and rod remain stationary when air is admitted to the cylinder. When the pilot valve is opened and air is admitted to the brake, the cylinder moves relative to the piston. Lever (2) is rotated about its fulcrum, applying the brake to the flywheel and stopping the engine. When the air pressure is relieved the brake shoe is withdrawn from the flywheel by spring (7), which bears against a third arm on lever (2).

There are no adjustments necessary on the brake and the only service requirements are the replacement of the shoe lining and the piston cup leather when necessary.

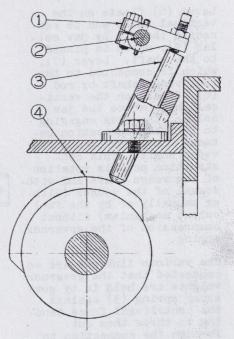


FIG. R-6

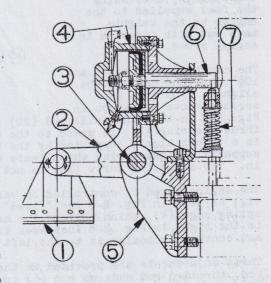


FIG. R-7

10. GOVERNOR AND SPEED CONTROL

The flyball type governor, mounted near the bottom of the forward end of the latch box and driven from the camshaft gear, is shown in Fig. R-8. Cast iron bearing (20) is adjusted and doweled to the latch box to allow .004" to .005" backlash between governor gear (19) which is pressed and keyed to the governor body, and the camshaft gear. Running clearance between governor body (21) and the bearing is .0015" to .0025" and lubrication is from a catch basin (11) in the top of the bearing. Basin (11) can be filled from an oil cup in the side of the latch box.

Governor weights (18) mounted or pins in the governor body, carry rollers (14) on riveted pins. As the flyballs tend to move out due to centrifugal force the rollers exert a force against quill rod (22) acting through plate (16) and ball bearing (17). The plate, which is loosely riveted to the rod cap to maintain the assembly when dismantling, rotates with the balls while the rod and cap remain stationary. The thrust reaction is taken by ball bearing (23) and retaining collar (24), which is secured to the governor body by two taper pins. The flyball thrust from the quill rod is transmitted, by means of forked lever (25), vertical shaft (10), lever (8) and rod (5) to governor spring (3).

Lever (8) floats on the vertical shaft and is connected thereto by jaw collar (9), which is pinned to the shaft. Lever (7) which is connected to the fuel wedge shaft by rod (6), floats on the vertical shaft above the jaw collar, the jaws engaging to form the connection between the governor and the wedge shaft. This construction permits rotation of the wedge shaft and withdrawal of the wedges (either manually or by the fuel cutout mechanism) without compression of the governor spring.

The various linkages are so connected that the governor weights are held in by governor spring (3) against the centrifugal force tending to throw them out. Through the connection to the fuel wedge shaft the wedges follow the motion of the weights, decreasing the fuel supplied to the engine as the weights move out with increase in engine speed.

The construction on 10" and 10½" bore engines differs slightly from that described above and shown in

FIG. R-8

Fig. R-8 in that the quill rod (22) rotates with the governor body and flyballs.

Thrust bearing (17) is moved to the outer end of the quill rod, where it is mounted in a thrust block, supported by the fork lever. A cover plate excludes dirt and supports a light spring which bears against the thrust block, holding the weights in. The adjusting screw (13) is not used in this construction.

The engine speed is controlled by varying the tension of governor spring (3). As will be seen in Fig. R-8 the "fixed" end of the governor spring is supported by spring cage (4), which follows the motion of control lever (1). Moving the lever to the right in Fig. R-8 increases the spring tension and hence the engine speed and conversely moving it to the left decreases the engine speed.

Three adjustments are provided in the governor linkage, setscrew (13) on the quill rod, threaded rod ends on rod (6) connecting to the wedge shaft, and adjusting nut (2), with its locknut, on the end of governor spring rod (5). Nut (2) controls the engine speed, and should be set to give the desired full load speed with the control handle in the last notch to the right. (NOTE: When the engine is idling

these nuts project beyond the spring cage and are accessible for adjustment.) This is the only adjustment with which the operator need normally be concerned. The others were set at the factory and should require no attention, unless parts are replaced. In such cases the rod ends on rod (6) should be set so that lever (7) is parallel with the renterline of the engine when the fuel wedge levers are vertical. Adjusting screw (3) should then be set to place the fuel wedges in the full load position when the engine is shut down, and the governor weights are fully in (See Section 0). Speed adjustment at full load should then be made as above.

11. MANEUVERING THE ENGINE

In the following the sequence of events as they take place when reversing the engine from AHEAD to ASTERN are described. Assuming that the engine is running the indicator pointer (See Fig. R-1) is in front of AHEAD and locking pin is registering with the hole in the locking disc. The handwheel is then turned in a direction to move the pointer toward "STOP" and when the wheel has been rotated approximately 90° the fuel cutout mechanism (See Paragraph 8) operates to pull out the fuel wedges and the engine begins to slow down. When the handwheel has been turned approximately one revolution from the "AHEAD" position the air brake pilot valve opens applying the brake and stopping the engine. When the indicator pointer reaches "STOP" the operator should hold the handwheel in this position until the engine has come to a full stop. Further rotation of the hand-wheel closes the air brake pilot valve and allows the fuel cutout mechanism to release the wedge shaft. After approximately $3\frac{1}{2}$ turns of the handwheel the latch shaft is in the ASTERN position and indicator pointer in front of ASTERN.

The handwheel can still be moved an additional 80 to 90° before the latch shaft comes up against its stop. This additional movement operates the pilot valve for the starting mechanism (See Paragraphs 5 and 7) and the engine begins to turn over on air. Almost immediately it begins to fire and the handwheel should then be turned back to bring the latch shaft in the ASTERN position which is reached when locking plunger (9) (See Fig. R-1) enters the hole in the locking disc. The engine will then be under governor control, its speed being determined by the setting of the speed control lever and fuel pressure regulating valve lever.

Maneuvering from full speed AHEAD to full speed ASTERN may be accomplished in approximately 10 seconds. Although not absolutely necessary it is advisable to slow the engine down to say 1/2 or 3/4 speed by means of the speed control lever before maneuvering. Maneuvering operations will also be smoother if the fuel pressure is lowered somewhat by means of the fuel pressure regulating valve. About 2500 to 3000 lbs. per square inch fuel pressure is suitable for maneuvering.

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CONTROL SYSTEM

The Control System includes all of the parts necessary for reversing the engine and operating it in the desired direction of rotation, starting and stopping the engine, and controlling its speed of rotation. According to the specific functions of the component parts, it may be subdivided as follows:

The Control Mechanism consisting of the Control Lever, mounted on the Control Unit, which is mechanically connected to the Pilot Valves and to the Governor and Fuel Cut-Out mechanisms. The functioning of all the various parts of the Control System is governed by the Control Lever either by means of mechanical connections or by means of pneumatic connections to the Pilot Valves.

The Reversing Mechanism consisting of the <u>Latch Shaft</u> and <u>Latch Mechanism</u> operated by the <u>Air Ram</u> and <u>Reversing Rack</u> which are mechanically connected to the <u>Latch Shaft</u>. The Reversing Rack is locked in the proper position by the <u>Interlocking Mechanism</u>. The position and movement of the Air Ram is controlled by two Air Ram Pilot Valves located in the Control Unit.

The Fuel Cut Out Mechanism in the Control Unit which serves to stop the engine by rotating the wedge shaft, thereby pulling out the fuel wedges and cutting off fuel from the engine.

The Governor which maintains the desired speed of rotation and the mechanical connections to the Control Lever by means of which this speed is changed.

The Starting Mechanism which consists of the individual starting air valves in each cylinder head (described in detail in Section H), the <u>Master Starting Air Valve</u> in the starting air manifold, and the <u>Pilot Valve</u> (in the Control Unit) for operating the master valve.

The Flywheel Air Brake which assists in stopping the engine between reversals and is therefore closely related to the reversing mechanism. It is also controlled by a pilot valve in the Control Unit.

The Cylinder Compression Relief Valves which serve the purpose of relieving the cylinder compression in the event that the engine becomes air locked. Since their operation is desired at the same period in the maneuvering cycle as that of the flywheel brake, they are connected to the Brake Pilot Valve in the Control Unit.

1. CONTROL LEVER, CONTROL UNIT & PILOT VALVES

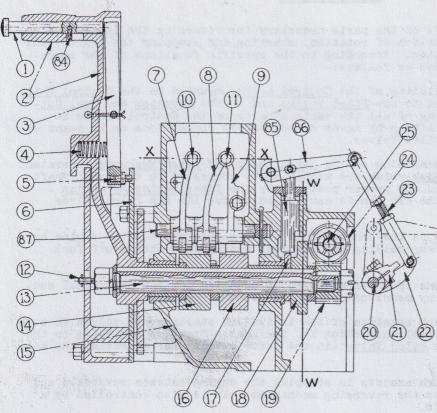
The engine is started, stopped and reversed, and the speed controlled by means of a single control lever located on the centerline of cylinder No. 2. The only other control lever provided is on the fuel pressure regulating valve which governs the fuel injection pressure. This lever is located close to the engine control lever for convenience in operation, so that both levers can be reached from the control station.

The control unit, shown in Fig. R-1, contains four pilot valves, two for operating the air ram, one for the flywheel brake and compression relief valves, and one for the starting air valve. These pilot valves are all actuated by the control lever, which is also mechanically connected to the latch shaft interlock, the governor spring for the governor control, and the fuel wedge shaft for the fuel cutout. Thus the engine is entirely controlled by the one control lever.

NOTE: IT IS OF UTMOST IMPORTANCE THAT DIRT, SCALE AND CHIPS BE KEPT OUT OF THE CONTROL UNIT PILOT VALVE HOUSINGS. CLEAN OUT ALL STARTING AIR PIPING BEFORE INSTALLING.

2. PILOT VALVE LEVERS & CAMS

Referring to Fig. R-1 control lever (2), which is keyed to shaft (13), is held in position by latch pin (5) engaging holes in latch plate (6). It may be released for maneuvering by pressure of the thumb on latch button (1) or it may be permanently unlocked to permit control from the pilot house by depressing and rotating the latch button. When a pilot house control is provided, a chain from the pilot house control stand engages a sprocket which is mounted on the hub of the control lever and transmits motion from the pilot house control stand to the engine control. Control shaft (13), which rotates in bronze bushings in housing (15), carries hubs (14) and (16) for the pilot valve cams, cam (18) for the governor spring control, cam (17) for the fuel cutout and gear (19) for the latch shaft interlock connections. All of these units are keyed and clamped to the shaft, which is drilled for



SECTION THRU CONTROL UNIT

FIG. R-1

each side, which are engaged by the two faces of a cam on hub (14). The right hand side of the cam engages for AHEAD and the left hand side for ASTERN on a right hand engine. When the control lever is in the vertical, or STOP position, lever (7) is also vertical, held in this position by a spring and both rollers are free of the cam. When the control lever is moved in the ahead direction (clockwise on a right hand and counterclockwise on a left hand engine) the lead-cam face contacts its mating roller and turns lever (7) in the opposite direction, thereby opening the ahead

lubrication and provided with a grease plug on

Referring to Figs. R-1 and R-2, the pilot valves are actuated from the cams on the control shaft by means of levers (7), (8), and (9) which are mounted in

the control unit on fulcrum shaft (87). Lever (7) controlling both pilot valves for the air ram. has two rollers, one on

pilot valve for the air ram. Thus the ahead pilot

the outer end.

valve, that is the valve to shift the latch shaft to the AHEAD position, is on the after side of the control housing and the astern valve is on the forward side. The lever rollers are so located with respect to the cam nose that the pilot valves open, admitting air to the air ram cylinder, when the control lever is turned 14° from the vertical, either AHEAD or ASTERN. As the handle is further rotated to approximately 59° from the vertical, the end of the nose or dwell period of the cam is reached and the roller drops down off the nose, allowing the valve to close and relieving the air pressure in the ram cylinder. The action is reversed as the control lever is moved toward the STOP position from either AHEAD or ASTERN running positions, the pilot valve being opened and air admitted to the ram cylinder as the lever reaches a point 59° from STOP. As it further approaches STOP the valve is closed and the ram cylinder again relieved when the lever reaches a point 14° from STOP.

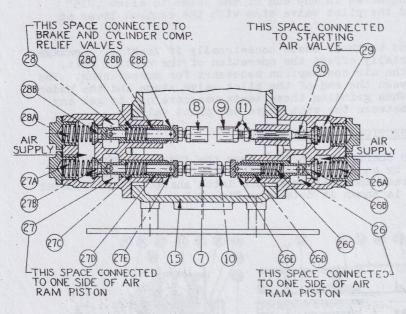
Lever (8) operates the pilot valve controlling the flywheel brake and compression relief valves. It has only one roller, so located with respect to the car that when the lever is in the STOP position it is up on the cam nose. The lever is then displaced and the pilot valve is open, admitting air to the brake cylinder and compression relief manifold. As the control lever is moved 140 in either direction the roller drops down to the cam base circle, allowing the pilot valve to close, thus relieving the brake cylinder and compression relief manifold. This action is reversed as the lever is moved toward the STOP position from either AHEAD or ASTERN running positions, applying the brake and opening the compression relief valves as the control lever reaches a point 14° from STOP. The operating cam toe is carried by hub (14).

Lever (9) operates the starting air pilot valve. Since it is not permissible to have this valve open during the stopping portion of the maneuvering cycle, that is when the control handle is moved to STOP from either AHEAD or ASTERN running positions, lever (9) is provided with pawls, one for AHEAD and one for ASTERN, which engage corresponding cam toes carried in hub (16). As the control handle is moved to a point 32° from STOP in either the AHEAD or ASTERN directions one of the cam toes engages and lifts its mating pawl, rotating lever (9) in a clockwise direction and opening the starting air pilot valve. As the motion of the control lever continues to a point 50° from STOP the end of the cam toe is reached and the pawl drops off the cam, allowing lever (9) to return and the pilot valve to close. On

the return stroke of the control lever, that is when it is moved toward STOP position from either AHEAD or ASTERN running positions, the pawl rotates on its fulcrum pin in lever (9) when it is contacted by the cam toe, allowing the cam to slip under it without moving lever (9) and opening the pilot valve. The pawls are held in position against stop pins in lever (9) by light tension springs, anchored to pins in the side of control housing (15). The mechanism is accessible through the inspection hole on the left hand side of the control housing.

3. AIR RAM PILOT VALVES

Fig. R-2 showing Section X-X in Fig. R-1, is a horizontal section through the pilot valves. Valves (26B) and (27B) are the air ram control valves, (27B) AHEAD and (26B) ASTERN in a right hand engine. The air ram is essentially a double acting piston and rod, the latter being connected through gearing to the latch shaft. The piston is actuated by compressed air at 125 to 200 lbs. pressure and, for the operation of the ram, it is essential that the pressure and relief on the two sides of the piston be under accurate control. This control is by means of the pilot valves (26B) and (27B) actuated by the control lever through the cam and lever (7) as previously described. The valves are identical on each side, and the operation is the same whether AHEAD or ASTERN. Referring to Fig. R-2 the outer chambers are connected to the air supply and the inner chambers (26) and (27) are connected to the two sides of the air ram cylinder. Fig. R-2 shows the mechanism with the control lever at STOP and lever (7) vertical. In this position the pilot valves (26B) and (27B) are both held closed by their spring (26A) and (27A) and vent valves (26D) and (27D) are held out against adjusting screws (10) in lever (7) by their springs (26C) and (27C). Both sides of



the air ram piston are therefore vented into the control housing through the drilled holes in the pilot and vent valves. As the control handle is moved AHEAD lever (7) is moved to the left as seen in Fig. R-2 (for a right hand engine) and vent valve (27D) slides into pilot valve (27B) collapsing spring (27C) until its head engages the end of the pilot valve and seals vent holes (27E). Further motion of lever (7) lifts valve (27B) off its seat, collapsing spring (27A) and admitting air to chamber (27) and so to the AHEAD side of the air ram piston. During this action vent valve (26E) on the opposite side is pushed out by spring (260) and follows the motion of lever (7). The vent passage through the drilled holes in the valves thus remains open, venting chamber (26), and allowing the air ahead of the piston to escape as the

piston is moved to the AHEAD position by the compressed air admitted through valve (27B).

The action for ASTERN is exactly opposite to that described above. The total motion of lever (7) each side of center is 3/8", 7/32" of which is utilized in closing the vent valves and 5/32" in opening the pilot valves. Adjusting screws (10) in lever (7) should be set so that the distance between the head of the vent valves and the end of the pilot valves is 7/32" on each side when the control lever is at STOP and lever (7) is vertical, with clearance between cam faces and rollers equal on each side.

4. FLYWHEEL BRAKE & COMPRESSION RELIEF PILOT VALVES

The flywheel brake is actuated by a single acting air piston and is released by a spring. Only one pilot valve is therefore necessary for its control. This valve, (28B) in Fig. R-2, is identical with the pilot valves for the air ram and its action in admitting air to and venting the cylinder is exactly the same. The valve is operated by lever (8) as previously described, and the adjusting screw in the lever should be set the same as the ones for the air ram pilot valves, that is to allow 7/32" opening of the vent valve when the lever roller is on the cam base circle.



The compression relief valves are also actuated by single acting air pistons with spring return, and are therefore operated by the same type of control valve. Since their operation is desired at the same time in the maneuvering cycle as the flywheel brake, the manifold feeding these valves is connected to the brake pilot valve and the one valve controls both flywheel brake and compression relief valves.

5. STARTING AIR PILOT VALVE

Valve (30) in Fig. R-2 is for the control of the master valve in the starting air manifold, described in detail in Paragraph 11. This is a piston operated valve, held closed by the air pressure on the valve head and opened by the pressure above a piston when the cylinder below is vented. The pilot valve operating the master valve must therefore vent the cylinder below the piston. It is a simple poppet valve, mechanically opened and spring closed. Referring to Fig. R-2 chamber (29) is connected to the cylinder below the piston in the master starting valve. When the pilot valve is opened by lever (9) as previously described, this chamber is vented into the control housing and the master starting air valve opens, admitting air to the starting air manifold. When the pilot valve is closed pressure immediately builds up below the piston and the master valve closes.

The position of lever (9) when free from the cams is determined by an adjusting screw in the lever and bearing against a boss in the control housing. This screw should be set to bring the cams on hub (16) (See Fig. R-1) into contact with the pawls on lever (9) when the control handle is 32° from STOP either AHEAD or ASTERN. Equalize the adjustment on either side, making the mean 32°. After locating the lever as above, set the adjusting screw in the end of the lever to allow .015" clearance between screw head and the pilot valve stem with the control lever at STOP.

The pilot valves should be ground to their seats occasionally if leaking. Leakage, unless excessive, will not materially effect the operation of the control unit, but it will of course increase the air consumption necessary for maneuvering. The seal for the vent valves is between the end of the pilot valve stems and the under side of the vent valve heads. When grinding these seats use care not to get any grinding compound into the fit between the vent valve and pilot valve.

6. AIR RAM, REVERSING RACK AND CONNECTION TO LATCH SHAFT

The power for rotating the latch shaft through 180° from the AHEAD to ASTERN positions or vice versa is supplied by an air ram, or double acting air piston, connected by means of a reversing rack and gearing to the latch shaft. It is located on the top of the latch box and is shown in detail on Fig. R-3.

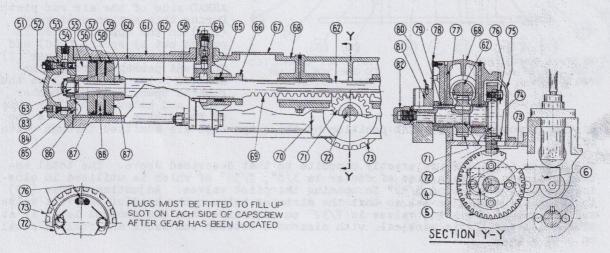


FIG. R-3

Referring to Fig. R-3, housing (68), which is bolted to the top of the latch box, carries reversing rack (62) and pinion shaft (72) in replaceable bronze bushings. If renewed bushings must be reamed to 2.002" - 2.003" and 2.249" - 2.2505" diameter respectively after pressing in, and the oil holes must be drilled through the bushings in line with the holes in the housing. The unit is located on the latch box with the pinion shaft at the center of the engine, midway between cylinders 3 and 4. Cylinder (61) is provided with a bronze liner to prevent rusting, and is bolted together with front head (64), to the after end of housing (68). A stuffing box (65) and gland (66), accessible through cover plate (67), seal the piston rod

where it passes through the front head. The after end of the cylinder is closed by back head (51). Connection (54) in the back head and a similar connection in the front head are connected by copper tubing to the pilot valves in the Control Unit, described in detail in paragraph 3.

The piston assembly is made up of piston (88) with ring (57), cup leathers (56) and (58), followers (87) and collars (59). The assembly is mounted on the after end of the piston rod (62), and is clamped by nut (63). The reversing rack teeth (69) which engage pinion (71) are cut in the forward end of the piston rod (62).

The travel of the piston is limited at each end by contact between followers (87) and the cylinder heads. In order to prevent shock the piston is cushioned at each end of its stroke by trapping part of the air ahead of it. Referring again to Fig. R-3 and assuming that air is being admitted to the right side of the piston from the pilot valve in the control housing, the piston will be moving toward the left. The air in front of it will be expelled through connection (54) and the pilot valve in the Control Unit, the vent valve of which will be open. As the piston approaches the end of its stroke collar (59) enters opening (86) in the head, closing it off, and traps the air in front of the piston. This trapped air must then pass through needle valve (85), which should be adjusted to produce the desired cushioning effect on the piston. Remove plug (83) to reach the needle valve for adjustment.

1

Check valve (53) is provided to admit air to the full face of the piston when it is to be returned to the opposite end of the cylinder. This valve is made necessary by the closing of opening (86) by collar (59), thus preventing air from chamber (52) reaching the full face of the piston until collar (59) clears the head. Valves (53) and (84) are duplicated in front head (64), but are not shown in Fig. R-3. The action of the piston at the front end of the cylinder is exactly the same as that described above. Valves (84) and (53) are not shown in their correct positions in Fig. R-3, valve (53) and connection (54) from the pilot valve actually being located on the horizontal centerline toward the engine in the back head and valve (84) 30° off the vertical. In the front head, both valves are in the top, 5/8" each side of the centerline, and the inlet connection from the pilot valve is on the horizontal centerline away from the engine.

Section YY in Fig. R-3 shows a transverse section through pinion shaft (72). This shaft, which is driven from reversing rack (62) by means of pinion (71) to which it is keyed, has a flange on its inner end to which is bolted helical gear (73). This gear meshes with a similar gear (5) on the latch shaft (4) and thus completes the connection between the air ram piston and the latch shaft. Housing (68) is located and doweled on the latch box so that these gears mesh properly, and if replaced the new housing must be carefully located, and new dowel holes drilled so that these gears are correctly meshed.

The holes in the hub on shaft (72) for mounting gear (73) are slotted, and if either gear (73) or its mating gear (5) on the latch shaft are replaced, gear (73) must be adjusted radially on the shaft to correlate the motion of the air ram piston and the latch shaft. The correct AHEAD and ASTERN positions of the latch shaft are shown by marks scribed on one of the latch shaft webs registering with a pointer mounted on the adjacent latch shaft bearing. The latch shaft should be set in the correct A-HEAD position and the gear and hub then adjusted radially to locate the air ram piston at the extreme end of its stroke, that is, against the back head of the cylinder. Three of the four capscrews (76) holding gear and hub together are then tightened. The one remaining capscrew will require plugs to be fitted on each side to fill up the slot in the hub (72). These plugs will retain the gear in its proper position and eliminate the necessity of redrilling and reaming for a dowel pin. In fitting these plugs make sure that each plug contacts both the end of the slot and the capscrew so that it would be impossible for the gear to slip, as any slippage would change the valve timing. After the plugs are fitted the capscrew may be tightened and secured by the lockwire which passes thru the head of all four of the gear retainer capscrews. Four oil cups on the top of the reversing rack housing provide lubrication for the reversing rack and pinion shaft, and should be oiled as often as necessary to keep the bearings well lubricated. Two small pipe plugs are provided in the top of the air cylinder for lubricating the piston.

Barring hub (81) on the outer end of the pinion shaft provides means for operating the reversing mechanism manually in an emergency or while working on the engine. A one inch bar about four feet long may be used.

The required motion of the latch shaft is 180° and the tooth ratio of the two gears is such that shaft (72) must rotate 270° to give this latch shaft motion. This requires a total piston travel of 10-1/16" which may be adjusted if necessary by changing the thickness of the gaskets under the cylinder heads. The position of shaft (72) and hence of the entire assembly, including the air ram piston and the latch shaft, is indicated by pin (80) in barring hub (81). This pin registers with the AHEAD and ASTERN on indicator plate (78). The AHEAD on this plate is forward

and the ASTERN aft. The pin rotates through the lower arc, and the reversing rack must therefore be moving aft (to the left in Fig. R-3) when the latch shaft is moving from ASTERN to AHEAD. The air must be admitted to the forward (or right hand in Fig. R-3) side of the piston to produce this motion, which puts the engine in AHEAD position. Therefore the ahead pilot valve in the control housing, (which is on the left or after side of the housing, as explained in paragraph 3) must be connected to the forward or front head of the ram cylinder. Conversely the astern valve is connected to the rear head. The position of the piston is aft when the engine is running AHEAD and forward when it is running ASTERN. (The above discussion holds true for both right and left hand engines.)

7. LATCHES AND LATCH SHAFT

For a given direction of rotation all the valves must be actuated in a definite sequence and with a definite timing. For direct reversible engines it is consequently necessary to provide dual sets of cams, one set for operation in the AHEAD direction of rotation, the other set for operation when running ASTERN. At the same time means must be provided for throwing one set of cams into operation, while at the same time the other set must be made inoperative.

In Atlas engines the AHEAD and ASTERN cams are mounted side by side on the camshaft. Referring to Fig. R-3 it will be noted that latches equipped with two rollers are interposed between the cams and the valve lifter rollers. The two latch rollers are offset and lined up relative to the cams in such a manner that in the AHEAD position of the latches one set of rollers contact the AHEAD cams while at not shown in Fig. R-3.) Thus in the position shown in Fig. R-3 the AHEAD cams actuate the latches which in turn actuate the valves by means of the lifters, pushrods and rockers.

By rotating the latch shaft 180° the latch fulcrum points are moved inward (toward the center of the engine) to a point where the ASTERN cams contact the other set of latch rollers. This inward movement frees the AHEAD latch rollers of the AHEAD cams and consequently the ASTERN cams now control the actuation of the valves.

The fuel valve timing is very nearly the same for both directions of rotation. For example, in one direction of rotation the fuel valve may open 8° before top center and close 18° after top center. Then if the rotation was reversed and the latch kept in the same position the fuel valve would open 18° before top center and close 8° after top center. In other words, the timing would be 10° early. It is possible to compensate for this slight difference in timing by properly positioning the ASTERN roller on the fuel valve latch. Consequently only one fuel cam is provided which serves for both AHEAD and ASTERN running and the fuel latch rollers are in line, not offset as on the other latches.

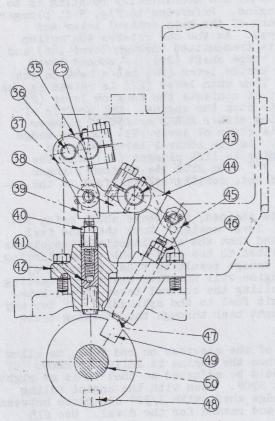
The case hardened steel latch rollers turn on steel pins carried in the bodies of the latches and riveted in place. In the inlet, exhaust and starting air latches, spacers between the walls of the latches and the sides of the rollers establish the positions of the rollers in line with the cams. The fuel valve latch does not require any spacers since only one cam is used and both rollers are in line. The rollers all have a clearance of .001" to .002" on the pins and a side clearance of 1/64".

The latch shaft is built up of six sections, each section comprising the crankshaft for the four latches of a single cylinder. The shaft is mounted on cast iron bearings which are bolted to the side of the centerframe. Journals are turned on the shaft at each end of each crank, and flanges at the ends of each section provide means of bolting the sections together. Bearing clearance is .001" to .0025" and end play is taken by the two outer bearings.

& LATCH SHAFT INTERLOCKING DEVICE

The latch shaft interlock is shown in Fig. R-4. The two plungers (41) and (47) are located fore and aft so that they are in line with adjacent latch shaft webs, and they engage slots (48) and (49) cut in the respective webs. These plungers are interconnected by rockers (38) and (44) and shaft (43), the whole assembly being mounted in bracket (42) on top of the latch box, just aft of the control unit. The device is operated from the main control shaft in the control unit by means of shaft (25), to the far end of which a helical gear, ((24) in Fig. R-1) is keyed and clamped, which gear in turn meshes with a similar gear ((19) in Fig. R-1) on the control shaft. Shaft (25) carries crank (35) on its overhung end, and pin (36) in the crank is connected through link (37) and fork (39) to plunger (41).

For plunger positions shown in Fig. R-4, the control handle is at STOP, the latch shaft is in AHEAD position, slot (49) registers with plunger (47), slot (48) is



180° out of register with plunger (41), and both plungers are up clear of the latch shaft webs so that the latter is unlocked and free to turn. Assume now that the control lever is moved in the AHEAD direction. The hand of the helical gears is such that shaft (25) will be rotated clockwise as viewed in Fig. R-4, which will lift plunger (41) through the action of crank (35) and link (37). Plunger (47) will be lowered at the same time, through the interconnection of the rockers (38) and (44) and shaft (43), and will enter slot (49) in the latch shaft web, thereby locking the shaft in the AHEAD position and preventing its shifting to any other position.

As a second assumption, consider the control handle to be moved toward ASTERN. The above action will be reversed, and plunger (41) will move downward. Since it is not in register with the slot in its mating latch shaft web it can move only until it contacts the web, and will then arrest the motion of the control lever. This action takes place when the control lever is moved 25° from STOP and it cannot be moved further until the latch shaft shifts to ASTERN and slot (48) is brought into register with plunger (41). Thus it is impossible to admit starting air to the engine unless the latch shaft is in the position corresponding to the direction in which the control handle is moved.

It should be understood that this interlock stop is primarily a safety device to prevent starting the engine before completion of the latch shaft shift, and it should not be abused by deliberately jamming the lever over against it, as this will result in excessive wear throughout the mechanism,

FIG. R-4 result in excessive wear throughout the mechanism, if not in damaged and broken parts. Normally the latch shaft will shift almost immediately upon opening of the pilot valve (which occurs with 14° motion of the control handle), and it will be possible to move the control handle right along to the starting air period, with only a slight pause at the 25° stop point. During this pause, while the latch shaft is shifting, the control handle should not be held up against the stop, with the plunger bearing against the latch shaft web and consequent wear on both parts.

Before disassembling the interlock drive mechanism the helical gears should be marked so that they may be remeshed in the same relation. Crank (35) and rocker (44) are pinned to their shafts with taper dowels, while the helical gears and rocker (38) are keyed so that the device can only be assembled in one way, so long as the gears are correctly meshed. If at any time the gears, shafts, crank or rockers are replaced, the plungers must be retimed, which may be done as follows. With the control handle at STOP, adjust crank (35) relative to shaft (25) so that the vertical distance from the top of the latch box up to the center of the pin in fork (39) is 4-1/4". Be sure that shaft (25) is forced to the left so that gear (24) (Fig. R-1) is bearing against the control housing boss, and allow .010" thrust clearance between crank (35) and the housing. Clamp crank (35), drill a hole through the shaft using #7 drill (.201" dia.) then taper ream for #4 taper dowel. Adjust rocker (44) relative to shaft (45) so that the vertical distance from top of latch box to center of pin in fork (45) is 3-1/16", clamp rocker and drill and ream rocker and shaft for #4 taper dowel.

Set latch shaft at some intermediate position, and move control lever in AHEAD direction until latch pin (5) (Fig. R-1) drops into the slot in latch plate (6). Position lever so that pin is about 1/8" from upper end of slot, and then adjust plunger (47) (Fig. R-4) relative to fork so that end of plunger bears against latch shaft web. This will allow some clearance between plunger and web when latch pin bears against upper end of slot. Repeat adjustment on plunger (41) for reverse, and tighten jam nuts to lock plunger adjustments. Interlock bracket (42) (Fig. R-4) is doweled to the latch box, and if replaced the new assembly must be located so that the plungers will enter the slots in the latch shaft webs before drilling the new dowel holes.

9. FUEL CUT OUT MECHANISM

The fuel cut out mechanism shown in Fig. R-1 serves to stop the engine by taking

the wedge shaft out of the control of the governor and mechanically rotating it to pull out the wedges and cut off fuel to the engine. Referring to Fig. R-1, plunger (85) bears on cam (17) which is rotated by means of the main control lever and shaft (13) to which both lever and cam are keyed. As the cam rotates the motion of plunger (85) follows the cam profile, and is transmitted through lever (86) and rod (23) to lever (22) which floats freely on wedge shaft (20). A second lever (21), which is clamped and keyed to the shaft beside lever (22) has a hook on its free end which projects out over lever (22). Thus when lever (22) is raised by the action of cam (17) and the connecting linkage, it contacts the hook on lever (21) and rotates the wedge shaft counterclockwise to stop the engine. The profile of cam (17) is such that when the engine is running either AHEAD or ASTERN plunger (85) is down, dropping lever (22) so that it is clear of lever (21) and the wedge shaft is free to float under governor control. As the control lever is moved toward STOP through SLOW position cam (17) begins to lift plunger (85) when the lever reaches a position 56° from STOP and at 48° from STOP the maximum plunger lift is reached and the fuel wedges are pulled out, cutting off all fuel to the engine.

The above action is reversed when the engine is started, the wedge shaft being released to governor control with 56° of control lever motion. Note that the fuel cut out does not begin to release until 48° , and that the starting air valve closes at 50° so that there is virtually no fuel admitted to the engine while the starting air is on, thus preventing any possibility of damage resulting from excessive cylinder pressures. This also means that the engine will not fire while the starting air valve is open, so that as soon as it is rolling the control lever should immediately be moved along to SLOW in order to admit fuel to the cylinders. If for any reason it does not fire the lever must be brought back through the starting cycle and the action repeated.

The fuel cut out should be adjusted, by means of the clevices on rod (23), to allow 1/32" clearance between levers (21) and (22) when the engine is idling at SLOW. If the wedge shaft is ever replaced, rod (23) should be adjusted so that it is at right angles to lever (22) with the control lever at STOP. Then with the engine idling at SLOW lever (21) should be clamped to the wedge shaft with 1/32" clearance between it and lever (22) and the wedge shaft drilled and reamed for the dowel. Use #15 (.180") drill and #3 Taper reamer.

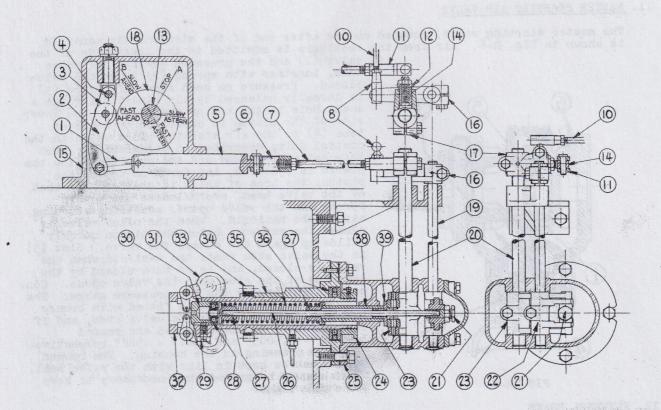
10. GOVERNOR AND GOVERNOR CONTROL

The flyball type governor, mounted near the bottom of the forward end of the latch box and driven from the camshaft gear, is shown in Fig. R-5. Cast iron bearing (34) is adjusted and doweled to the latch box to allow .004" to .005" backlash between governor gear (33) which is pressed and keyed to the governor body, and the camshaft gear. Running clearance between governor body (32) and the bearing is .0015" to .0025" and lubrication is from the force feed system of the engine.

The engine speed is controlled by varying the governor spring tension through a linkage from the control lever, as shown in the upper portion of Fig. R-5. (This is section W-W in Fig. R-1 taken through the governor control cam (18)).

Referring to Fig. R-5, it is seen that the governor spring reaction is transmitted from lever (23) which carries hardened rollers that bear against collar (39), through vertical shaft (20) to upper lever (17). This lever is connected by rod (7) to governor cam plunger (5) and by linkage is made to follow motion of governor cam (18). As shown in Fig. R-5, the control lever is in the FAST AHEAD position and cam plunger (5) is pulled to the left the limit of its travel compressing governor spring (35) to its shortest length and allowing fuel wedges to be drawn governor quill rod (26) to the left till linkage is solid. As the control handle is moved back toward SLOW, the cam drops allowing the roller (3) and cam plunger governor weights (31) to move out and push the wedges out decreasing the fuel supply to the engine.

Governor weights (31) mounted on pins in governor body (32) carry rollers on riveted pins. As the flyballs tend to move out due to the centrifugal force the rollers exert a force against sleeve (38) acting through spring (35), spring guide (27), ball bearing (28) and plunger (30). Plunger (30) rotates with the governor body while quill rod (26) and spring guide (27) remain stationary. The thrust reaction is taken by ball bearing (37) and retaining collar (24) which is threaded on governor body (32). The clearance for collar (24) is adjusted to .010" and the collar is then secured to the governor body by a setscrew and lockwire. The governor weight thrust is transmitted directly to the governor spring (35). The spring reaction is taken by sleeve (38) and collar (39) to vertical shaft fork (23).



The quill rod motion is independent of the linkage which compresses the governor spring and is transmitted to the fuel wedge shaft through an independent vertical shaft (19) actuated at its lower end by fork (22) and at its upper end through lever (16) and ball joint (8). The spring reaction is such that the governor weights are held in by governor spring (35) against the centrifugal force tending to throw them out. Through the linkage to the fuel wedge shaft the wedges follow the motion of the weights, moving out and decreasing the fuel supplied to the engine as the weights move out with increase in speed. At SLOW (Point "B" on the cam) practically all tension on the governor spring is released and the torsion spring on the wedge shaft is acting as the governor spring. The action ASTERN is exactly as described for AHEAD, cam (18) being symmetrical about line A. The speed range of the engine from FAST to SLOW is adjusted by lever (17). Turning threaded sleeve (12) will cause the lever to lengthen or shorten thereby causing smaller or greater travel of governor spring lever (23).

For full speed setting (control lever at FAST), the tension of the governor spring is varied through levers (17) and (23) by lengthening or shortening rod (7) which is threaded with right and left hand threads. This setting must be coordinated with the speed range setting to insure proper operation of both adjustments.

For adjustments of the wedge shaft linkage, setscrew (21) bearing against the end of the quill rod (26) should be set to equalize the motion of lever (22) on each side of its midposition.

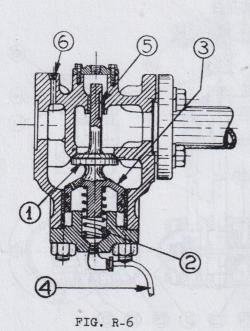
The torsion spring on the wedge shaft is primarily for the purpose of taking up the lost motion in the linkage, but since it acts in the same direction as the governor spring and is considerably lighter it serves well as a governor spring during idling and is so used. The idling speed may be varied by adjusting the clamp holding this spring to the wedge shaft, thus changing the tension of the spring. It should be set at about 100 to 120 R.P.M. at SLOW, which should be obtained by tightening the spring about one half turn from its free position.

There is also another spring acting on the wedge shaft. It is mounted on a stud on the centerframe and bears against a lever clamped to the shaft, serving as a buffer spring to prevent over regulation of the governor when the propeller is thrown clear of the water in rough seas. It does not enter into the normal governing of the engine. The adjusting nuts on the mounting stud should be set so that the upper spring washer just contacts the lower nut when the engine is at SLOW.



11. MASTER STARTING AIR VALVE

The master starting valve, mounted on the after end of the starting air manifold, is shown in Fig. R-6. Air from the receivers is admitted to the lower side of the

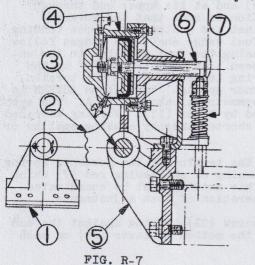


valve (1) and the pressure against the valve head, together with spring (2) keeps the valve closed. Pressure on both sides of piston (3) is normally balanced by air bleeding through a small hole in the top of the piston. The lower side of the piston is connected by means of tube (4) to the air starting pilot valve in the control unit, described in paragraph 5. When this valve is opened and the pressure below the piston is relieved, the force on top of the piston, the area of which is greater than that of the valve head, overbalances the upward forces and the valve opens, admitting starting air to the manifold. When the pilot valve is closed the pressure below the piston quickly builds up again and closes the valve. Slot (5) in the valve stem vents the manifold when the valve is closed, and is in turn closed by the lowering of the stem when the valve opens. nection (6) is for the air pressure gauge. cast iron valve housing is fitted with bronze bushings for the piston and valve stem, and if replaced they should be bored and reamed 3.4995" - 3.5005" and .561" - .562" respectively after pressing in the housing. The reamed holes must be kept in line with the valve seat, which should be ground when necessary to keep the valve tight.

12. FLYWHEEL BRAKE

The flywheel brake assembly is shown in Fig. R-7. Brake shoe (1) which is faced with brake lining, is carried by the horizontal arm of crank shaped lever (2).

This lever is mounted on shaft (3), and carries



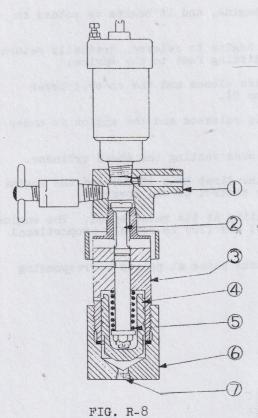
the brake cylinder (4) in trunnions on its vertical arm. Shaft (3) is supported by bracket (5) which is bolted to the after end of the centerframe. The projecting end of the piston rod (6) bears against the compressor cylinder and therefore the piston and rod remain stationary when air is admitted to the cylinder. When the pilot valve in the Control unit is opened, as described in paragraph 4 and air is admitted to the brake, the cylinder moves relative to the piston. Lever (2) is rotated about its fulcrum, applying the brake to the flywheel and stopping the engine. When the air pressure is relieved the brake shoe is withdrawn from the flywheel by spring (7), which bears against a third arm on lever (2).

There are no adjustments necessary on the brake and the only service requirements are the replacement of the shoe lining and the piston cup leather when necessary.

13. COMPRESSION RELIEF VALVES

NOTE: These valves are not supplied as standard equipment, but only when specifically ordered.

The pneumatically operated cylinder compression relief valves, illustrated in Fig. R-8, serve to relieve the pressure in the cylinders in the event that the engine becomes air bound on top center. These valves receive air from a manifold mounted just below the starting air manifold. As previously explained, the air is supplied from the flywheel brake pilot valve in the control unit. Since it is only at infrequent intervals that the operation of these valves may be required, a globe valve is placed in the line feeding the manifold, and it is recommended that it normally be kept closed. If at any time the engine refuses to start due to the cylinders being air bound, the valve should be opened while the engine control lever is at STOP, and the cylinder pressures will immediately be relieved.



Referring to Fig. R-8, valve body (3) is screwed into tee (1), which is in turn screwed into the cylinder head.

Valve (2) is held against its seat in the body by spring (5), which is secured to the top of the valve stem by a nut and washer.

Piston (4) bears against the end of the valve stem, and when air from the manifold is admitted to the hole (7) in cap (6) the force on the piston overbalances the spring force and the force due to the cylinder gases on the head of the valve and the valve is opened, relieving the cylinder pressure through the drilled holes in the valve body.

The relief valves should not need any adjustment, other than to grind the seats in occasionally if they leak.

14. MANEUVERING THE ENGINE - SUMMARY OF CONTROL EVENTS

Assume that the engine has been running ASTERN and that it is desired to go AHEAD. The Control Lever has then been located somewhere between FAST and SLOW on the ASTERN side and the first step is to move it to the STOP position as shown in FIG. R-9. On its way up to STOP the Control lever has then caused the fuel to be cut off and the Flywheel Air Brake to go on. Consequently with the Lever in STOP as shown the engine will rapidly come to a stop. The lever should be kept in the STOP position

After the engine has stopped, the Control Lever can be moved toward START on the AHEAD side. Referring to the numbered positions on Fig. R-9, the following events take place.

until the engine has come to a full stop.

- (1) In this position the pilot valve controlling the flywheel brake and the compression relief valves is closed and the vent is opened, releasing the brake and closing the compression relief valves. At the same point the ahead pilot valve for the air ram is opened and the ram operates to put the latch shaft in the AHEAD position.
- (2) Keep the control lever in this position for a moment until the air ram has shifted the latches to AHEAD. Watch the indicator pin on the barring hub of the air ram mechanism which indicates the latch shaft position.
- (3) In this position the latch shaft interlock mechanism operates and prevents further motion of the control lever until the latch shaft has been shifted to AHEAD position.
- (4) In this position the starting air pilot

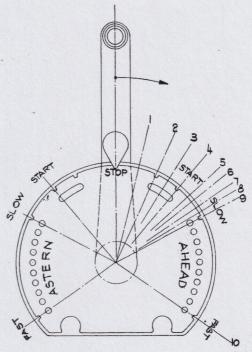


FIG. R-9

valve is opened admitting starting air to the engine, and it begins to rotate in the AHEAD direction of rotation.

- (5) In this position the fuel cutout mechanism begins to release, gradually returning the wedge shaft to governor control and admitting fuel to the engine.
- (6) In this position the starting air pilot valve closes and the control lever should immediately be moved on to SLOW (position 9).
- (7) In this position the fuel cutout is entirely released and the engine is under control of the governor.
- (8) In this position the air ram pilot valve closes venting the ahead cylinder.
- (9) In this position the control lever enters the first hole (SLOW) and the engine is idling at approximately 100 to 120 RPM under control of the governor.
- (10) In this position (FAST) the engine is operating at its rated speed. The engine speed at the various holes between positions (9) and (10) is roughly proportional to the position of the hole.

The various control events on the ASTERN side take place at points corresponding to those on the AHEAD side.

1. The lubricating oil system consists of the day tank, two lubricating oil pumps (pressure and scavenge), the lubricating oil filter, the lubricating oil cooler and the necessary piping and manifolds to carry the oil through the system and to the bearings. In addition to the main lubricating oil system as outlined above there is also the Madison-Kipp lubricator, supplying a measured quantity of oil to each piston and cylinder liner. The normal oil flow is from the day tank to the pressure pump, then through the oil cooler to the manifold in the base supplying the main bearings. In special cases (when engines are ordered with a full flow filter) the normal oil flow is from the pressure pump through the filter and then through the oil cooler to the manifold in the base supplying the main bearings. Drilled holes in the crankshaft carry oil to the crankpin bearings and the rifle drilled connecting rods feed the piston pins. The oil from the bearings drains down to a sump in the after end of the base, from which it is sucked up by the scavenge pump and discharged back to the day tank.

The by-pass filter (Std. equip.) is fed from the pressure pump discharge line, ahead of the oil cooler, and the discharge from this filter lubricates the rotary pump drive and the camshaft bearings adjacent to the camshaft gear and the high pressure fuel pump crank. When a full flow filter is used this line comes direct from the pressure pump discharge line to the rotary pump drive and camshaft bearings. The intermediate camshaft bearings are lubricated from catch basins in the tops of the bearings.

A four-way cock interconnecting the piping to and from the lubricating oil cooler permits by-passing and isolating the cooler. A pressure relief valve in the line protects the pressure pump in the event that the cock is thrown to an intermediate position (and thus shut off), or against a stopping up of the oil cooler. The cock should always be thrown quickly from one position to the other, and should never be left in an intermediate position.

The lubricating oil pressure is regulated by means of a relief valve connected in the pressure pump discharge line. This valve should be adjusted so that the pressure gage (located on the gage board) shows a reading of 35 to 40 lbs. per square inch, when the oil is hot.

Note that low lubricating oil pressure may not necessarily be due to relief valve adjustment. It may result from one or more of the following causes. They should be investigated before attempting to correct the pressure by adjusting relief valve at the pressure pump.

(a) Low lubricating oil level in day tank.

(b) Restriction in suction pipe to either of the lubricating oil pumps.
(c) Broken pressure pipe or fitting.

Broken pressure pipe or fitting.

(d) Crankshaft bearing failure.

Worn pump gears. (f) Viscosity of oil too low, excessive temperature of oil, or thinning out with fuel oil.

2. LUBRICATING OIL DAY TANK

The cylindrical lubricating oil day tank, has a capacity of about 16 gallons on 10" bore engines and about 20 gallons on engines with larger bore. It should be mounted vertically with the bottom at least three feet above the engine room floor, and should be piped by the customer to the discharge from the lubricating oil sump pump and the suction of the pressure pump. The former connection should be 1" to 1-1/4" pipe, leading to the 1-1/4" pipe tap hole in the top of the tank, and the latter connection should be 1-1/4" to 1-1/2" pipe, and should lead to the 1-1/4" or 1-1/2" pipe tap hole 6" to 8" above the bottom of the tank. A drain valve should be connected to the bottom of the tank.

A gage glass near the top indicates the oil level, which should be maintained between the center and top of the glass when the engine is running. Under no circumstances should it be permitted to drop below the glass. The tank should be drained and flushed out at intervals to keep the sludge in the bottom from building up to the pump suction connection. New oil should be added to the system through the filler hole in the top of the tank, which is protected by a screen.

3. LUBRICATING OIL PUMPS

The lubricating oil pump drive is shown in Fig. T-1. The pressure pump (14) and scavenge pump (3), together with the fuel transfer pump (6) are mounted in a common housing on the after end of the control side of the engine. The lubricating oil

pumps, which are identical except for the length of the shafts and the keyways, are gear type reversible pumps, employing an internal gear, an idler and a crescent shaped baffle to maintain the direction of flow through the pump regardless of direction of rotation. When the engine reverses the crescent shifts position, following the rotation of the idler, and maintaining the direction of flow of the oil

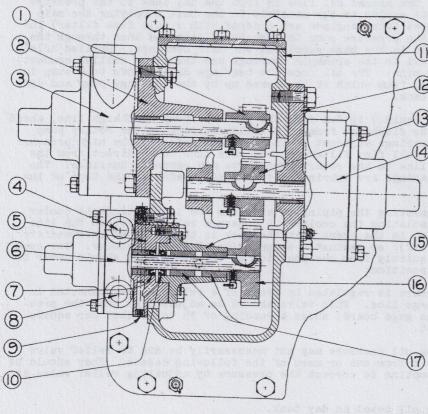


FIG. T-1

the stop. If a pump has been disassembled, re-assemble it to adapters (2) or (12) and turn the shaft by hand in both directions of rotation. It can then be felt when the crescent hits the stops. This is important because if the crescent cannot move the oil flow will not be reversed when the engine reverses and consequently the lubricating oil pressure will drop.

The lubricating oil pumps are mounted in the housing in adapters (12) and (2) which are doweled to the housing after positioning for a gear backlash of .004" - .005". Cylindrical fits locate the pumps in the adapters so that the pumps may be replaced without disturbing the gear setting. If the adapters are ever replaced for any new dowel holes drilled.

Bronze bushings in the adapters carry the pump shafts, and if replaced must be reamed to .7500" - .7505" after pressing in. Use care to keep reamed holes square with face of adapter. The bushings adjacent to the pumps are lubricated by leakage along the shaft from the pump and the outboard bushings from catch basins on the adapter castings which are filled by the lubricating oil spray nozzle which lubricates the whole assembly. (Note: On later engines both inboard and outboard bearings are pressure lubricated by oil lines inside the pump housing.) The oil holes for the outboard bushings must be drilled when renewing bushings. The pinions driving the pumps are keyed to the shafts and locked with setscrews and mesh with a gear on the after end of the camshaft. The setscrew heads are drilled for locking wire, and should be well wired when reassembling. The gears are accessible through cover

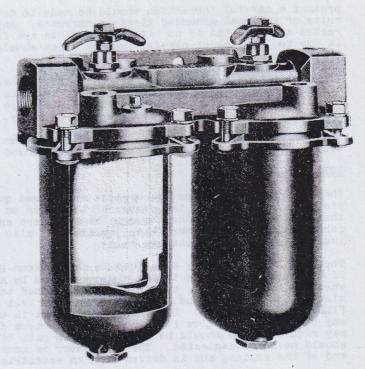
4. LUBRICATING OIL FILTER - (By-pass Type - Standard Equip.)

The filter is of the metal element type as shown on Fig. T-2. The elements are made up of flat metal ribbon wound around a central spool, adjacent layers being slightly separated from each other by raised ridges running across the ribbon. The successive

If dismantled the pump must be reassembled with the parts in the same positions, as reversing the assembly will reverse the suction and discharge ports. The correct assembly may be determined by remembering that the crescent always moves through the suction zone when reversing. There is a projection on one side of the cover which acts as a stop for the crescent, and the cover should be assembled with this projection on the suction port side of the pump. Follow these instructions in determining the flow direction of the pumps rather than the arrows stamped on the casings, as these arrows may not always be correct.

The total end play between the pump rotor and the end covers and adapters (2) and (12) should be very small, only about .001" to .003". However, some end play must be allowed so that when the engine is reversed the crescent can move in the new direction of rotation until it is up against to adapters (2) or (12) It can then be felt when the crescent canmot move and consequently the lu-

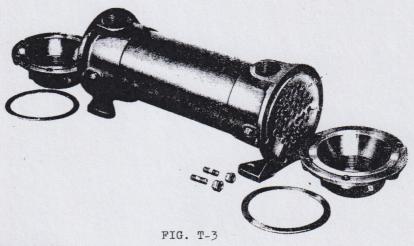
layers of the ribbon are spaced .003" apart and it is these spaces that form the filtering medium. The oil flows from the outside toward the center and leaves the dirt on the outside of the spool. The filter may be cleaned by turning the cleaning handles on top, which rotates a knife bearing on the edge of the windings, scraping off the dirt and allowing it to settle to the bottom of the sump tank. The filter should preferably be cleaned when the engine is not running so that the dirt may settle to the bottom, although there is no objection to cleaning with the engine running. Cleaning should be at sufficiently frequent intervals to prevent stoppage of oil flow and the sump tanks should be drained before the dirt in the bottom builds up to the level of the elements. Experience will determine the correct intervals.



5. LUBRICATING OIL FILTER - (Full Flow Type - Special Equip.)

FIG. T-2

The filter is a duplex unit of the metal element type and is very similar to the bypass type described above, except that the filter is equipped with a switch over valve which allows either of the two units to be cut out for cleaning or servicing. For care and operation of this filter follow instructions shown above for the bypass type.



6. LUBRICATING OIL COOLER

The construction of the Ross type oil cooler is shown on Fig. T-3. The shell of the cooler is a completely closed circuit effected by brazing the tube sheets on each end to the seamless copper shell, and then mechanically rolling the tubes securely into the tube sheets at both ends. The bonnets are bolted to the shell flanges, with molded asbestos gaskets between, and can be removed for inspection and cleaning of the inside of tubes. The flow of the oil is guided by bronze baffles inside the shell to produce the most efficient heat transfer.

Zinc electrode plugs are provided in the bonnets to prevent electrolysis. They should be examined thirty days after installation and every thirty days thereafter. Any appreciable erosion within this period indicates electrolytic action, and if

present a careful inspection should be made to determine if it is due to short circuits or external grounded electric currents. Any such conditions should be corrected at once, but if no external currents are found it is evident that the erosion is due to local electrolysis, and the zincs should be replaced frequently to protect the equipment.

The cooler should be cleaned periodically. Remove the cooler from the engine, take off the bonnets and clean the inside of the tubes. Fill the jacket with suitable cleaning solution, but avoid any fluids which are corrosive to bronze or copper. Drain and blow out with compressed air carefully.

The drain plugs at the bottom of both bonnets should be removed and all water in the cooler drained out whenever the engine is allowed to stand in freezing weather.

7. LUBRICATOR AND DRIVE

The Madison-Kipp lubricator supplies a measured quantity of lubricating oil to the pistons, introduced at the center of the liner on each side. Nipples screwed into the liners and projecting through the cylinders and sealed thereto by packing glands (multi-collar thrust bearings only).

The lubricator is fully described in the Madison-Kipp bulletin attached at the end of the book. Oil feeds to the pistons should be adjusted to 20-25 drops per minute when the engine is new, but this may be reduced to approximately 15 to 20 drops per minute after the pistons and rings have been well worn in. KEEP THE LUBRICATOR WELL FILLED WITH CLEAN OIL. Use the same oil that is used in the engine. Do not under any circumstances allow it to run dry as serious damage to the pistons and liners may result. This should be made a regular part of the engine room routine and should never be neglected. The lubricator is mounted on a bracket on the forward end of the engine, and is driven from an eccentric on the end of the camshaft.

WATER COOLING SYSTEM

1. Atlas Diesel Engines are furnished with either raw water or fresh water cooling systems.

In raw water systems, the sea water is pumped directly thru the oil cooler, thru the engine and is then discharged overboard. This system uses a single pump either centrifugal or plunger type.

Fresh water or closed cooling systems, recirculates fresh water from a storage or surge tank and requires dual water pumps, one for the fresh water and the other for the raw water which is pumped thru a heat exchanger for cooling the fresh water.

With either of the above systems the water circuit from the oil cooler thru the engine is the same, while the arrangement or flow to the pump and cooler can vary considerably.

- 2. The water circuit from the oil cooler thru the engine is as follows:
 - (a) The water passes thru the oil cooler, cooling the lube oil and then to the water inlet manifold which distributes the water to the lower portion of each cylinder. The water rises to the top of the cylinders and then thru brass nipples (screwed into the cylinder) up into the cylinder head. Each nipple is sealed between the cylinder and head by means of a rubber grommet. The water circulates thru the cylinder heads and out thru elbows to the exhaust manifold. The exhaust manifold is made up of several sections and the water is by-passed from each and finally discharged at the top of the forward end of the manifold. From here, the water is passed overboard (in the case of raw water cooling) or recirculated back to the pump or surge tank depending on the type of installation.
 - (b) In addition to the main flow there are several minor parallel circuits as follows:
 - Air Compressor The water is piped directly from the main cylinder inlet manifold to the air compressor cylinder. From this cylinder it flows thru a pass-over pipe to the cylinder head and then to the aft end of the exhaust manifold.
 - 2. Fuel Spray Valve Cooling (Engines with $ll\frac{1}{2}$ " or larger bore) On engines with $ll\frac{1}{2}$ " or larger bore there is provided a fuel spray valve cooling circuit. Nozzles, discharging cool water directly against the spray valve bosses, are screwed into the cylinder head water jackets, and greatly reduce the tendency for coke to build up on the spray valve tips. The nozzles also prevent muck and scale from accumulating in the center of the heads around the valve bosses. The nozzles are fed from a manifold extending fore and aft just below the exhaust manifold. Since these nozzles discharge into the cylinder head water jackets there is no return line for this circuit.
 - 3. Valve Cage Cooling (Engines with $1l\frac{1}{2}$ " or larger bore only) Water is piped from the main water inlet manifold up to the valve cage cooling manifold (inlet) and then by copper tubing to each valve cage. The water is then returned to an outlet manifold which discharges into the exhaust manifold water outlet connection. On certain raw water cooling installations, this water is piped overboard.
 - 4. Thrust Bearing Atlas Multi-collared Type (Used only with raw water cooling systems) The thrust bearing cooling water is piped directly from either the main water inlet manifold, or the circulating water pump discharge. The water circulates thru the lower half of the bearing and then by means of pass-over pipes to the upper half of the bearing. After circulating thru the upper portion of the bearing the water is piped overboard.
 - 5. On certain engines (raw water cooled) the bilge pump discharge is connected to the water inlet manifold by a three-way cock, and the engine may be temporarily run at slow speed on this pump if the main circulating pump is out of service. Provision should be made for connecting the suction to a sea chest if the pump is to be used in this way.

3. DRAINING THE WATER

If the engine is to be allowed to stand idle in freezing weather it will be necessary to drain all water. Drain plugs will be found on the water pumps, air compressor exhaust manifold, water inlet manifold and the thrust bearing if it is the Atlas multi-collared type. If the engine is equipped with valve cages it will also

be necessary to remove the water. This can be accomplished by removing the cages, blowing the water out with air, or sucking it out with a hand suction pump.

4. PISTON TYPE CIRCULATING WATER PUMP (Engines with 13" or larger bore)

For construction of the pump refer to the Parts Catalog Plate facing the "Circulating Water Pump" group list sheet. Referring to this plate the pump piston is connected by means of a piston rod, crosshead, connecting rod and strap to an eccentric on the crankshaft. The pump body is divided into two chambers so that each side of the piston acts as a separate pump. Each chamber has a separate set of disc type, spring loaded, suction and discharge valves.

The piston rod packing nut is easily accessible and can be tightened with a pin or drift. New packing can be installed after loosening the splash guard and sliding it out of the way. A hand hole in the outer end of the pump body permits inspection and servicing of the piston. However, if much work is to be done on the pump, it is recommended that the connecting rod be unbolted from the eccentric and the whole pump assembly removed from the centerframe.

The piston assembly is made up of two piston discs, separated by a spacer and faced with cup leathers. Brass washers, approximately five on each side, are let into the leathers between the pistons and spacers, so that the clamping is through metal only, and the assembly cannot work loose due to compression of the leathers. It is important that these washers always be used on each side, and that the clamp nut be securely tightened and cotter pinned.

By removing the whole pump assembly as previously described and also the centerframe cover above the pump mounting, the crosshead and eccentric strap are made readily accessible for inspection or service. The strap which is babbitt lined, is fitted to the eccentric with a clearance of .006" - .010" on the diameter and has a side clearance of .003" - .006".

A bronze bushing is pressed into the crosshead end of the connecting rod for the wrist pin bearing. If replaced the new bushing should be reamed after pressing in to allow a clearance of .001" to .002" between the bushing and pins. The crosshead is reamed to a slightly smaller diameter, so that the clearance between crosshead and pin is .0005" to .0015".

Air chambers are provided to prevent water hammer, one on the suction and one in the discharge side of the pump. The chamber on the suction side is fitted with a ball check or snifter valve and a pet cock. When the pet cock is opened air is admitted to the chambers with each suction stroke of the pump. This valve should be opened as often as necessary to keep the chamber charged with air. Water hammer in the system indicates a lack of air in the chamber and the snifter valve should be opened. If the pet cock is left open continuously it should be opened just enough to prevent water hammer. If left wide open the pump capacity is lowered and the engine may not receive enough cooling water.

A zinc block is bolted in the bottom of the pump suction chamber to protect the various metals from electrolytic action. This block should be replaced when about 75% dissolved. New blocks can be installed after removing either the air chamber elbow or the suction line flange from the suction chamber.

5. PISTON TYPE CIRCULATING WATER PUMP (Engines with 112" or smaller bore)

For construction of pump refer to Parts Catalog Plate facing the "Circulating Water Pump" group list sheet. The drive is by means of piston rod, crosshead and connecting rod to a crank which in the case of 10" and $10\frac{1}{2}$ " bore engines is mounted on the end of the camshaft. On $11\frac{1}{2}$ " bore engines the crank is on the end of the jackshaft which is gear driven from the crankshaft.

For the functioning of the pump, servicing of the piston rod packing, and the piston construction see paragraph 4. Crank pins and crosshead pins should slide freely in the corresponding connecting rod bushings. Allow about .0015" to .003" clearance.

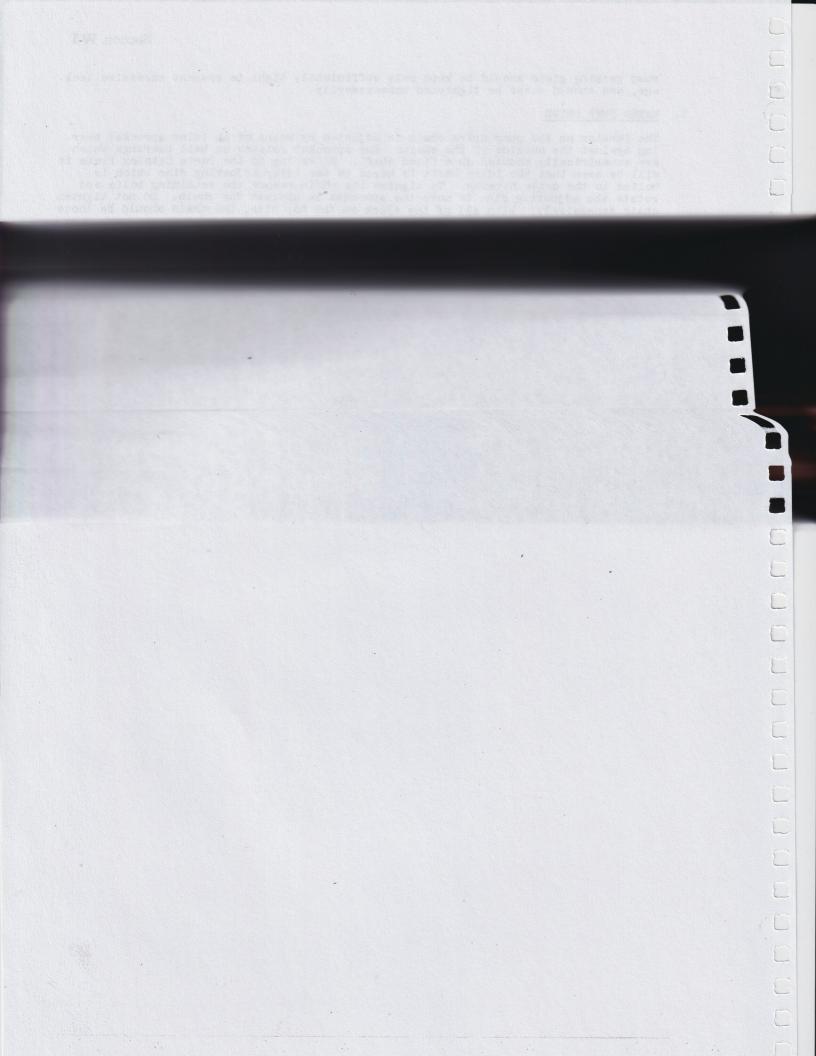
6. CENTRIFUGAL PUMPS (Single or Dual)

The water pumps, driven by a roller chain from a sprocket on the crankshaft, are mounted on a housing at the end of the engine. For illustration of the pumps and drive refer to the Parts Catalog Plate facing the "Circulating Water Pump" group sheet. The pumps are driven from opposite ends of a common drive shaft, rotating on ball bearings. Either pump may be removed by unbolting the pump mounting bracket from the drive housing and breaking the shaft coupling. Both pumps are identical and are interchangeable. When replacing a pump, the half coupling on the drive shaft should be removed and replaced by the one supplied with the new pump. The

pump packing gland should be kept only sufficiently tight to prevent excessive leakage, and should never be tightened unnecessarily.

7. WATER PUMP DRIVE

The tension on the pump drive chain is adjusted by means of an idler sprocket bearing against the outside of the chain. The sprocket rotates on ball bearings which are eccentrically mounted on a fixed shaft. Referring to the Parts Catalog Plate it will be seen that the idler shaft is keyed to the idler adjusting disc which is bolted to the drive housing. To tighten the chain remove the retaining bolts and rotate the adjusting disc to move the sprocket in against the chain. Do not tighten chain excessively. With all of the slack on the top side, the chain should be loose enough to permit a vertical movement of approximately 3/4" to 1". If the eccentric does not provide sufficient adjustment to take up the slack in the chain it is probable that the chain is excessively worn and should be replaced. The ball bearings for the pump drive shaft and idler sprocket are force feed lubricated from the engine pump. They should be examined at annual inspections, and replaced if showing evidence of wear.



AIR COMPRESSOR

1. SINGLE STAGE COMPRESSOR

On engines with 13" or smaller bore a single stage compressor is used. This air compressor is of the single acting type and is located at the after end of the engine. The cast iron, jacketed cylinder is bolted to the top of the centerframe directly behind number six cylinder. The cylinder head contains the spring loaded, disc type, suction and discharge valves. The compressor output is controlled by a diaphragm type suction valve unloader. This unloader is connected to the air tanks and when the pressure in these tanks reaches a pre-determined value, usually 225 lbs. per square inch, it acts to hold the suction valve open, thus cutting out the compressed air delivery. The unloader is mounted directly over the suction valve.

The piston, which is driven from the crankshaft by a connecting rod, strap and eccentric, is fitted to the cylinder with a clearance of .004" to .006". Five piston rings in all are used. Three 3/8" wide step cut compression rings are installed in grooves above the wrist pin and two 3/8" wide step cut, ventilated oil rings are placed below the pin. Side clearance is .0025" - .005" for all rings. The ring gaps should be .012" on the two top rings and .009" on all the lower rings.

The wrist pin is given a clearance of .000" to .001" in the pin bores and a clearance of .001" to .002" in the bearing assembly of the connecting rod. The pin is secured in the piston by a setscrew threaded into one of the pin bosses and locked by a jam nut. Shims between the foot of connecting rod and the strap allow for adjustment of the piston height. The top of the piston should be flush with the top of the cylinder when the cylinder is pulled down, and with the eccentric at top center. The strap is allowed a diametral clearance of .006" to .010" and a side clearance of .003" to .005".

2. TWO-STAGE COMPRESSOR

A two-stage single acting compressor is used on $14\frac{1}{2}$ " and 15" bore engines. It is located at the forward end of the engine and is bolted to the centerframe. A stepped piston is used which is driven by a connecting rod, strap and eccentric on the crankshaft. The piston and cylinder construction is shown on the Parts Catalog plates. It should be noted that the first stage is formed between the top of the piston and the cylinder head whereas the second stage is formed between the lower face of the piston step and the upper face of the cylinder step. The first stage or intermediate pressure is approximately 68 pounds per square inch and second stage pressure is the final discharge pressure of the compressor.

There are two lubricating oil holes on the air compressor cylinder which are combined into one lead to the mechanical oiler. It takes very little oil to lubricate the compressor and the mechanical oiler should be set for not more than one drop of oil per revolution of the oiler shaft. This will be a total of approximately 4 to 6 drops of oil per minute to the compressor if the engine is running at full speed. Under no circumstances should this amount of oil be increased.

The intermediate cooler, which is cast integral with the cylinder body, is provided with a safety valve set at 100 pounds per sq. inch. It is mounted on the side of the cylinder. If this safety valve pops the first stage discharge valves may be sticking or leaky, or the 2nd stage suction valve may not perform its function properly. Do not allow the intermediate stage safety valve to pop. If this happens, check the above mentioned valves and correct the trouble.

The lower portion of the intermediate cooler forms a water trap for the condensate which forms when the air is cooled. A drain is provided for this water. The drain line is carried out to the forward end of the engine where a cock is provided for draining purposes. The air compressor intermediate cooler should be drained at regular intervals, as otherwise the water which is formed will be carried into the 2nd stage. The water trap portion of the intermediate cooler holds approximately 2 quarts, and the drainage periods should be spaced at such intervals that less than this amount is drained out at one time.

The compressor output is controlled by a diaphragm type suction valve unloader acting on one of the first stage suction valves. The unloader should be connected to the air tanks and when the pressure in these tanks reaches a predetermined value, usually 225 lbs. per square inch, one suction valve is held open, thus cutting out the first stage air welivery. Due to the large clearance volume in the second stage no air will be delivered by this stage when the intermediate pressure is atmospheric. Consequently the first stage suction valve unloader controls the total output of the compressor. The unloader is mounted on a small cover over the first stage suction valves.

XI - Ed 1-2

The piston is provided with four compression rings on its large diameter and four compression and one oil control ring on the smaller diameter lower part. The oil control ring is mounted below the piston pin. The side clearance in the ring grooves should be .003" to .005" for all rings. The rings gap on all the large diameter rings and the two upper small diameter rings should be .016". The other rings should have a gap clearance of .012".

The case hardened and ground piston pin is stepped, with differential fits in the piston pin bosses. The fits are .0005" to .0015" press on the small end and metal to metal to .0015" loose on the large end. Rotation of the pin in the piston is prevented by the engagement of a dowel which projects radially from the large end of the pin with a groove in the bottom of the boss. A setscrew threaded into the smaller pin boss enters an indentation in the pin to act as a retainer. The setscrew is in turn secured by a locknut. A piston pin clearance of .0015" to .0025" is allowed in the connecting rod bushing.

Shims between the foot of the connecting rod and the top of the eccentric strap allow for adjustment of the piston height. The top of the piston should be flush with the top of the cylinder when the piston is on top dead center. The cylinder nuts should be tight when making this adjustment. No adjustment is provided, or necessary, for second stage clearance. All that is required is that the top of the piston be flush with the top of the cylinder in accordance with above instructions. The eccentric strap is allowed a diametral clearance of .006" to .009" and a side clearance of .005" to .008".

The construction of the suction and discharge valves is clearly shown on the parts catalog plate facing the "Cylinder and Head" group list sheet. Note that the suction valves are provided with spring retainers which screw on the ends of the valve stems. The retainers are locked by means of snugly fitting cotter pins and should be screwed down to allow a maximum suction valve lift of 1/8". On the first stage suction valves particularly, it is important that the spring retainer cotter pin fits snugly in the valve stem hole. Cotter pin should not be smaller than 1/8" dia. and should be long enough to allow the ends to be bent over so that pin will be securely locked. The small cover over the first stage suction valves in the cylinder head should be removed approximately once a month to make sure that the valve spring retainers are securely locked by their cotter pins. If the cotter pins should work out the spring retainers might unscrew allowing the suction valves to drop down into the cylinder with consequent damage to piston and head.

MAINTENANCE & INSPECTION

1. GENERAL RULES

Observing the following general rules will go a long way toward insuring satisfactory and trouble-free operation. Refer to preceding sections for detail instructions.

KEEP YOUR ENGINE CLEAN

Inspect the engine regularly and keep it wiped clean. If oil is left standing it quickly hardens and must be washed or scraped off. It is much easier to keep the engine clean than to get it clean, and there is always less trouble with a clean engine than with one that is covered with oil and dirt.

LEAVE WELL ENOUGH ALONE

When the engine is running satisfactorily and smoothly, do not continually try to better the operation with minor adjustments.

NEVER ALLOW YOUR ENGINE TO SMOKE

When the exhaust from an engine is smoky it clearly indicates that combustion is not perfect and that residue, in the shape of smoke, is clinging to the oily surfaces of the cylinders, pistons, piston rings, valves, etc. When this happens you are creating trouble for yourself and doing an injustice to the engine. Therefore, the first thing in consideration of the operation of a Diesel engine is: DO NOT ALLOW YOUR ENGINE TO SMOKE

KEEP A COMPLETE LOG OF ENGINE OPERATION

A complete log should always be kept of the engine operation, and back sheets should be consulted frequently and compared with present conditions. In this way gradual changes can be detected and investigated and insignificant troubles corrected before becoming real ones. Any unusual noises or other irregularities should be logged so that they will be investigated at the regular routine inspections.

INSPECTING REPAIRS

At completion of any adjustment or repair job, always make a thorough inspection to see that all parts have been correctly replaced, that bolts and nuts are tight, and that all cotter pins and locking wires are in place. If work involved rotating parts, bar engine around at least two full revolutions (so that camshaft is turned one revolution) to be sure that all parts are clear. Be sure that no tools or rags are left inside the engine.

2. SMOKY EXHAUST

Smoky exhaust indicates defective combustion which is usually due to one of the following causes:

- (a) Excessive carbon on spray valve tips.
- (b) Leaking spray valve.
- (c) Leaky exhaust, inlet, or air starting valves.
- (d) Buffer springs may be incorrectly adjusted.
- (e) Fuel cam or roller may be worn.
- (f) Leaky or stuck piston rings.
- (g) Uneven cylinder load balance.

TURBO-CHARGER

Maintenance, inspection, general instructions and parts list are contained in a separate booklet usually placed after the parts catalog section of this book. If this booklet is not included, one will be supplied by writing the A.I.D.E. Co., Oakland or the Elliot Co. at Jeannette, Pa. When requesting a new booklet always be sure and give the Turbo-charger Serial Number and the Engine Serial Number.

If exhaust smoke is not even but occurs in the form of puffs it is likely that the combustion is defective in one or two cylinders only. Where the trouble lies can usually be determined by cutting out spray valves one at a time. When this is done however, the engine should not carry more than about 3/4 load or the remaining cylinders will be overloaded.

INSPECTION AND MAINTENANCE ROUTINE

The following routine for regular inspection and maintenance work is suggested as a guide for the operator, but experience with the engine over a period of time may indicate changes that should be made in the schedule.

It will be noted in the following schedules that spray valve cleaning has not been included. It is believed the spray valves should be cleaned only when necessary, rather than at definite intervals. The necessity for cleaning will be indicated by increased or uneven exhaust temperatures or smoky exhaust and at either of these indications the spray valves should be inspected and cleaned, if necessary.

In the following, work to be done under each routine should include work listed under preceding routines. For example, work under "Annual Routine" includes everything listed under all other routines.

4-HOUR ROUTINE

- (a) Hand oil the following points:
 - 1. The inlet and exhaust valve stems.
 - 2. The rocker arms at their fulcrums and at their push rod ends. 3. Inlet and exhaust lifters, fuel wedges, lifter and buffers.
 - 4. Wedge shaft bearings.
 - 5. Tachometer drive. 6. Governor bearing.
 - 7. Bilge pump connecting rod both ends. 8. Mechanical lubricator strap.

For oiling the inlet and exhaust valve stems it is preferable to use penetrating oil. If this is not available a mixture of equal parts of engine lubricating oil and kerosene may be used. (A mixture of two-thirds engine fuel oil and one-third lubricating oil can be used in an emergency.) For all other points in above schedule use engine lubricating oil.

- (b) Check the oil level in the mechanical lubricator. Fill the lubricator with clean engine oil of the grade used in the engine when necessary.
- (c) Turn the handle of the lubricating oil filter.
- (d) Turn the handle of the fuel oil filter.

Always turn filter handles immediately after stopping the engine.

DAILY OR 24-HOUR ROUTINE

- (a) Clean out the sump tanks of the lubricating oil and fuel oil filters.
- (b) Hand oil the air brake.
- (c) On engines equipped with pneumatic control, hand oil the air ram and interlock and grease the control unit shaft with cup grease.

200 TO 300-HOUR ROUTINE

- (a) Check intake and exhaust valve timing.
- (b) Check spray valve timing. balance.) (See Section 0) (After starting engine check cylinder load
- (c) Clean out lubricating oil day tank if lubricating oil is dirty or dark in color.
- (d) Remove crankcase doors and inspect connecting rods. Be sure that all connecting rod bolts are tight and that everything is in order. Inspect lower part of cylinder liner bore.

(e) On engines equipped with waste type filters these may or may not need repacking. The time between packings will vary with the type of lubricating oil used and with the operating conditions to which the engine is subjected. When the lubricating oil turns black rapidly following an oil change, the filter should be repacked.

SEMI-ANNUAL ROUTINE

- (a) Pull cylinder heads and pistons, remove rings and clean pistons and grooves thoroughly. Check rings for side and end clearance.
- (b) Examine cylinder liner walls. Watch for shoulders due to ring travel.
- (c) Grind intake and exhaust valves. Check valve springs for length and tension and for defects.
- (d) Recondition spray valves. Inspect stem packing and repack if necessary. Inspect stem for wear and replace if worn. Inspect and clean spray valve tips. Grind stem to tip.
- (e) Inspect main and connecting rod bearings. Check clearances and inspect bearing surfaces. Adjust clearances if necessary.
- (f) Inspect gear train carefully, observing backlash, indications of wear on teeth, and clearance on intermediate gear bearings.
- (g) Inspect camshaft and latch shaft assemblies. Watch for worn or loose cams, loose or worn rollers or pins on the lifters. Be sure all keys and lock bolts are in place and tight.
- (h) Inspect water pump and renew zinc plug if necessary.
- (i) Inspect engine control parts, adjust and grind valves if necessary.
- (j) Disassemble lubricating oil cooler and inspect for corrosion.
- Clean thoroughly before reassembling. Renew zinc plugs if necessary.

 (k) Check propeller shaft coupling bolts and thrust bearing and flywheel clamp bolts.
- (1) Check all hold-down bolts between engine and foundation. If they are loose check the engine alignment.

ANNUAL ROUTINE

- (a) Check crankshaft and thrust shaft alignment. If shaft needs realignment it is recommended that the work be done by an experienced and careful mechanic.
- (b) Examine cylinder jackets and exhaust manifold water jackets. If scale is over 1/16" thick it should be removed by scale remover solution.
- (c) Remove and inspect lubricating oil and fuel oil transfer pumps. Note conditions of bearings, shafts and seals. Replace if necessary.
- (d) Remove top cover and mounting plate on high pressure fuel pump. Note condition of pump plungers and barrels. Disassemble crossheads and connecting rods and inspect for wear. Inspect suction and discharge valves and grind seats. Check valve lifts.
- (e) Disassemble governor and inspect carefully all moving parts for wear and signs of distress. Inspect entire linkage between governor and wedge shaft for lost motion and wear. Fuel wedges, links and pins should also be inspected for wear and replaced if necessary.
- (f) Inspect Mechanical Lubricator and connections to cylinder liners. Inspect ratchet mechanism for wear and proper functioning. Hand crank lubricator and observe the feed to each liner. Watch for water leaks at the nipples going through the water jackets.
- (g) Clean out crankcase thoroughly. Be sure that all cleaning solution is drained out after cleaning is completed.

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FOREWORD

This Parts Catalog has been compiled to serve the dual purpose of providing a means for ordering parts and to furnish illustrations to aid in the dismantling and reassembling of the various units of the engine.

This Parts Catalog is made to conform to the original construction of the engine, and The National Supply Co. does not assume the responsibility or obligate itself to maintain this catalog to conform to any subsequent changes made on the engine after it leaves the factory. Complete records of all changes and service orders for each engine are maintained at the factory in an effort to always supply correct parts, but due to occasional substitution of parts in the field, of which we have no knowledge, and the fact that we have no assurance that parts furnished from the factory are installed, we cannot guarantee the furnishing of correct parts.

The right is reserved to change the construction or material of any part or parts without incurring the obligation of installing such changes on engines already delivered.

INSTRUCTIONS FOR ORDERING PARTS

Always furnish Engine Number when ordering parts or when communicating with factory or agency. This number will be found on name plate located on operating side of engine. It is <u>VERY NECESSARY THAT THE ENGINE NUMBER BE GIVEN</u> as it helps to insure the furnishing of correct parts and is also the means whereby the factory service records of each engine are maintained.

Always give PART NUMBER, PART NAME AND QUANTITY. If part has no Part Number then give a COMPLETE DESCRIPTION AND SIZE OF PART.

Be particular to state POST OFFICE ADDRESS, TOWN, COUNTY and STATE to which parts are to be shipped.

Specify how merchandise is to be shipped--whether by FREIGHT, EXPRESS or PARCEL POST.

Confirm all Telephone and Telegraph orders in writing.

Claims for shortages or errors must be made within five days from the receipt of goods or same will not be considered.

Broken or damaged goods should be refused, or a complete description made of damage by the carrier agent on the freight bill. If this is done, full damage can generally be collected from the transportation company.

No responsibility is assumed for delay or damage to merchandise while in transit. Our responsibility ceases upon delivery of shipment to the transportation company, from whom a receipt is received showing that shipment was in good condition when delivered to them; therefore, claims if any, should be made with the transportation company and not with The National Supply Co. - Engine Division-Springfield, Ohio

INSTRUCTIONS ON "HOW TO USE PARTS CATALOG"

In order TO LOCATE PART NUMBERS it is IMPERATIVE that the person concerned thoroughly understands the makeup of this book. He should CAREFULLY READ THE INSTRUCTIONS given on this and the following page, and thoroughly familiarize himself with the necessary steps involved. Particularly is this important when sub-assemblies are involved.

DO NOT ORDER PARTS BY REFERENCE NUMBERS as these numbers sometimes change and wrong parts might be supplied.

This catalog is made up of four basic sections, as follows:-

- l. INDEX SHEET -- This sheet lists the various groups into which the engine is divided and must be used for obtaining the group sheet number. This sheet also lists any special parts used on engine.
- 2. GROUP LIST SHEET -- This sheet lists the parts which comprise the group, and are numbered with the prefix "L" or "2L" NOTE Catalog may contain sheets which are not used Use only those sheets listed on index.
- 3 PLATE (OR LINE DRAWING) -- Plates are arranged to face the group sheet to which they apply, and in most cases shows only the parts listed in the group. Occasionally a plate may include two or more groups making it necessary to always first obtain the group number from the index. If this is not done you may by chance turn to a plate showing the part wanted but will not find it listed on the group sheet facing this plate.
- NOTE:---- If no plate is found facing the group sheet, then the part wanted can be identified by the description. This will apply mainly to piping, and in this connection the actual pipe and fittings on the engine should always be measured and then ordered accordingly, due to unavoidable variations between engines.
- 4. SUB-ASSEMBLIES -- The term "Sub-assembly" (or the Word "Assembly" appearing in the part name) is used to indicate parts which are made up of two or more parts (or pieces) and yet must be considered as a unit part. For example, parts that are welded together, parts that have bushings pressed in, or parts that have to be machined together.

 A Sub-assembly list will be found immediately following the last group sheet, and itemizes the various parts used in each assembly. These assemblies are arranged in numerical sequence.
- NOTE: ---- Certain parts of assemblies indicated by an "*" in place of a reference number are not sold individually, and if wanted, the complete assembly must be ordered.

 Sub-assembly lists contains assemblies used on several different engines. Use only assemblies listed on group list sheets.

REFERENCE NUMBERS ON PLATES OR ASSEMBLY DRAWINGS

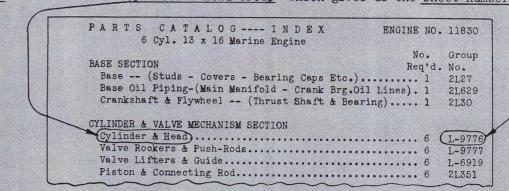
- SINGLE NUMBERS or the TOP NUMBER (when more than one number appears in the circle) refers directly to a corresponding number on the group list sheet.
- A circle with MORE THAN ONE NUMBER indicates part in question is a component part of a sub-assembly. The top number will refer to a corresponding number on the group list sheet, and the lower number will refer to a corresponding number in the sub-assembly.
- TO FIND A PART WITH TWO REFERENCE NUMBERS IN THE CIRCLE PROCEED AS FOLLOWS: (NOTE: Select a part on any plate and follow step by step as explained.)
 - list -- Using the top number in the circle locate corresponding reference number on the group list sheet, which will be an assembly.
 - 2nd -- Using the Part Number of the assembly locate same in the numerical assembly list at rear of book.
 - 3rd -- Refer back to the plate and obtain the second or lower number in the reference circle, then locate this number in the reference number column of the sub-assembly, and this will be the part desired.
- If there are MORE THAN TWO NUMBERS in the reference number circle, proceed exactly as outlined above, only this time the part in the first assembly located will be another sub-assembly, so therefore it will be necessary to find the second assembly, and then referring back to the plate take the third number in the reference circle and match it with the corresponding number in the second assembly.

The following page will show a typical example and illustrate the above explanation step by step.

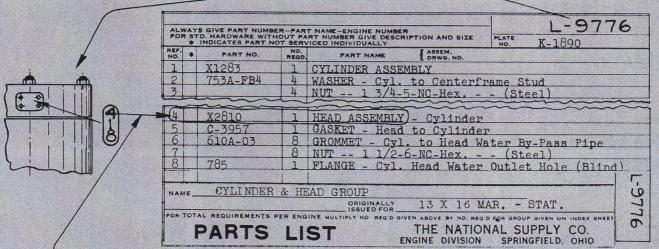
The following illustrated example will show the procedure as explained on opposite Page, for finding parts involved in sub-assemblies.

For this illustration assume that the part number for the Cylinder Head Cleanout Cover is wanted:-

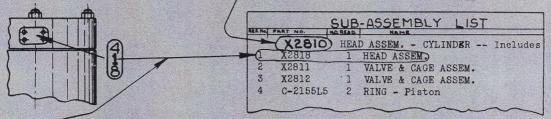
We know that this cover would be listed with the "Cylinder Head" so we turn to the Index Sheet and locate the "Cylinder & Head Group" which gives us the sheet number.



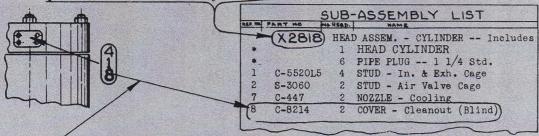
We find the sheet number for this group to be L-9776, and now we turn to this sheet and opposite we find a Plate or group drawing.



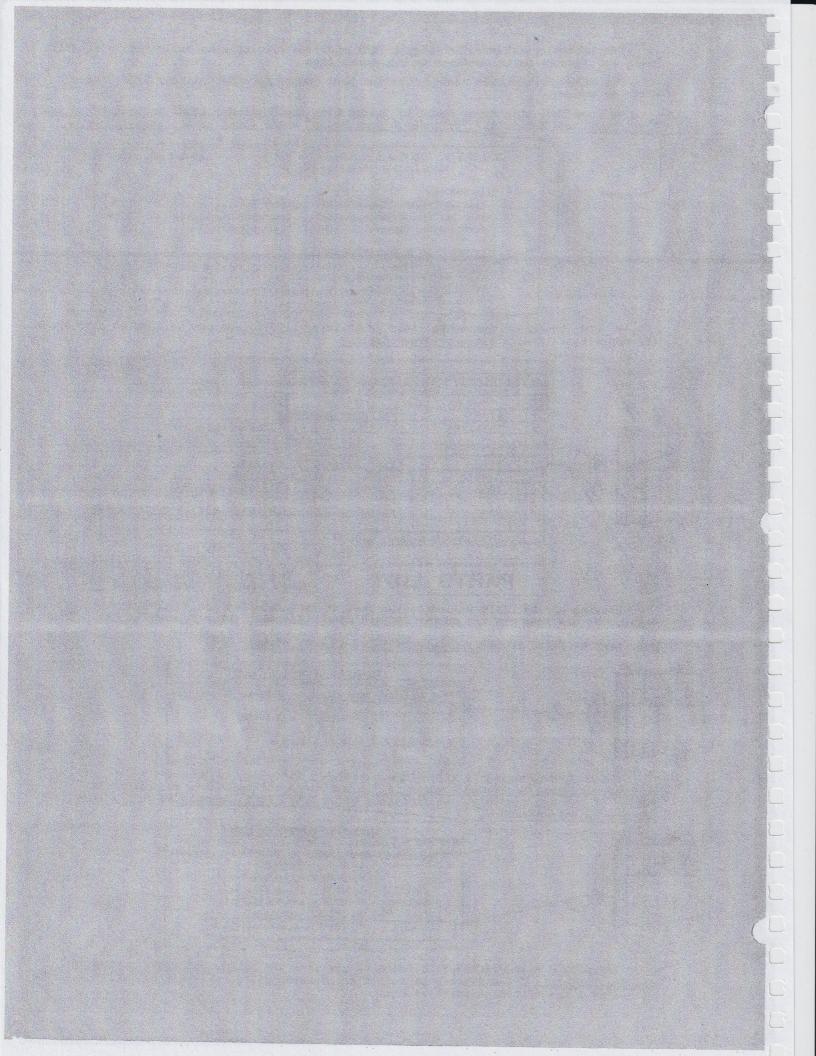
Looking at the Plate we locate the part we want and find the reference number to be 4-1-8. We now take the top number "4" and match this with the reference number "4" on the group list sheet. We find this to be X2810 Head Assembly, so that this assembly must next be found in the sub-assembly list at rear of book.



After finding assembly X2810 in sub-assembly list, we now take the second of the reference numbers in the oval which is "1" and match this with the corresponding number of the sub-assembly. We find this to be X2818 Head Assembly so we now have to proceed to this assembly.



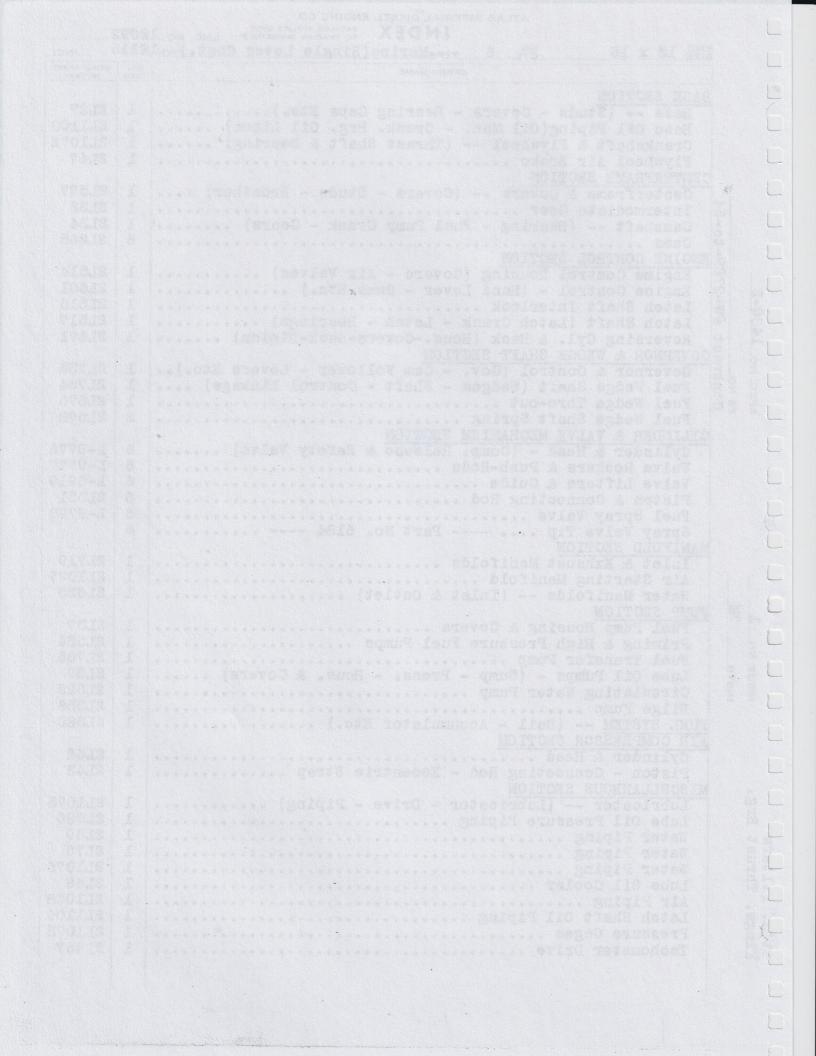
After this assembly X2818 is found we now take the <u>bottom reference number in</u> the <u>oval which is "8"</u> and match this with the corresponding reference number in X2818. We now have the unit part which we want.

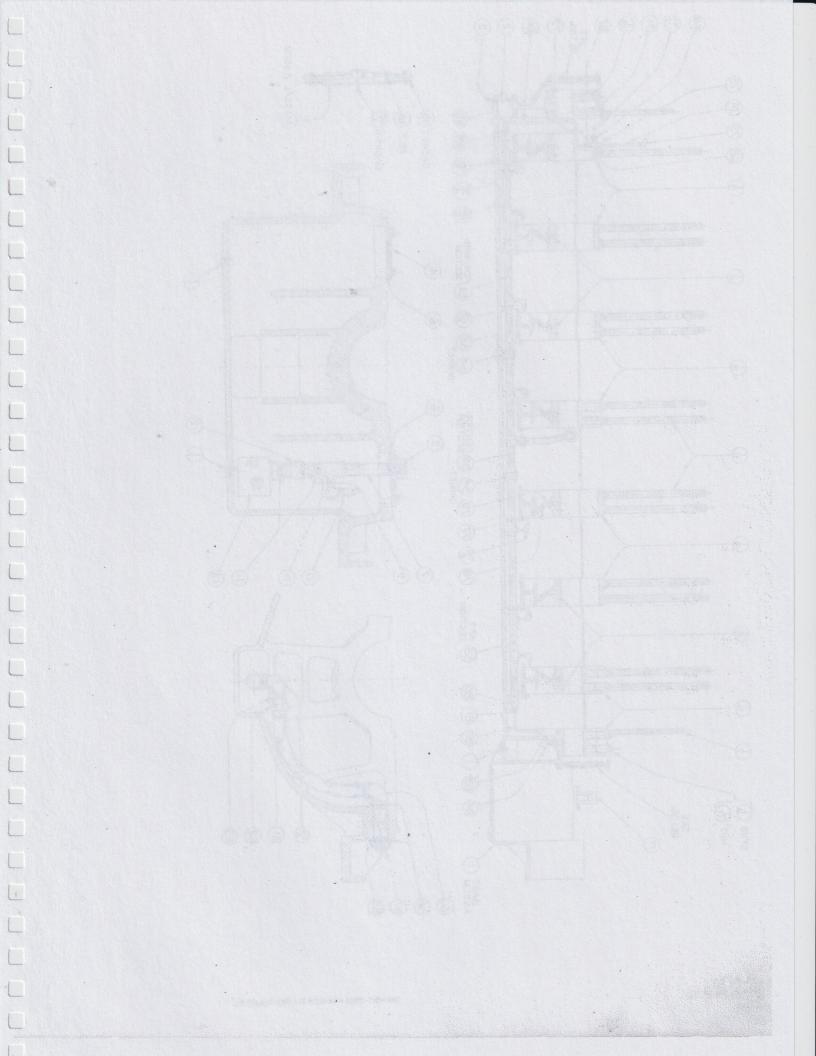


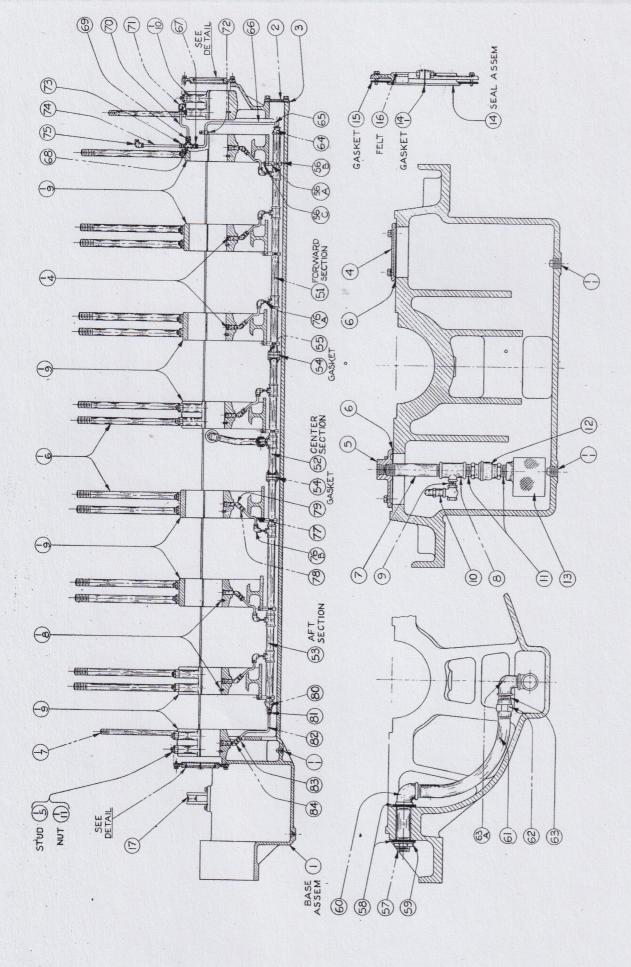
CATALOG APPLIES ONLY TO ENGINES INDICATED INDEX ENG. NO. 12092 TypeMarine(Single Lever Cont.) To 12115 ENG. 13 x 16 BASE SECTION Base -- (Studs - Covers - Bearing Caps Etc.)...........
Base Oil Piping(Oil Man. - Crank. Brg. Oil Lines) 1 2L27 2L1108 Crankshaft & Flywheel -- (Thrust Shaft & Bearing) 1 2L1072 Flywheel Air Brake 1 2L47 CENTERFRAME SECTION Centerframe & Covers -- (Covers - Studs - Breather) 1 2L577 2L33 Intermediate Gear 1 5 Camshaft -- (Bearing - Fuel Pump Crank - Gears) 2L34 2L265 ENGINE CONTROL SECTION 1 2L514 1 21.601 Latch Shaft Interlock 1 2L516 Latch Shaft (Latch Crank - Latch - Bearings) 2L517 Reversing Cyl. & Rack (Hous.-Covers-Rack-Pinion) 2L491 1 GOVERNOR & WEDGE SHAFT SECTION 1 21.733 1 2L734 1 2L676 SES Fuel Wedge Shaft Spring 21678 CYLINDER & VALVE MECHANISM SECTION Cylinder & Head - (Comp. Release & Safety Valve) L-9776 Valve Rockers & Push-Rods L-9777 6 Valve Lifters & Guide L-6919 Piston & Connecting Rod 21351 6 L-9778 6 Spray Valve Tip --- Part No. 6184 ---- MANIFOLD SECTION . Inlet & Exhaust Manifolds 2L719 2L1027 1 2L623 一門 PUMP SECTION Fuel Pump Housing & Covers 2L37 Priming & High Pressure Fuel Pumps 1 2L534 Fuel Transfer Pump 2L705 Lube Oil Pumps - (Sump - Press. - Hous. & Covers) 1 2L39 Circulating Water Pump 1 2L525 Bilge Pump 2L356 FUEL SYSTEM -- (Rail - Accumulator Etc.) 1 2L380 AIR COMPRESSOR SECTION Cylinder & Head 2142 Piston - Connecting Rod - Eccentric Strap 2L43 1 MISCELLANEOUS SECTION 2L1073 Lubricator -- (Lubricator - Drive - Piping) 1 Lube Oil Pressure Piping 1 2L580 Water Piping 1 2169 Water Piping 1 2L70 Water Piping 1 2L1076 Lube Oil Cooler 2L66 Air Piping 1 2L1028 Latch Shaft Oil Piping 1 2L1109 Pressure Gages 2L1075

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ALWAYS GIVE PART NU	BER-P	ART NAME-ENGINE NUMBER PART NUMBER GIVE DESCRIPTION AND SIZE PLATE No. 100 19
DRWG NO BEFT ART NO.	NO.	PART NAME ASSEM. DRWG. No. K-1718
1 71 12774	1	BASE ASSEMBLY
2 F-6112 3 ZC1282		GASKET - Cover to Base
4 1111		CAPSCREW 1/2-13-NC x 1 1/4 Lg (St.)
4 201279	6	LOCKWASHER 1/2 SAE Reg (St.) COVER - Base Oil Sump Hole - (Blind)
7 / 5/ 201278 8 / 6 201280	2	COVER - Base Oil Sump Hole - (Strainer Side)
8 7 6 2C1280 5 7 6 2C1280	8	CAPSCREW 3/8-16-NC x 1 Lg (St.) '
10 / /		LOCKWASHER 3/8 SAE Reg (St.)(NIPPLE 1 1/4 x 7 1/2 Lg (Brass)
T 10 11 18 8	1	TER 1 1/4 x 1 1/4 x 1/2 Std. Reducing (Brass
14 / 10 PG21L 1/2	1 1	CLOSE NIPPLE •• 1/2 Std. • (Brass) VALVE • Pressure Relief • (35 LbV)
15 // // 11	2.	CLOSE NIPPLE 1 1/4 Std (Brass)
7 16 0-9066 12 0-90669111/ 17 201/272 13 x2775	1	VATAR - Check STRAINER ASSEM Lube Oil
18 / 14 X582 15 C-295	2 2	SHAL ASSEM Crankshaft Oil GASKET - Oil Seal to Base
3 0-295	24	CAPSCREW - 3/8-16-NC x 1 Lg (St.) / 1
L6 0-3379		LOCKWASHER 3/8 SAE Reg (St.)
1/23 T-5948	2	BRACKET - Barring Over
1 29 35	8	CAPSCREW 3/4-10-NC x 2 Lg (St.) LOCKWASHER 3/4 SAE Reg (St.)
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		ORIGINALLY 6 C.VI. 13 x 16 MARINE
ORM 240 REV. 1/46 2M TRANS.	PER EN	IST ATLAS IMPERIAL DIESEL ENGINE CO.
PINTED IN U.S.A.	<u></u>	OAKLAND, CALIF. MATTOON, ILL/A

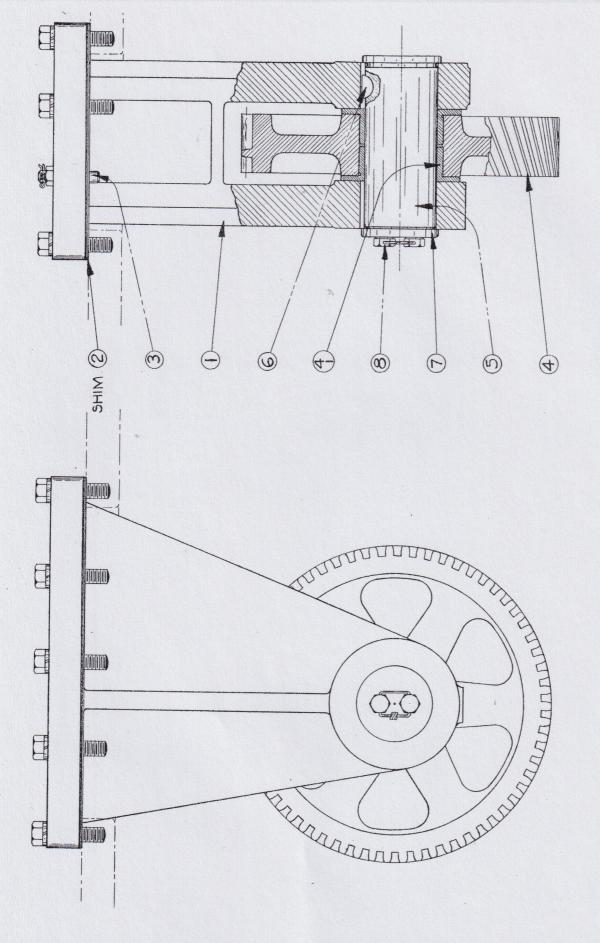


PLATE No. W-1656

DO NOT ORDER PARTS BY REF. NUMBERS

Retyped from sheet dated 4-28-49. 2L33 ALWAYS GIVE PART NUMBER - PART NAME - ENGINE NUMBER W-1656 FOR STD. HARDWARE WITHOUT PART NUMBER GIVE DESCRIPTION AND SIZE DRWG NO PART NO PART NAME BEARING - Intermediate Gear W-1500 SHIM - Bearing to Centerframe - (1/64) C-1210-C C-1210 2 SHIM - Bearing to Centerframe - (.003) C-1210 2 C-1210-E 12 CAPSCREW - 5/8-11-NC x 2-1/2 Lg. - (St.) 12 LOCKWASHER - 5/8 SAE Reg. - (St.) 5 PIN - Bearing to Centerframe Dowel C6633L2-1/2 C - 6633HALF NUT - 1/2-13-NC-Hex. - (St.) 7 COTTER PIN - 1/16 x 3/4 Lg. - (St.) 9 GEAR ASSEM. - Intermediate X2782 F-6125 4 PIN - Intermediate Gear 201287 5 11 WOODRUFF KEY - 1/4 x 1 Std. - (St.) . ? 6 WASHER - Pin Retainer CAPSCREW - Washer to Pin 13 7 C-8202 1 C-2408 8 C2408L-7/8 WIRE - #16 Ga. x 5 Lg. - (St.) 15 ; 17 19 0 21 2 1 25 6 27 3 29 0 31 2 33 4 35 B 37 8 39 0 41 2 43 14 16 47 18 49 50 INTERMEDIATE GEAR GROUP P. HAND SEE ORIGINALLY ISSUED FOR 6 CYL. 13 x 16 MARINE FOR TOTAL REQUIREMENTS PER ENGINE MULTIPLY NO. REQ'D GIVEN ABOVE BY NO. REQ'D FOR GROUP GIVEN ON INDEX SHEET THE NATIONAL SUPPLY CO. PARTS LIST

ENGINE DIVISION SPRINGFIELD, OHIO

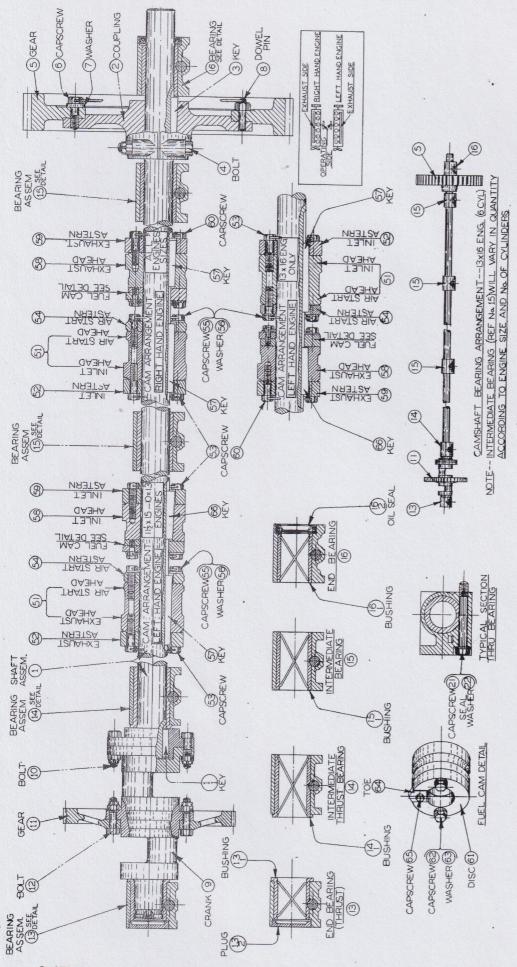


PLATE NO. (ED.4) DO NOT ORDER PARTS BY REF. NUMBERS

Retyped from sheet dated 2-28-47. "1-4-6-54 -Added Part # Line26

2L34

ALWAYS GIVE PART NUMBER -- PART NAME -- ENGINE NUMBER

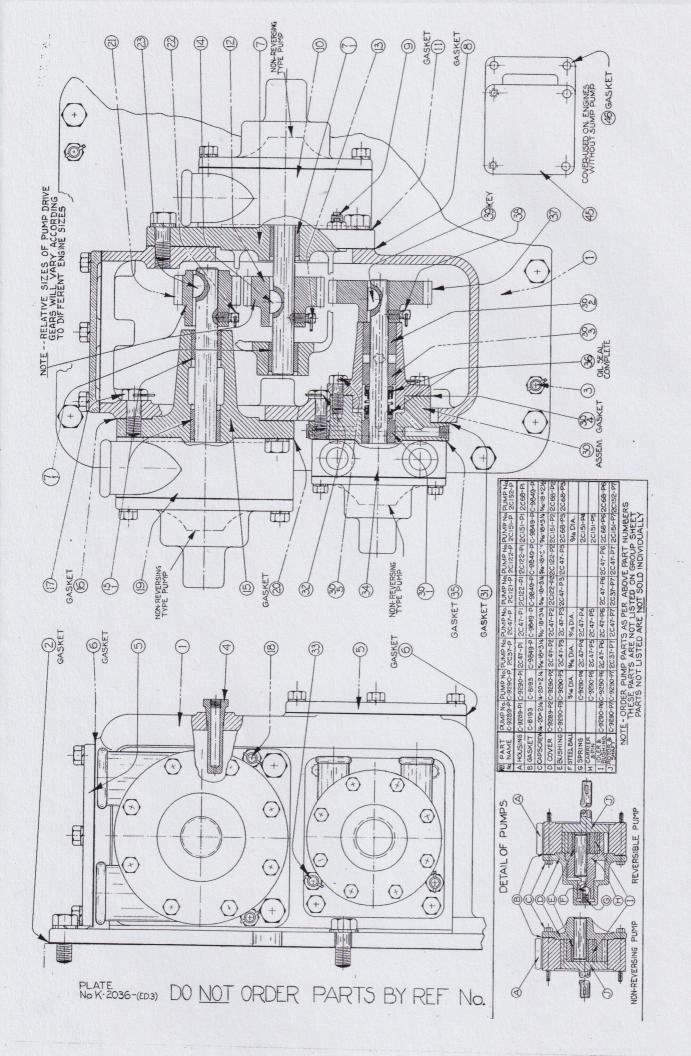
PLATE (See Note Below)

		FOR STD. H	THE RESERVE THE RESERVE THE PERSON NAMED IN	PART NO	PART NAME ASSEM NO. K-1719
	DRWG. NO.	NO	PART NO	REO'D.	
1	F-5891	1	X532	1	CAMSHAFT ASSEMBLY
	0 8300	2	W-1501	1	HUB - Camshaft Gear
3	C-7108	3	C-7108L4	1	KEY - Hub to Camshaft
	C-2510	4	C2510L41/2	2	BOLT - Camshaft Gear Hub Clamp
,	***			2	CASTLE NUT - 5/8-18-NF-Hex (St.)
O'COL		_		2	COTTER PIN - 1/8 x 1-1/4 Lg (St.) GEAR - Camshaft Drive
7			F-6127	1	GEAR - Camshaft Drive
	C-2410	6 (C2410L1-3/4	6	CAPSCREW - Gear to Hub
-	C-6160	7	1222A-C3	6	WASHER - Gear to Hub Capscrew
	C-6633	8	C-6633L2	2	PIN - Gear to Hub Dowel
				2	HALF NUT - 1/2-13-NC-Hex (St.)
			,	1	WIRE - (Capacrew & Dowel) - 16 Ga. x 39Lg (SCRANK ASSEM H.P. Fuel Pump
		9	X2783	1	CRANK ASSEM H.P. Tuel Pump
	C-2608	10	C-2608L2	4	BCLT - Crank. to Camshaft Coupling
,				4	CASTLE NUT - 1/2-20-NF-Hex (St.)
				1	WIRE - #16 Ga. x 18 Lg (st.)
			F-6109	1	GEAR - Lube & Fuel Pump Drive
	C-2608	12	C-2608L2	4	BOLT - Gear to Crank
)				4	CASTLE NUT - 1/2-20-NF-Hex (St.)
				1	WIRE - #16 Ga. x 18 Lg (St.)
	201334	13	X2784	1	BEARING ASSEM Fuel Pump Crank- (End-Thrust
3	C10004		X2834	1	BEARING ASSEM Camshaft - (Pump End-Thrust)
	C-1342	15	G680-C	6	BEARING ASSEM Camshaft
	C-7919	16	X2074	1 1	BEARING ASSEM Camshaft - (Gov. End)
			3 A3305	9	CAPSCREW -5/8-11-NC- x 4-1/2 Lg(St.)
7	The second secon	22	C-4921	9	WASHER - Camshaft Brg. Bolt Saal
)					
)	a to be and a control of the control				
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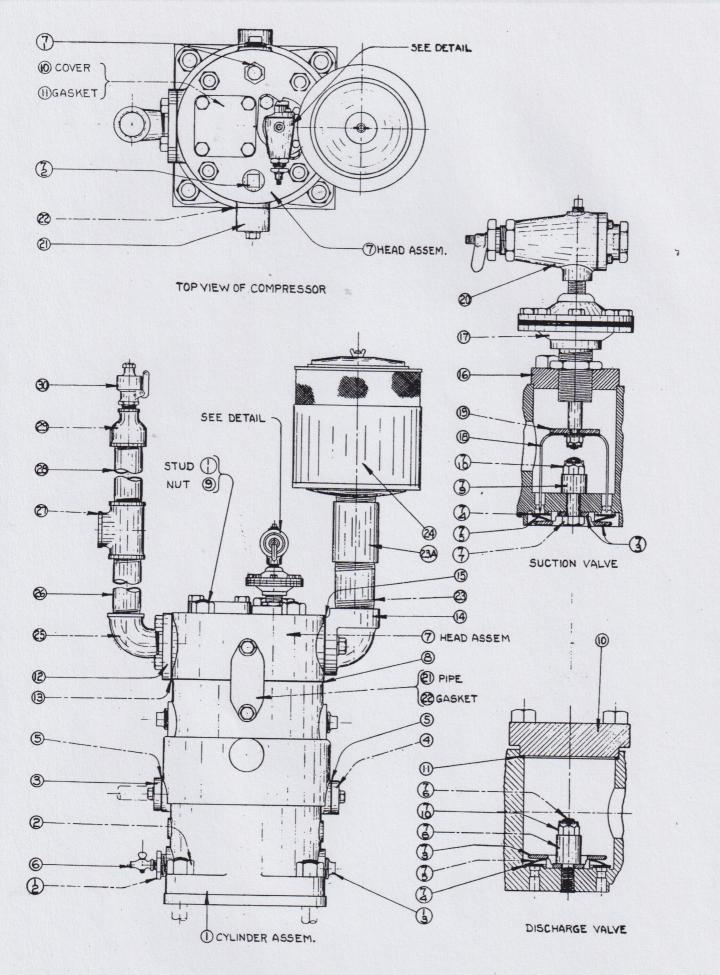
5					
			The College of Section (Section 1987) and the College of Section (Sectio		
7			ano 629 we 439	PA	RTS CATALOG NOTE
		Tie	a Plate No		RTS CATALOG NOTE Warine Engines (Non Turbo A
9	-	Ila	e Plate No	K-23	56 for Stationary Engines (Non Turbo.)
-		IIa	e Plate No	K-27	09 for Marine - Turbo - Charged.
_		1			
	35	NAME CA	MSHAFI & FUE	L PU	MP CRANK GROUP ORIGINALLY 6 CYI. 13 x 16 MARINE R H
35	e cee	OR TOTAL	DECLUREMENTS PER E	NGINE	ORIGINALLY 6 CYL. 13 X 16 MARINE R.H. AULTIPLY NO. REQ'D GIVEN ABOVE BY NO. REQ'D FOR GROUP GIVEN ON INDEX SHEET

LIST

THE NATIONAL SUPPLY CO. ENGINE DIVISION SPRINGFIELD, OHIO



etyp	d from	9/1	-43 (No chan	ges	
L,	<i>H</i>	1	- y -	, T	
					
					2139
ALWAYS GIVE PART NUMBER-					PART NAME—ENGINE NUMBER PART NUMBER GIVE DESCRIPTION AND SIZE PLATE NO. K-1898 K-2036
LINE NO.	DRWG. NO.	REF.	PART NO.	NO.	PART NAME ASSEM.
1		1	K-1706	1	HOUSING - Rotary Pump Drive
_ 2	9 4	2	_2C1211	V	GASKET - Housing to Centerframe
3			1/	11	CAPSCREW 1/2-13-NC x 1 1/4 Lg (St.)
- 4				10	LOCKWASHER 1/2 SAE Reg (St.)
1 3			m morned mis	1	PLAIN WASHER 1/2 SAE Std (St.) PIN - Housing to Centerframe Dowel
6 7	C-7950	3	0-7950L1 5/8	2	HALF NUT 3/8-24-NF-Hex (St.)
8				2	
9		4	201319	1	NOZZLE - Pump Gear Lube Oil
10		5	201205	2	COVER - Pump Housing - (Top & Side) X
11	V.	6	201206	2	GASKET - Cover to Housing
12				18	CAPSCREW 3/8-16-NC x 7/8 Lg (St.)
13				18	LOCKWASHER 3/8 SAE Reg (St.)
14	070	17	X2791	1	ADAPTOR ASSEM Lube Press. Pump
16	201219	8	201217	1	GASKET - Adaptor to Housing
$\frac{10}{17}$			60464	3	CAPSCREW 1/2-13-NC x 1 1/4 Lg (St.)
18				3	LOCKWASHER 1/2 SAE Reg (St.)
19	C\$8265	9	C-8265L1	3	PIN - Adaptor to Housing Dowel
20					
21		-		-	10.174.1700 W 7. TO
22	2037	10	2037-P	3	PUMP - Lube Pressure GASKET - Pump to Adaptor
23	C-9849	1	C-9849-P	8	CAPSCREW 5/16-18-NC x 3 1/4 Lg (St.)
r 25		7		8	LOCKWASHER 5/16 SAE Reg (St.).
26	1	12	201218	1	GEAR - Lube Press. Pump Drive
27		13	202502	1	SETSCREW Cear to Pump Shaft
28		14		1	WOODRUFF KEY 3/16 x 3/4 Std (St.)
29	1 2 4	1-1-		11	WIRE #16 Ga. x 8 Lg (St'.)
$\frac{30}{31}$	201221	115	X2793	17	ADAPTOR ASSEM Lube Sump Pump
$\frac{31}{32}$	THE RESIDENCE AND ADDRESS OF THE PARTY OF TH	16	201810	1	GASKET - Adaptor to Housing
33	C-2408	17		4 2	CAPSCREW - Adaptor to Housing
34				1	WIRE #16 Ga. x 12 Lg (St.)
35		1		2	CAPSCREW 1/2-13-NC x 1 1/4 Lg/ (St-)
36	- de la companya della companya della companya de la companya della companya dell	30	a cocceta	2	PIN - Adaptor to Housing Dowel
	048265	18	C-8265L1	2	PIN - Adaptor to Housing Dowel
39				+	
40		119	2047-P	1	PUMP - Lube Sump
41	C-9849	20	C-9849-P	3	GASKET - Pump to Adaptor
42				8	CAPSCREW 5/16-18-NC x 3 1/4 Lg (St.)
43				18	LOCKWASHER 5/16 SAE Reg (St.)
44		21	201220	++	GEAR - Lube Sump Pump Drive
46	-17	22	202502	9	WOODRIFF KEY - 3/16 x 3/4 Std - (St.)
47		100		77	WIRE #16 Ga x 8 Lg (St.)
48					
H 49					1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
50		4 -	1 -		TO A MONOTHIN CHOND
2L4	O	NAI	E LUBE OIL	PU	ORIGINALLY 6 CYL. 13 x 16 MARINE -R.H.
THE ANALYSIS AND ANALYSIS OF THE PERSON OF T	OTABEE	FOR	TOTAL REQUIREMENTS	PER I	ENGINE MULTIPLY NO. REO'D GIVEN ABOVE BY NO. REO'D FOR GROUP GIVEN ON INDEX SHEET
1 200	REV. 1/46 2M TRANS		PARTO	3 1	CT. ATLAS IMPERIAL DIESEL ENGINE CO.
N N ED I) U.S.A.	11.17	1 1 11 1 7		OAKLAND, CALIF!



1 4	TYPED DLC DATE 5-3-49 CHKD 188UED LEW DATE 5-7-47							
	Retyped from 10-23-43 (no changes)							
	#3							
	The state of the s							
	2L42							
			FOR S	YS GIVE PART NUME TD. HARDWARE WIT	BER-	PART NAME—ENGINE NUMBER PART NUMBER GIVE DESCRIPTION AND SIZE PLATE NO. PLATE		
L	LINE NO.	DRWG, NO.	REF.	PART NO.	NO.	PART NAME ASSEM. W-1235		
	1		1	G900-J	1	CYLINDER ASSEM Air Compressor		
_	2		2	A 7706	4	NUT 7/8-9-NC-Hex (St.)		
	3	C-491	3 4	C=3306 783	1	FLANGE - Water Inlet (Blind)		
	-5	0-101	5	S-2332	2	GASKET - Flange to Cylinder		
L	6				4	CAPSCREW3/8-16-NC x 1 Lg (St.)		
1	7					LOCKWASHER 3/8 SAE Reg (St.)		
	8	C-9045	6	C-9045P 1/4	1	COCK - Tee Handle Air (Water Drain)		
L	10		7	X1117	1	HEAD ASSEM Cylinder		
	11	S-901	8	901A-J	1	GASKET - Head to Cylinder		
_	12		9		4	NUT 3/4-10-NC-Hex (St.)		
	13		10	F-1695	1	COVER - Discharge Valve Hole		
	14		11	S-1733	1	GASKET - Cover to Cyl. Head CAPSCREW - 1/2-13-NC x 1 1/4 Lg (St.)		
L	16		12	C-5279	i	FLANGE - Air Comp. Discharge Pipe		
1	17		13	C-4026	1	GASKET - Flange to Cyl. Head		
	18				4	CAPSCREW 5/8-11-NC x 1 1/2 Lg (St.)		
	19		14	201212	<u> 1</u> _	ELBOW - Air Comp. Suction Pipe		
	20		15	S-2329	1	GASKET - Elbow to Cyl. Head CAPSCREW 5/8-11-NC x 1 1/2 Lg (St.)		
L	21				2	LOCKWASHER 5/8 SAE Reg (St.)		
1	23		16	C-9160	ĩ	FIANGE - Suction Valve Unloader Adaptor		
1	24				2	CAPSCREW 1/2-13-NC x 1 Lg (St.)		
	25	C-9158	1	C-9158P	1	DIAPHRAGM - Suction Valve Unloader		
	26		18	S-1397	1	PRONG - Suction Valve Unloader		
	27		19	C-8222	+	WASHER - Unloader Prong Retainer (Upper) PLAIN WASHER 1/4 SAE Std (St.)		
_	29				i	CASTLE NUT1/4-28-NF-Hex (St.)		
	30				1	COTTER PIN 1/16 x 1/2 Lg (St.)		
	31	C-9159	20	C-9159P	1	PILOT - Suction Valve Unloader		
	32		07	77 4 37	-	DIDII Owl to Hond Hoton Dy Dogs		
	33	S-1710 S-618	55	34-X 610A-X	1	PIPE - Cyl. to Head Water By-Pass GASKET - By-Pass Pipe		
	35	2-010	HA	OLUARA	2	CAPSCREW 1/2-13-NC x 2 Lg (St.)		
	36		1		2	LOCKWASHER 1/2 SAE Reg. = (St.)		
	37			<u> </u>				
	38	+	0.5		7	Compressor Suction NIPPLE 2 x 4 1/2 Lg (W.I.)		
1	39		23 23A		1	COUPLING - 2 Std. Pipe (M.I.)		
(202467	24	2C2467P	1	AIR CLEANER		
L	42		,			Compressor Discharge		
	43	+	25		1	STREET ELL 1 1/4 Std (M.I.)		
	44		26		1	NIPPLE 1 1/4 x 6 Lg (W.I.)		
1	46	<u> </u>	27		1	TEE 1 1/4 Std (M.1.) NTPPLE 1 1/4 x 8 Lg (W. I.)		
	47	1	29		i	REDUCING(Bell)-1 1/4 x 1/2 std (M.I.)		
	48	C-9974	30	C-9974P 1/2	1	VALVE - Pop Safety		
	49		<u> </u>		+	1		
26	50 OPP. HA	AND SEE		AIR COMPRE	330	OR CYLINDER & HEAD GROUP (6")		
L			NAM	E MAIL OOM MI		ORIGINALLY ISSUED FOR 13 x 16 MARINE		
DA	OPP. RO	M. SEE	FOR TO	OTAL REQUIREMENTS F	ER E	NGINE MULTIPLY HO HEG D GIVEN ABOVE BY NO. REG'D FOR GROUP GIVEN ON INDEX SHEET,		
	M 240 R	EV. 24/1M TRANS. U.S.A.		PARTS	L	IST ATLAS IMPERIAL DIESEL ENGINE CO.		

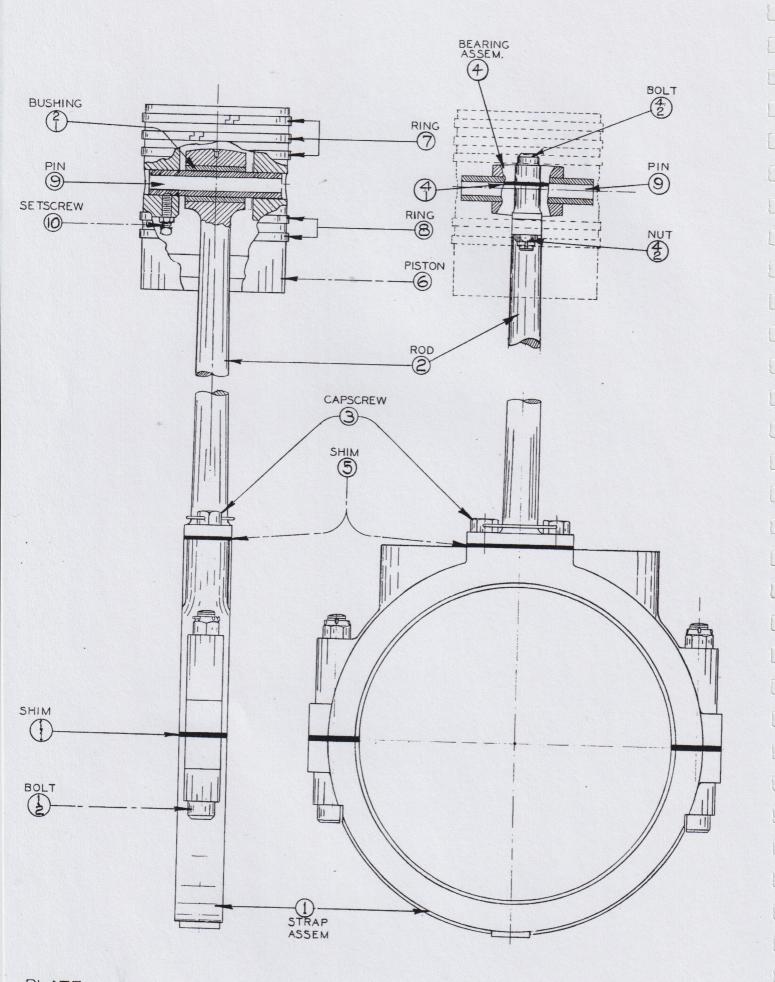
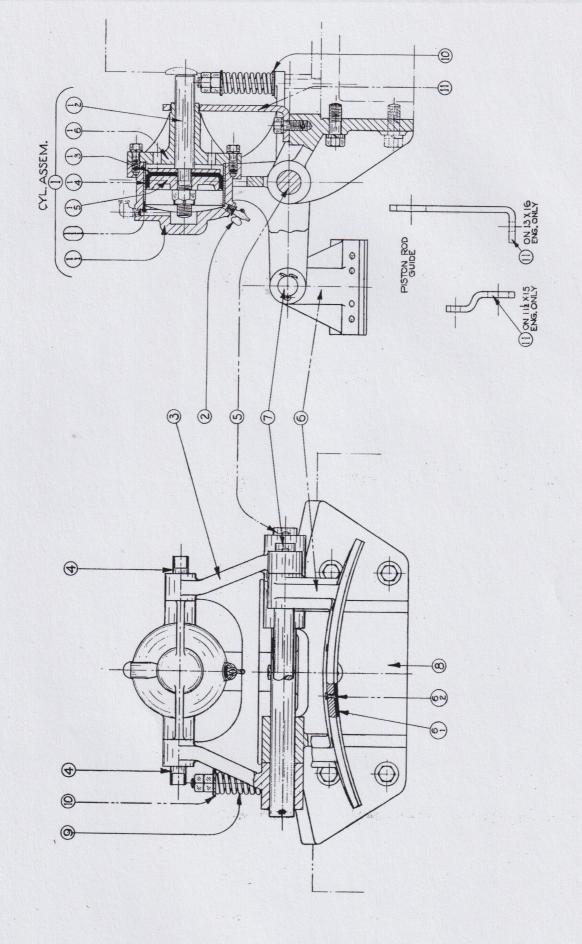


PLATE No. W-1671 (ED.2) DO NOT ORDER PARTS BY REFERENCE NUMBERS

Retyped from 9-21-39 (No changes) "3 ALWAYS GIVE PART NUMBER—PART NAME—ENGINE NUMBER
FOR STD. HARDWARE WITHOUT PART NUMBER GIVE DESCRIPTION AND SIZE
* INDICATES PART NOT SERVICED INDIVIDUALLY PLATE NO. W-1673 NO. PART NO. DRWG. NO. 1 STRAP ASSEM. - Air Comp. Eccentric F-3266 1 G930-03 1 1 ROD - Connecting 929-03 F-6580 2 CAPSCREW C-2412 3 C-2412Ll 3/4 WIRE -- #16 Ga. x 10 Lg. - (St.) 4 BEARING ASSEM. - Piston Pin 5 G130-4 F-6605 2 COTTER PIN -- 1/8 x 1 Lg. - (St. 6 11 SHIM - Rod to Eccentric Strap (1/32) 7 0-4432-B 0 - 44325 SHIM - Rod to Eccentric Strap (.010) 8 C-4432 5 0-4432-D 9 PISTON 10 F-3097 925-J6 6 RING - Piston C-2155L6 11 7 C-2155 RING - Piston C-2455L6 12 C-2455 8 PIN - Piston 13 927-J6 C-1075 9 1 SETSCREW -- 3/8-16-NC x 1 Ig. -Sq. Hd. Cup Pt. (St.) 10 14 1 NUT -- 3/8-16-NC-Hex. -- (St.) 15 10 16 17 18 19 21 22 23 25 26 27 28 29 31 83 34 35 36 37 38 40 41 42 43 44 45 46 47 48 49 50 PISTON RULL ORIGINALLY ISSUED FOR ROD & STRAP CHOUP COMPRESSOR REQ'D FOR GROUP GIVEN ON INDEX SHEET FOR OFF. ROT. SEE AS IMPERIAL DIESEL ENGINE CO. MATTOON, ILL. OAKLAND, CALIF

DATE 11-24-44 CHKD.



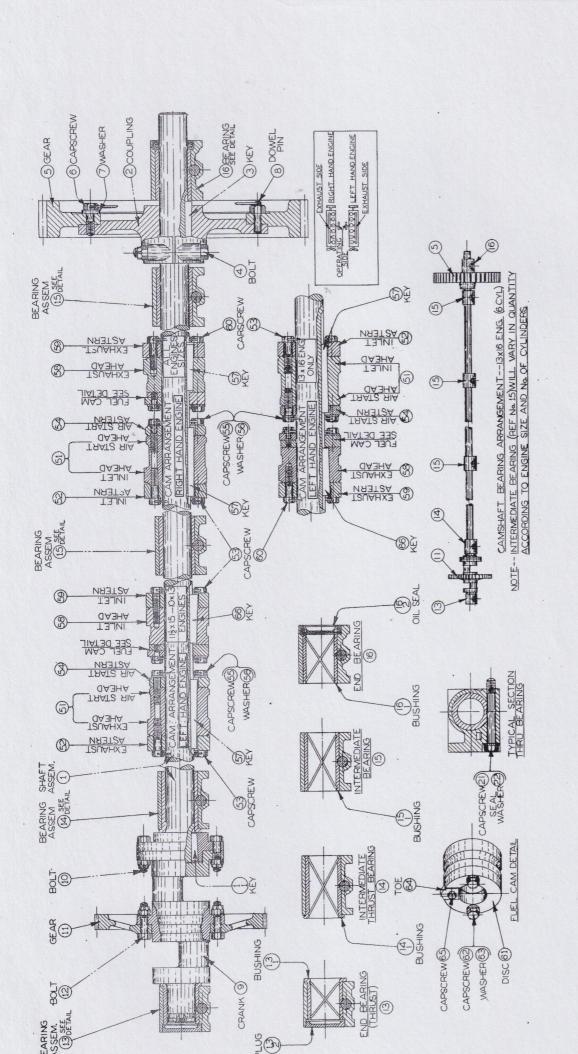
	ТУРЕ	CB DATE 10-23-43 CHKD. DATE BY APRVD.	
etyped from	9-27-39 (No Chan	ges)	
		. O	
		O HA N	
		2L47	
	ALWAYS GIVE PART NUMBER- FOR STD. HARDWARE WITHO * INDICATES PART NOT SE	PART NAME—ENGINE NUMBER UT PART NUMBER GIVE DESCRIPTION AND SIZE PLATE K-1824 NO. K-1824	
LINE DRWG. NO.	REF. PART NO.	NO. PART NAME ASSEM. DRWG, NO.	
1	1 X2797	1 CYLINDER ASSEM Fly. Air Brake (& Piston)	
2 C-9045	2 C-9045-P 1/4 3 F-6031	1 COCK - Air 1 LEVER - Brake Shoe	
4	4 S-2620	2 PIN - Air Brake Cyl. To Lever	
5	5 S-2635	1 SHAFT - Brake Shoe Lever to Post 2 COTTER PIN 1/4 x 2 Lg (St.)	
7	6 X549	1 SHOE ASSEM Fly. Air Brake	
8:	7 S-2636	1 SHAFT - Brake Shoe 2 COTTER PIN 1/4 x 1 3/4 Lg (St.)	
$\frac{9}{10}$	8 W-1428	1 POST - Flywheel Air Brake	
11		5 CAPSCREW 3/4-10-NC x 2 Lg (St.)	
12 13: C=326	9 582-E	5 LOCKWASHER 3/4 SAE Reg (St.) 1 SPRING - Brake Shoe Lever	
$\begin{bmatrix} 13 & G-326 \\ 14 \end{bmatrix}$	10 C-7948	2 WASHER - Spring Retainer	
15	77 5043	2 NUT 5/8-11-NC-Hex (St.) 1 GUIDE - Piston Rod	
16 2C3187	11 5941	1 CAPSCREW 1/2-13-NC x 3 Lg (St.)	
18		1 LOCKWASHER 1/2 SAE Reg (St.)	
$\frac{19}{20}$			
21			
22 23	1		
$\frac{23}{24}$			
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R OPP.HAND SEE	NAME FLYWHEEL A	IR BRAKE GROUP ORIGINALLY 6 CYL. 13 x 16 MARINE -R.H.	
2L48	FOR TOTAL REQUIREMENTS PE	ASSUED FOR THE TOP CROWN ON INDEX SHEET	
40 REV, 5-42 1M TRA	PARTS	I ICT ATLAS IMPERIAL DIESEL ENGINE CO.	
1M BONI		OAKLAND, CALIF. MATTCON, ILL.	
	1000000		

		ALWA	YS GIVE PART N	UMBER-	-PART NAME-ENGINE NUMBER	
INE	DRWG. NO.	FOR S	PART NO.	NO.	PART NUMBER GIVE DESCRIPTION AND SIZE No.	,
1	DRWG. NO.	NO.	201342	REQD.	BRACKET - Oil Cooler	~~~~
2			EV MY TH	6	CAPSCREW 1/2-13-NC x 1 1/4 Lg (St.) LOCKWASHER 1/2 SAE Reg (St.)	
3	y a representative in gent anything \$ 600% of months of the			6	LOCKWASHER 1/2 SAE Reg (St.)	
4					The state of the s	
5		4	2C49P	1	OIL COOLER	
6			t a district May in which drives whiten, indicated by a first an extending of print the following in the parties of	4	CAPSCREW 3/8-16-NC x 1 Lg (St.) PLAIN WASHER 3/8 SAE Std (St.)	
7 8		+		**	Linui madrint - Of Child South - (South	
9						
10			garage in Private Mills and Employment reporting more action. Supplied the first to			
11						
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					GROUP * * (ROSS COOLER)	-

5 TO	TYPED MED DATE 8-2-43 CHKD M & DATE BY APRYSE
Revised & Added Pip	Retyped from 12-26-39 - W
	e Clamps
	ALWAYS GIVE PART NUMBER—PART NAME—ENGINE NUMBER 2L69
	FOR STD, HARDWARE WITHOUT PART NUMBER GIVE DESCRIPTION AND SIZE * INDICATES PART NOT SERVICED INDIVIDUALLY PLATE NO.
NO. DRWG. NO.	REF. PART NO. NO. PART NAME ASSEM. A=238
2	Water Pump to Inlet Manifold 1 NIPPLE 2 x 6 1/2 Lg (Galv. Iron)
3	1 ELBOW 2 Std (M.I.)(Galv.)
. 5	1 NIPPLE 2 x 6 Lg (Galv. Iron) 1 TEE 2 x 1 1/4 x 2 Std. Reduc.(M.I.)(Galv.)
6	1 CLOSE NIPPLE 1 1/4 Std (Galv. Iron)
8	1 TEE1 1/4 x 1 1/4 x 3/4 Std. Reduc. (M.I.) (Galv.)
- 8 9 2C10	1 CLOSE NIPPLE 1 1/4 Std (Galv. Iron) 2010-P1 1/4 1 RELIEF VALVE
	1 NIPPLE 2 x 4 1/2 Lg (Galv. Iron)
11 C-9054	C-9054-P2 1 COCK - Three Way 1 NIPPLE 2 x 2 3/4 Lg (Galv. Iron)
13	Three Way Cock to Cooler
14	1 NIPPLE 2 x 6 Lg (Galv. Iron)
16	1 ELBOW 2 Std (M.I.)(Galv.) 1 PIPE2 x 11 1/2 Lg(Thr'd. 2 Ends)-(Galv. Iron)
17 20158	2C158-P2 1 UNION
18	1 NIPPLE 2 x 2 3/4 Lg (Galv. Iron) 1 REDUCING BUSHING2 1/2 x 2 Std(Galv. Iron)
20	Cooler to Inlet Manifold
21 22	1 REDUCING BUSHING 2 1/2 x 2 Std(Galv. Iron)
23 2C158	1 NIPPLE 2 x 2 3/4 Lg (Galv. Iron) 2C158-P2 1 UNION
24	1 PIPE 2 x 13 Lg. (Thr'd. 2 Ends) - (Galv. Iron)
25	1 ELBOW 2 Std (M.I.)(Galv.) 1 NIPPLE 2 x 5 1/4 Lg (Galv. Iron)
27	Water Out. Man. to Ex. Man
28	1 NIPPLE 2 x 3 1/2 Lg (Galv. Iron) 1 ELBOW 2 Std (M.I.)(Galv.)
30	1 CLOSE NIPPLE 2 Std (Galv. Iron)
31 32	1 ELBOW 2 Std (M.I.) (Galv.)
32	1 PIPE2 x 129 1/4 Lg. (Thr'd. 2 Ends) (Galv. Iron) 1 CROSS 2 Std (M.I.) (Galv.)
34	1 PIPE PLUG 2 Std (C.I.)(Galv.)
35	1 NIPPLE 2 x 11 Lg (Galv. Iron) Water Inlet Man. to Air Comp. Cyl
37	1 NIPPLE 1/2 x 2 1/2 Lo (Galv. Iron)
38	l ELBOW 1/2 Std (M.I.)(Galv.) l PIPE1/2 x 29 Lg.(Thr'd. 2 Ends)(Galv. Iron)
40	Air Comp. Cyl. Head Outlet to Water Manifold
41	1 NIPPLE 1/2 x 3 1/2 Lg (Galv. Iron)
$-\frac{42}{43}$ 20158	2C158-P 1/2 1 UNION 1 PIPE1/2 x 47 Lg(Thr'd. 2 Ends)(Galv. Tron)
44 :	Water Out. Man. to Ex. Man
45 ;	203192 2 CLAMP - Pipe to Air Inlet Man. 203193 2 CLAMP - Water Pipe
`47	1 BLOCK - Clamp
48 :	2 CAPSCREW 3/8-16-NC x 2 1/4 Lg(St.) 2 NUT 3/8-16-NC-Hex (St.)
50	2 LOCKWASHER 3/8 SAE Reg (St.)
OPP.HAND SEE	NAME WATER PIPING GROUP (FOR ROSS OIL COOLER)
R OPF. ROT. SEE	FOR TOTAL REQUIREMENTS PER ENGINE MULTIPLY NO. REQ'D GIVEN ABOVE BY NO. REQ'D FOR GROUP GIVEN ON INDEX SHEET
240 REV. 5-42 IM TRAN	DADEC LICT ATLACIMPEDIAL DIESEL ENGINE CO
IM BOND	OARLAND, CALIF.

Charged, the set of the part Note Charged, the set of the part Charged Charged	To	rom 10/13/39 (No Changes)
ALWAYS GIVE PART HUMBER PART NAME - BIGNINE NAMES PART NAME	E-10-A3 A	aded Thion Fitting Part Now.
Fig. 271 NASSWARE WITHOUT PART NUMBER SAYS DESCRIPTION AND SIZE FACT NO. FORT NAME SAYS SA	Added Dr	No Added Line 42
Fig. 271 NARDWARE WITHOUT PART NUMBER CRYP DECEMBER STATUM FORTH NAME STATUM STATUM	· .	2170
Section Sect		FOR STR. HARDWARE WITHOUT BART NUMBER GIVE DESCRIPTION AND SIZE
	LINE DOWN NO	* INDICATES PART NOT SERVICED INDIVIDUALLY
REDUCING BUSHING 2 x 1 5td (Calv. Iron)	NO.	Ex Man. Inlet Line to Ex. Valve Cage
C-9049		1 REDUCING BUSHING 2 x 1 Std (Galv. Iron)
1 NIPPLE 1 x 4 1/2 Lg (Galv. Jron)	3 0040	The state of the s
1 NIPPLE 1 x 2 1/2 Lg (calv. Iron)		1 NIPPLE 1 x 4 1/2 Lg (Galv. Iron)
SC156 C-3598 MANIFOLD - Ex. Velve Cage Cooling (Inlet) C-3598 MANIFOLD - Ex. Velve Cage Cooling (Outlet) C-3591 C-3591 C-3581 C-3	6	1 ELBOW 1 Std (M.I.) (Galv.)
C - 2508	8 20159	
C-455 B CLAMP - Menifold Support		C-3392 1 MANIFOLD - Ex. Valve Cage Cooling (Inlet)
		The state of the s
## ANT 1/2-13-NC-Hex (Stá) 6 TUBE(Inlet)3/8 ODX .035 x 14	13	8 LOCKWASHER 1/2 SAE Reg (St.)
10		
		6 TUBE(Inlet) 3/8 ODx . 035 x 14 Lg (S.D. Cop)
C-9816 C-9816-P 3/8 24 NUT - Tube Fitting		6 TUBE(Outlet) 3/8 ODX .035 x 14 Lg (S.D. Cop)
20		C-9816-P 3/8 24 NUT - Tube Fitting
CLOSE NIPPLE 1 1/4 Std (Calv. Iron)	20	
23 C-9048		1 CLOSE NIPPLE 1 1/4 Std (Galv. Iron)
25		C-9048-P1 1/4 1 GLOBE VALVE
1 NIPPLE 1 1/4 x 4 1/2 Lg ((Galv. Tron)		
1 STREET ELL 1 1/4 Std (Mo. 1.) (CRIV.)	26 20100	7 MIPPIE 1 1/4 x 4 1/2 Lg - (Galv. Iron)
1 PIPE PLUG 1 Std (C.I.)(Galv.) 6 TUBE 1/2 O.D. x .049 x 14 1/2 Lg(H.D. Cop.) 5 TUBE 1/2 O.D. x .049 x 35 Lg(H.D. Cop.) 1 TUBE 1/2 O.D. x .049 x 45 Lg(H.D. Cop.) 1 TUBE 1/2 O.D. x .049 x 45 Lg(H.D. Cop.) 24 C-9817-P 1/2 12 CONNECTOR - Tube Fitting 25 C-9816		1 STREET ELL 1 1/4 Std (Male) (GREV-0)
5 TUBE 1/2 0.D. x .049 x 35 Lg(H.D. Cop.)		1 PIPE PLUG 1 Std (C.I.)(Galv.)
1 TUBE +1/2 0.D. x .049 x 43 Lg(H.D. Cop.) 32 C-9817		6 TUBE 1/2 0.D. x .049 x 14 1/2 Lg (H.D. Cop.)
33 C-9817 C-9817-F 1/2 12 CONNECTOR - Tube Fitting 34 C-9821 C-9821-F 1/2 12 ELBOW - Tube Fitting 35 C-9816 C-9816-P 1/2 24 NUT - Tube Fitting 36 C-9816 C-9816-P 1/2 24 NUT - Tube Fitting 37 C-3286 2 CLAMP - Manifold 38 2 CAPSCREW - 1/2-13-NC x 7/8 Lg (St.) 38 2 LOCKWASHER - 1/2 SAE Reg (St.) 39 C-8267 2 CAP - Support Clamp 40 4 CAPSCREW - 1/2-13-NC x 1 1/4 Lg (St.) 41 4 NUT - + 1/2-13-NC - Hex (St.) 42 1 REDUC. BUSHING(Man. End Tee)-1 x 3/8 Std(Galv III 44 St. Std. 45 Std. Std. Std. 46 Std. Std. Std. Std. 47 Std. Std. Std. Std. Std. 48 Std. Std. Std. Std. Std. Std. 49 Std. Std. Std. Std. Std. Std. Std. Std. 40 Std.		1 TUBE 1/2 0.D. x .049 x 43 Lg (H.D. Cop.)
35 C-9816 C-9816-P 1/2 24 NUT - Tube Fitting 36 C-3286 2 CLAMP - Manifold Support 37 2 CAPSCREW - 1/2-13-NC x 7/8 Lg (St.) 38 2 LOCKWASHER - 1/2 SAE Reg (St.) 39 C-8267 2 CAP - Support Clamp 40 4 CAPSCREW - 1/2-13-NC x 1 1/4 Lg (St.) 41 4 NUT - 1/2-13-NC-Hex (St.) 42 1 REDUC. BUSHING(Man. End Tee) - 1 x 3/8 Std(Galv It 43 44 45 46 47 48 49 46 47 48 49 49 47 48 49 49 49 49 40 40 40 40	83 C-9817	C-9817-P 1/2 12 CONNECTOR - Tube Fitting
36 C-3286 2 CLAMP - Manifold Support	Management Controller service and a service or a service	
2 LOCKWASHER 1/2 SAE Reg (St.) 39		G-3286 2 CLAMP - Manifold Support
39		2 CAPSCREW 1/2-13-NC x 7/8 Ls (St.)
4 NUT 1/2-13-NC-Hex (St.) 1 REDUC. BUSHING (Man. End Tee)-1 x 3/8 Std (Galv Tr 43 44 45 46 47 48 49 50 PPF-HAND SEE NAME WATER PIPING GROUP ORIGINALLY 6 CYL. 13 x 16 MARINE - R.H. ISSUED FOR 6 CYL. 13 x 16 MARINE - R.H. FOR TOTAL REQU. SEMENTS PER ENGINE MULTIPLY NO. REQ'D GIVEN ABOVE BY NO. REQ'D FOR GROUP GIVEN ON INDEX SHEET		G-8267 2 CAP - Support Clamp
1 REDUC. BUSHING (Man. End Tee)-1 x 3/8 Std (Galv It 43 44 45 46 47 48 49 50 50 ORIGINALLY 6 CYL. 13 x 16 MARINE - R.H. DEF. ROT. SEE FOR TOTAL REQU. REMENTS PER ENGINE MULTIPLY NO. REQ'D GIVEN ABOVE BY NO. REQ'D FOR GROUP GIVEN ON INDEX SHEET		
44 45 46 47 48 49 50 50 CORIGINALLY 6 CYI. 13 × 16 MARINE - R. H. SISSUED FOR TOTAL REQUIREMENTS PER ENGINE MULTIPLY NO. REQ'D GIVEN ABOVE BY NO. REQ'D FOR GROUP GIVEN ON INDEX SHEET	***************************************	1 REDUC. BUSHING (Man. End Tee) -1 x 3/8 Std (Galv Ir
45 46 47 48 49 50 DPP.HAND BEE NAME WA'LER PIPING GROUP ORIGINALLY 6 CYT. 13 x 16 MARINE - R.H. ISSUED FOR TOTAL REQUIREMENTS PER ENGINE MULTIPLY NO. REQ'D GIVEN ABOVE BY NO. REQ'D FOR GROUP GIVEN ON INDEX SHEET		
46 47 48 49 ? 50 DEPT. HAND BEE CLI344 NAME WATER PIPING GROUP ORIGINALLY 6 CYL. 13 x 16 MARINE - R. H. ISSUED FOR TOTAL REQUIREMENTS PER ENGINE MULTIPLY NO. REQ'D GIVEN ABOVE BY NO. REQ'D FOR GROUP GIVEN ON INDEX SHEET		
48 49 50 50 NAME WATER PIPING GROUP ORIGINALLY 6 CYI. 13 × 16 MARINE - R.H. ISSUED FOR TOTAL REQUIREMENTS PER ENGINE MULTIPLY NO. REQ'D GIVEN ABOVE BY NO. REQ'D FOR GROUP GIVEN ON INDEX SHEET		
49 ? 50 SPP. HAND BEE NAME WATER PIPING GROUP ORIGINALLY 6 CYT. 13 × 16 MARINE - R. H. ISSUED FOR TOTAL REQUIREMENTS PER ENGINE MULTIPLY NO. REQ'D GIVEN ABOVE BY NO. REQ'D FOR GROUP GIVEN ON INDEX SHEET		
PPF. HAND BEE NAME WATER PIPING GROUP ORIGINALLY 6 CYT. 13 X 16 MARINE - R. H. ISSUED FOR TOTAL REQU. ZEMENTS PER ENGINE MULTIPLY NO. REQ'D GIVEN ABOVE BY NO. REQ'D FOR GROUP GIVEN ON INDEX SHEET FOR TOTAL REQU. ZEMENTS PER ENGINE MULTIPLY NO. REQ'D GIVEN ABOVE BY NO. REQ'D FOR GROUP GIVEN ON INDEX SHEET		
ORIGINALLY 6 CYT. 13 X 16 MARINE - R.H. OPP. ROT. SEE FOR TOTAL REQU. ZEMENTS PER ENGINE MULTIPLY NO. REQ'D GIVEN ABOVE BY NO. REQ'D FOR GROUP GIVEN ON INDEX SHEET		WATER PIPING GROUP
FOR TOTAL REQU. REMENTS PER ENGINE MULTIPLY NO. REQ'D GIVEN ABOVE BY NO. REQ'D FOR GROUP GIVEN ON INDEX SHEET	2L1344	ORIGINALLY 6 CYL. 13 X 16 MARINE - R.H.
	OPP. ROT. SEE	FOR TOTAL REQU. SEMENTS PER ENGINE MULTIPLY NO. REQ'D GIVEN ABOVE BY NO. REQ'D FOR GROUP GIVEN ON INDEX SHEET
1240 REV. 5-42 IM TRANS IM BOND MATTOON, ILL.		MATTOON !!!

ORM 240 REV. 5-42 1M TRANS.



ALWAYS GIVE RART NUMBER—PART NAME—ENGINE NUMBER POR STD. HARDWARRE WITHOUT PART NUMBER GIVE DESCRIPTION AND SIZE PLATE NO. REC. PART NO. REC. PART NO. REC. PART NO. REC. OF PART NO. REC. REC. REC. REC. REC. REC. REC. REC	ES TO BUR DATE 1-3-49 CHKD BY DATE 1-3-49								
ALWAYS GIVE PART NUMBER—PART NAME—ENGINE NUMBER PLAYE K-1877	retyped from 4-18-40 (No changes)								
FOR STD. HARDWARE WITHOUT PART NUMBER GIVE DESCRIPTION AND SIZE No. K-1877 -									
FOR STD. HARDWARE WITHOUT PART NUMBER GIVE DESCRIPTION AND SIZE No. K-1877 -									
FOR STD. HARDWARE WITHOUT PART NUMBER GIVE DESCRIPTION AND SIZE No. K-1877 -	2 265								
Line DRWG.NO. REF. PARTINO. REC. PARTINAME DISWE. NO. F-2653									
1									
3 C-2408 53 C-2408L1 3/4 2 CAPSCREW Astern Cam to Ahead Cam 1 WIRE #16 Ga. x 10 Lg (St.) 5 S-2979 54 597-E6 1 CAM - Air Starting (Astern) 6 C-2408 55 C-2408L1 1/2 2 CAPSCREW - Air Start. Cam to Inlet Cam 7 S-2233 56 881A-E 2 WASHER - Air Start. Cam Capscrew 8									
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7 S-2233 56 881A-E 2 WASHER - Air Start. Cam Capscrew 8	70								
S									
9 2CL432 57 2Cl432L5 1/2 1 KEY - Inlet & Air Starting Cam to Camshaft 10 10 11 F-2643 58 560-P6 1 CAM - Exhaust - (Ahead). 12 S-3033 59 532A-P6 1 CAM - Exhaust - (Astern) 13 C-2408 60 C-2408L1 3/4 2 CAPSCREW - Astern Cam to Ahead Cam 14 .									
11 F-2643 58 560-P6 1 CAM - Exhaust - (Ahead). 12 S-3033 59 532A-P6 1 CAM - Exhaust - (Astern) 13 C-2408 60 C-2408L1 3/4 2 CAPSCREW - Astern Cam to Ahead Cam 14 1 WIRE - #16 Ga. x 10 Lg (St.) 15 S-2978 61 881-E 1 DISC - Fuel Cam 16 C-2408 62 C-2408L1 1/2 2 CAPSCREW - Disc to Exhaust Cam 17 S-2233 63 881A-E 2 WASHER - Fuel Cam Capscrew 18 F-1656 64 880-E 1 TOE - Fuel Cam 19 C-2406 65 C-2406L 3/4 1 CAPSCREW - Toe to Fuel Cam Disc 20 1 WIRE - #16 Ga. x 12 Lg (St.)	Ct /								
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18 F-1656 64 880-E 1 TOE - Fuel Cam 19 C-2406 65 C-2406L 3/4 1 CAPSCREW - Toe to Fuel Cam Disc 20 1 WIRE #16 Ga. x 12 Lg (St.)									
1 WIRE #16 Ga. x 12 Lg. +- (St.)	سوس								
21 2C1432 66 2C143214 1/2 1 KEY - Exhaust & Fuel Cam to Camshaft	· +4								
$-\frac{22}{2}$									
	4.								
25	ત્રો								
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29 30 4									
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34 35 35	To the same								
36	124								
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40 Left Hand 10 x 13 & 11 1/2 x 15 Engines Inlet	The same of the sa								
Cams Listed above are used as Exhaust Cams Exhaust Cams 42 are used for Inlet Cams.	Cams								
42 are used for Inlet Cams. Left Hand 13 x 16 Engines Cams same as									
14 listed above									
45 46									
47									
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49 7									
AOPP. HAND THE CAM GROUP (INBOARD HOTAPION)									
ORIGINALLY 6 CYL HAR 10x13 to 13x16 1 6	3 15								
AD REV. 1/46 2M TRANS. PARTS LIST ATLAS IMPERIAL DIESEL ENGINE CO. AND REV. 1/46 2M TRANS. PARTS LIST ATLAS IMPERIAL DIESEL ENGINE CO. MATTOON, ILL.	5.///J								
INTESTINUES, A. MATTOON, ILL.	1. 1 364								

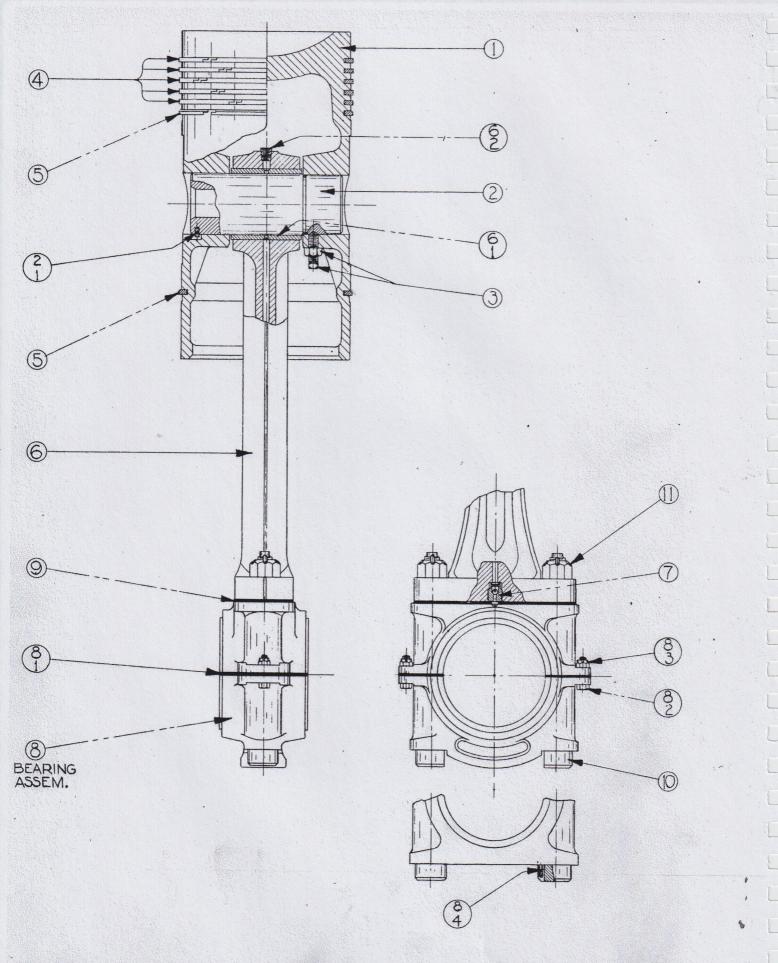


PLATE No. W-1751

DO NOT ORDER PARTS BY REF. NUMBERS

TYPEDABC DATE 7-23-46 typed from 11-24-44 (no changes) ALWAYS GIVE PART NUMBER-PART NAME-ENGINE NUMBER PLATE W-1751 FOR STD. HARDWARE WITHOUT PART NUMBER GIVE DESCRIPTION AND SIZE ASSEM. NO. PART NAME LINE DRWG. NO. PART NO. REQD NO. PISTON K-1297 1 PIN ASSEM. Piston 1 2 X1289 2 SETSCREW--3/4-10-NC x 2 1/4 Lg. - Sq. Hd. Cup 3 3 4 NUT -- 3/4-10-NC-Hex. -5 6 RING - Piston (Compression) 5 C-2155L13 7 4 C - 2155RING - Piston (Oil Control) 2 C-2355L13 8 C-2355 5 9 ROD ASSEM. - Connecting X3105 F-6221 10 VALVE ASSEM. - Ball Check X3106 11 2C1515 BEARING ASSEM. - Connecting Rod 1 X3107 12 W-1552 8 SHIM - Bearing to Rod - (1/16) 2C1487-A 201487 9 1.3 SHIM - Bearing to Rod -1 201487-B 14 2C1487 9 SHIM - Bearing to Rod - (1/64)
BOLT - Connecting Rod to Bearing 2 2C1487-C 9 15 2C1487 2 201463 10 16 NUT - Connect. Rod Bolt 2 S-2716 11 17 COTTER PIN -- 1/4 x 2 3/4 Lg. - -18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 38 39 40 41 4.2 43 44 45 46 CONNECTING ROD GROUP OPP. HAND SEE ORIGINALLY 13 X 16 MAR. & ENGINE MULTIPLY NO. REQ'D GIVEN ABOVE BY NO. REQ'D FOR GROUP GIVEN ON INDEX SHEET R OPP. ROF, SEE OR TOTAL REQUIREMENTS PER ATLAS IMPERIAL DIESEL ENGINE CO. 247 REV. 1/46 2M TRANS. ED IN U.B.A.

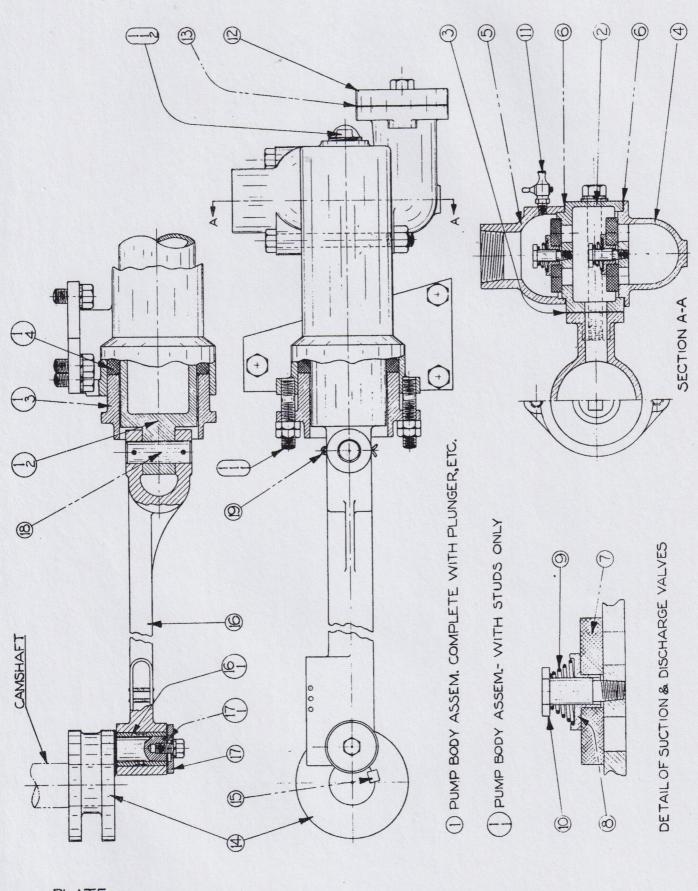
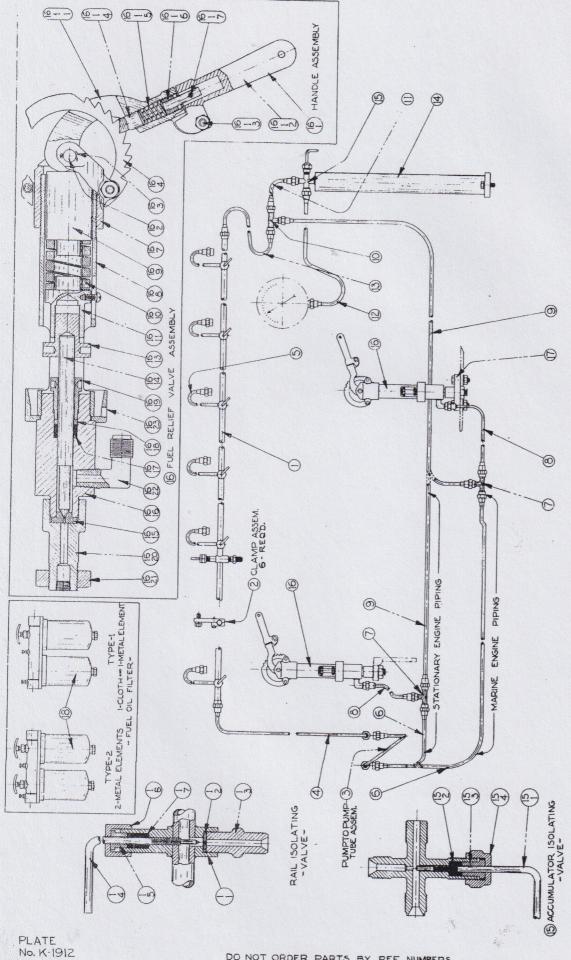


PLATE No.W-1731

DO NOT ORDER PARTS BY REF. NUMBERS

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4		X**			1
	,4°1	ALWA	VS CIVE PART NU	MBER	PART NAME—ENGINE NUMBER PLATE W. 1777
	1 /	FOR S	TD. HARDWARE W	ТНОФТ	PART NUMBER GIVE DESCRIPTION AND SIZE No. W-1751
NE .	DRWG.NO.	REF.	PART NO	NO.	PART NAME DRWG. NO.
1		1	X1123		PUMP ASSEM Bilge
2		/		3	CAPSCREW 5/8-11-NC x 1 1/4 Lg (St.) LOCKWASHER 5/8 SAE Reg (St.)
4 1	er 077	2	214-E	7	GRID - Bilge Pump Discharge Valve
5	W-83	3	C-1217	9	GASKET - Grid to Pump Body
6		5.0	St. St. St. du 1	2	CAPSCREW 5/8-11-NC x 6 Lg (St.)
7		777		2	LOCKWASHER 5/8 SAE Reg (St.)
8		4	W-1690	1	BONNET - Suction Valve
	C-242	5	216-E	1	BONNET - Discharge Valve
200	S-2050	6	215A-E	2	GASKET - Bonnets to Grid CAPSCREW 5/8-11-NC x 6 Lg (St.)
11 12	· ·	1		2	NUT 5/8-11-NC-Hex (St.)
manual.	s-1788	7	219-E1	2	VALVE - Bilge Pump Suction & Discharge
	S-2289	8	219A-6	2	BUSHING - Bilge Pump Valve
	C-461	9	218-E	2	SPRING - Bilge Pump Valve
	3-2046	10	217-7	2	STUD - Bilge Pump Valve
17	0-9045	11	C-9045-P 1/	4 1	COCK - Air (Discharge Bonnet)
18		1		11	PIPE PLUG 1/4 Std (Brass)
	C-5356	12	788-B	1	FLANGE - Bilge Pump Suction Pipe GASKET - Flange to Pump Bonnet
$\frac{20}{21}$	- X	13	S-924	2	CAPSCREW 5/8-11-NC x 1 1/2 Lg (St.)
22					Orac Domina
-	0-1123	14	266-CX	1	CRANK - Bilge Pump Drive
24	S-3234	15	5354	1	KEY - Crank to Camshaft
	F-3271	16	G264-03	1	ROD ASSEM Bilge Pump Connecting
	C-8880	17	X2362	1	WASHER ASSEM Connect. Rod Retainer CAPSCREW 1/2-13-NC x 3/4 Lg (St.)
27		1		17	LOCKWASHER 1/2 SAE Reg (St.)
29	S-2002	18	264B-E	1	PTN - Conn. Rod to Pump Plunger
30	0-2002	1		2	COTTER PIN 3/16 x 2 1/2 Lg. (St.) 5
31					
32					
33					
34					
36					
37	1				
38					
39		-			
40					
41					
43	1				
44					
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46		1			
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48	 	-		-	
50					
-	AND SEE	NA	ME BILGE P	UMP /	GROUP
	357	11 11	and the second s	13,5	ORIGINALLY C CVT. 13 x 16 MARINE - R.H.



DO NOT ORDER PARTS BY REF. NUMBERS

/ES	12	2-30-40	Line .	17 Part No. of Capscrew	Was	X210 BY DATE // -// CHKD. APRVD.
	. Li	ne 18 L	ength	of Capscrew	Wa	s light of the second of the s
		N				AND
			H	The second secon	12072467	
(Fr			ALWAY	S GIVE PART NUMBER	R-PA	RT NAME FINGING NUMBER 2 L 380
L						ART NUMBER GIVE DESCRIPTION AND SIZE PLATE K-1012
1	NO.	DRWG. NO.	REF.	FART NO.	NO.	T ASSEM.
	1	K-613	190	Х8	1	RAIL ASSEM Fuel
1	7/2	S-2238	2	G1203-AX3		CLAMP ASSEW Fuel Rail
	3		Carrier School Consumption		6	CAPSCREW 1/2-13-NC x 1 1/4 Lg (St.)
	+	0 7740	2	vene	6	LOCKWASHER 1/2 SAE Reg (St.)
		C-3348 C-3348	3	X575 X3055	7	TUBE ASSEM Pump to Pump (13") TUBE ASSEM Pump to Rail (38")
Ļ	100000000000000000000000000000000000000		5	X5011	6	TUBE ASSEM Rail to Spray Valve (27")
			6	X1007		TUBE ASSEM Pump to Tee (Opp. Reg. Valve) - (108")
_	. 8		7	F-707		TEE - Fuel Tube
		C-3348	18	X688	1	TUBE ASSEM Tee to Regulat. Valve (16")
		C-3348	9	X895		TUBE ASSEMTee to Tee(Opp. Accumulator)-(78")
L	12	C-3348	10	F-707 X575	1	TEE - Fuel Tube TUBE ASSEM Tee to Accumulator (13")
1		S-3178	122	X4	7	TUBE ASSEM Tee to Accumulator (15") TUBE ASSEMAccumulator to Press. Cage (84")
_		C-3348	13	X3054	1	TUBE ASSEM Tee to Rail (20")
{	16					
		F-6457_	14	X3234		ACCUMULATOR ASSEM Fuel
	18	NEW TOTAL CONTROL OF THE PROPERTY OF THE PROPE	1			CAPSCREW 1/2-13-NC x 1 1/4 Lg (St.)
	20			G1215-E	7	LOCKWASHER 1/2 SAF Reg (St.)
L	21		15	GLOLOSI	٠	VALVE ASSEM Accumulator Isolating
1	22	W-28	16	G1230-E1	1	VALVE ASSEM Fuel Pressure Regulating
7	23		17	S-2132		BRACKET - Fuel Press. Regulating Valve
	24			L		CAPSCREW 5/8-11-NC x 2 Lg (St.)
	25		ļ		2	· · · · · · · · · · · · · · · · · · ·
	26		1		2	LOCKWASHER 5/8 SAE Reg (St.)
	28	gyllystalaster for the subject of the same way of the	-			
	29	reflect ABO decide a chiefe of the chiefe file which can a second file of the chiefe o				L.P. Fuel Piping - Filter to H.P. Pump
1		F-6418	18	F-6418-P	1	FILTER - Fuel
_	31				2	REDUCING BUSHING 1/2 x 3/8 Std (C.I.)
	32	NO. O PROGRAMMENT OF THE PROGRAM OF	-		2	CAPSCREW 1/2-13-NC x 1 1/4 Lg (St.)
	33	C-9804	1 . /	0-9804-P 1/2	2	LOCKWASHER 1/2 SAE Reg (St.) ELBOW - Tube Fitting
L	35	V VUUT		2 000x-1 1/6	1	TUBE 1/2 0.D. x .049 x 9 Lg(H.D. Cop.)
	36	C-9804		C-9804-P 1/2	1	ELBOW - Tube Fitting
	37	had a rich or hand a common of a fire a rich and a character common and an			1	REDUCING BUSHING 1/2 x 3/8 Std (C.I.)
1	38			The second section of the second seco		
	39 40			the manufacture and the contract of the contra		Decay Davidah Vala to Marin D
L	41	C-9801	1	C-9801-P 3/8		-Press. Regulat. Valve to Trans. Pump(By-pass Line). CONNECTOR - Tube Fitting
(42	0-0001	1	J-JOOL-F O/O	1	TUBE 3/8 0.D. x .035 x 118 Lg(S.D. Cop.)
L	43	C-9801	1 (0-9801-P 3/8	1	CONNECTOR - Tube Fitting
1	44				1	TEE 1/2 x 1/2 x 1/4 Std. Reducing(Brass)
	45	Max. And Williams W. Captile Sect Cappain. Capti	ļ		1	CLOSE NIPPLE 1/2 Std (Brass)
1	46	or man contra di anno e sono di con contra con di anno di contra con di contra con di contra con di contra con	+		3	VHAIR TUVV
	48			paramental and an extra parame	3	MACHINE SCREW-/4-20 x 3/8 Lg-Rnd.Hd(St.)
L	19				· · · · ·	LOCKWASHER 1/4 SAE Reg (St.)
(50;				******	
L.,		OT ZCT	NAME_	FUEL SYSTEM	d GI	
1	P. ROT	21381 _	ii	TAL BEOLUPELS ASS	N.F	originally 6 CYL. 13 x 16 MARTNE - R.H.
-	1.1	••••	FOR I	ITAL REQUIREMENTS PER ENGI	ME MALL	ATTIAC INADECTIAL DIECE ENCLASE
L	.o. 2.	2 15 55	i in a	"AIT I D	Annusani	ST ATLAS IMPERIAL DIESEL ENGINE CO.
			Harris Sales			1

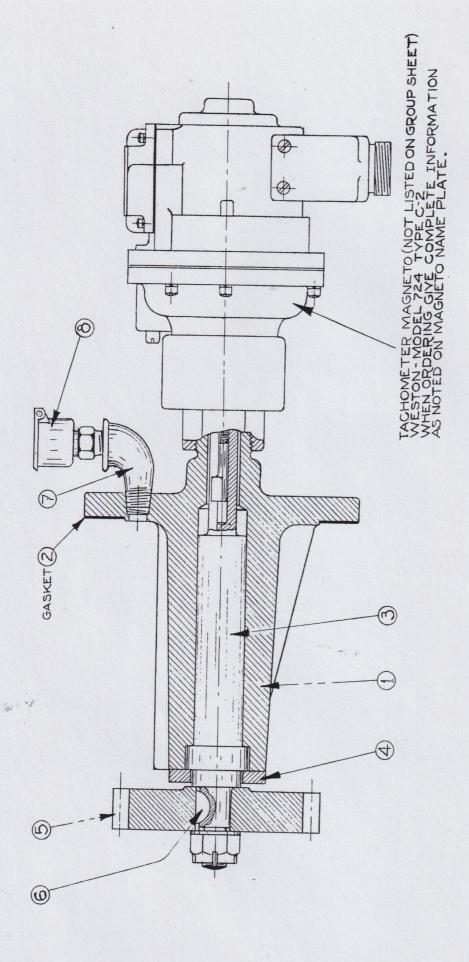


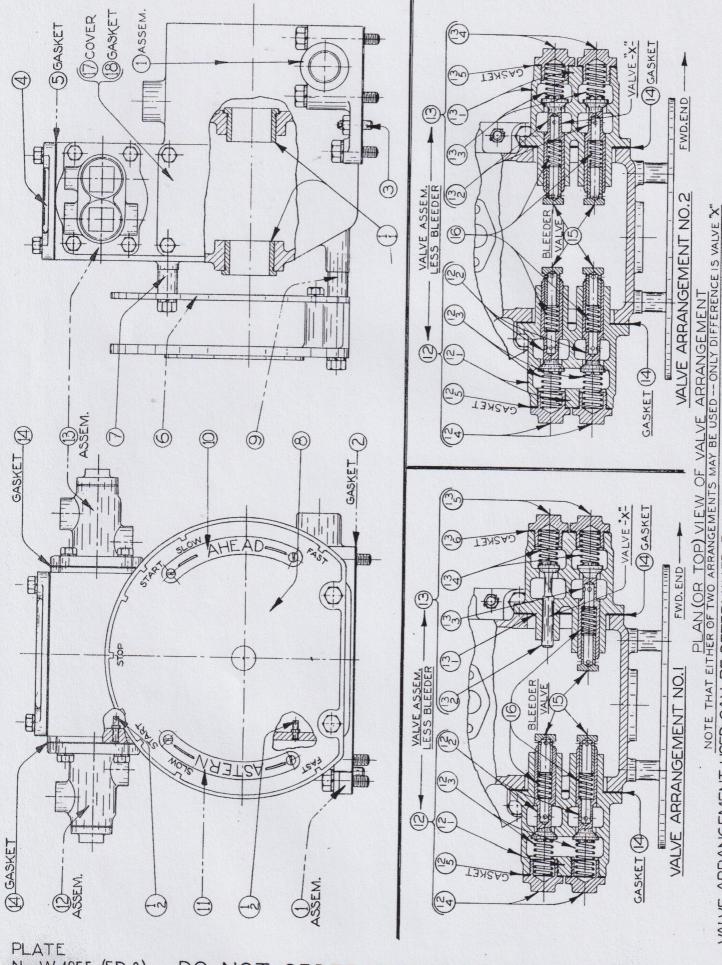
PLATE No. W:1784 ED-2

DO NOT ORDER PARTS BY REF. No.

Retyped from sheet dated 1-21-49. 2L 457 ALWAYS GIVE PART NUMBER - PART NAME - ENGINE NUMBER FOR STD. HARDWARE WITHOUT PART NUMBER GIVE DESCRIPTION AND SIZE PLATE NO. W-1784 DRWG NO PART NAME BEARING-Tachometer Drive Shaft W-16822 C-7527 GASKET-Bearing to Centerframe CAPSCREW-3/8-16-NC x 7/8 Lg.- (St.) LOCKWASHER-3/8 SAE Reg. - (St.) 3 201881 SHAFT - Tachometer Drive WASHER- Tach. Drive Shaft Thrust 201880 MACHINE SCREW-1/4-20-NC x 1/2 Lg.Flat Hd(St 5 2C1882 GEAR - Tachometer Drive 6 WOODRUFF KEY-1/8 x 1/2 Std.- (St.) PLAIN WASHER - 3/8 SAE Std. - (St.) CASTLE NUT-3/8-24-NF-Hex/--(St.) 1 COTTER PIN-3/32 x 3/4 Lg. - (St.) 1 7 STREET ELL- 1/8 Std. -- (M.I) 8 OIL CUP -1/8 Hinged Lid-Gits #802 or Eq. (St. S TACHOMETER DRIVE GROUP 6/c 13 x 16 MARINE FOR TOTAL REQUIREMENTS PER ENGINE MULTIPLY NO. REQ'D GIVEN ABOVE BY NO. REQ'D FOR GROUP GIVEN ON INDEX SHEET PARTS LIST THE NATIONAL SUPPLY CO. ENGINE DIVISION SPRINGFIELD ONIO

Removed Tv	$\frac{8}{15} = \frac{1}{2}$	Part No. Was B-11 Half Nut Added Four Of	2C1 ts &	1 5/32 iii lups 9
4-7-44 Rem	oved	Part No. 202 No. Req. wa	149	·r.ine
An Tank III	ALWAY	S GIVE PART NUMBER	-PAR	T NAME - ENGINE NUMBER RT NUMBER GIVE DESCRIPTION AND SIZE PLATE V-1000 (FW 0)
	REF.	INDICATES PART NOT	NO.	T ASSEM.
NO. DRWG. NO.	NO. *	PART NO.	REQD.	The state of the s
1 W-1787	1	X3262 F-6473	1	HOUSING ASSEM Reversing Rack GASKET - Housing to Latch Box
2 .	2	L =04:10	12	CAPSCREW 1/2-13-NC x 1-1/4 Lg (St.)
3			12	LOCKWASHER 1/2 SAE Reg (St.)
5 202394	3	202394L1 1/4	2 4	PIN - Housing to Latch Box Dowel OIL CUP Lunkenheimer #540 Size 0 - 1/8 Pipe Thread - (St.)
7	A	F=6472	1	COVER - Rack Housing Top
8	5	202151	1	GASKET - Cover to Housing
10			4	CAPSCREW 3/8-16-NC x 7/8 Lg (St.)
11			4	LOCKWASHER 3/8 SAE Reg (St.)
12	6	C-9731	1	COVER - Rack Housing End .
13	7	0-9735	1	GASKET - Cover to Housing CAPSCREW 3/8-16-NC x 1-1/4 Lg (St.)
14			4	LOCKWASHER - 3/8 SAE Reg (St.)
15	11	J	1 4	DOUGHADITETT OF DATE HOLE
17				
18	1			
19				
20	10	202132	1.1.	COVER - Rack Housing Side - (Gear Cover)
21	1.1	202159		GASKET - Cover to Housing CAPSCREW 3/8-16-NC x 1 Lg (St.)
22	-	4 -	+ 7	LOCKWASHER 3/8 SAE Reg (St.)
23	12	C-9745	1	PLATE - Rack Indicator
25	13	202167	3	SPACER - Plate to Housing
26	-		3	MACHINE SCREW 1/4-20 x 1-1/8 LgFlat Hd.(St
27	1.4	X3265	1	COVER ASSEM Cylinder & Rack Housing End
28	15		5	PACKING RING - Garlock #235 2-3/4 0.D. x 2 I.D. x 3/8 wide #
29		003505	1	GLAND - Packing
30 31	16	201505	2	NUT 5/8-11-NC Hex (St.)
$\frac{31}{32}$			2	HALF NUT == 5/8=11=NC=Hex. == (St.)
33 202147	17	X3264	1	CYLINDER ASSEM Reversing
34	18	202162	2	GASKET - End Cover to Cylinder & Housing
35		The spiritual property of the second	4	NUT - 3/4-10-NC-Hex (St.)
36		11 7 C 17 (1)	4	LOCKWASHER 3/4 SAE Reg (St.) COVER - Rev. Cylinder End
37	20	W-1572 2C1506	4	GASKET - Cover to Cylinder
38	120	802000	6	NUT == 5/8=11=NC=Hex. == (St.)
40			6	LCKWASHER 5/8 SAE Reg (St.)
41 201497	21	X3060	2	VALVE ASSEM Air Cyl. Check
42	22	201504	18	VALVE - Air Cyl. Bleeder
43			2	PIPE PLUG == 3/8 Std. C't's'k. Hd. = (C.I.)
44	mma	204017	12	SHIM - Rev. Cyl. End Cover
4.5	POA	SU#U&/	ins	N N
47		f .	-	1
48				
49				CONTINUED ON SHELT NO. 2 COMOGO
50			CITT	TAYLOTTO P. TAKER ADOND
21.1244	- NAM	E REVERSING	CYL	INDER & RACK GROUP ORIGINALLY FOR 6-CYL. 13 x 16 MARINE - R.H.
JR OPP. ROT. SEE	FOR	TOTAL REQUIREMENTS PER E	NGINE N	AULTIPLY NO. REQ'D GIVEN ABOVE BY NO. REQ'D FOR THIS GROUP GIVEN ON INDEX SHEET
		PARTS		The state of the s
06-30 NO. 240 NRC		IMILIO	Posts	dakland, calif. MATTOON, ILL.
1 3 3 6 5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6				

INE /	FOR STD.	HARDWARE WITHO	UTP	RT NAME-ENGINE NUMBER ART NUMBER GIVE DESCRIPTION AND SIZE PLATE K-1989 (Ed 2) T ASSEM.
DRWG. NO.	NO. *	PART NO.	REQU	PART NAME ORWG.NO. CONTINUED FROM SHEET NO. 1
3 F=6475 4	28	X3263 202137	1 2	RACK ASSEM Reversing - (& Piston Rod) KEY - Reversing Rack Guide CAPSCREW 3/8-16-NC x 7/8 Lg (St.)
6 7 8 9 10 11 12	30 31 32 33 34	201500 2071-P6 F-6944 F-6943 202157	2 2 2 2 2	LOCKWASHER 3/8 SAE Reg (St.) PISTON - Air Cylinder RING - Piston CUP-SEAL - Air Cyl. Piston SEE SERVICE NOT FOLLOWER - Cup-Seal COLLAR - Air Cyl. Piston
12 , 13 14	35		1	CASTLE NUT 1-1/4-12-NF. Hex (St.) COTTER PIN 3/16 x 2 Lg (St.)
15 16 17 18 19 203880	37 38 C- 39 40	F-6463 202130 -6908L1-5/8 202152 X3756 -6808L2-1/4	1	SHAFT - Reversing Rack Pinion PINION - Reversing Rack KEY - Pinion to Shaft SLEEVE - Rev. Rack Pinion Shaft COLLAR ASSEM Latch Position Indicator KEY - Collar to Shaft
22 S • 912 23 24 25 26 27	42 43 44	727A-FXC4 202339 202131 -2510L1-1/4	1 1 1 4	WASHER - Collar Retainer NUT - Indicator Collar Retainer LOCKWASHER Shakeproof Type-12 - 1 1/8 - (SGEAR - Latch Shaft Control CAPSCREW - Gear to Shaft
		C1438L 1/2	5	WASHER - Gear to Shaft Capscrew WIRE #16 Ga. x 16 Lg (St.) PIN - Cear Retainer Capscrew Spacer
31 32 33 34				
35 36 37				
38 39 40 41				
42 · · · · · · · · · · · · · · · · · · ·				
46 47 48	- SERV	ICE NOTE When Suppl	The second second	g new Piston Cup-seal F-6944 to replace
50		Leather F-6	232	on Engines below #12076 always include Ring with each Cup-seal.



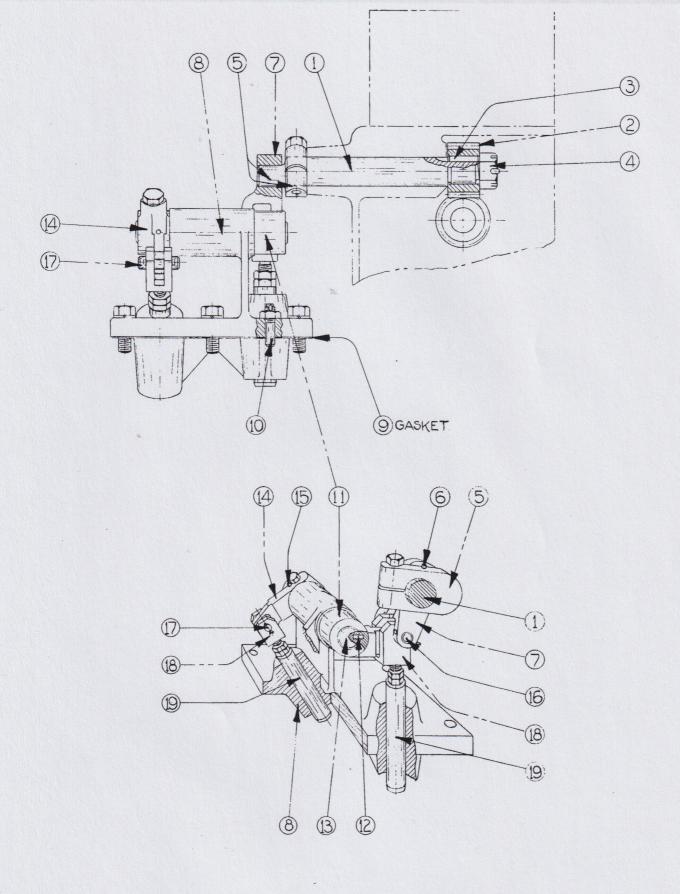
VALVE ARRANGEMENT USED CAN BE DETERMINED BY NOTING THE NUMBER OF BLEEDER VALVES (REF. 15) SPECIFIED ON GROUP LIST SHEET. IF 3 ARE SPECIFIED-ARRANGEMENT NO.2 IS USED.

No. W-1855 (ED-3) DO NOT ORDER PARTS BY REF NUMBERS

3-31-41 Added Part Nos. 202332 & 202337 Also Eight 3/8 Capserew & Lockweshers 72-10-44 Removed Line 2 12-27-51 Line 27 was C-7446 ALWAYS GIVE PART NUMBI: {-PART NAME-ENGINE NUMBER FOR STD. HARDWARE WIT! OUT PART NUMBER GIVE DESCRIPTION AND SIZE * INDICATES PART NOT SERVICED INDIVIDUALLY W-1855 ASSEM. DRWG. NO. INE PART NO. PART NAME DRWG. NO NO X3267 HOUSING ASSEM. - Engine Control 202262 GASKET - Housing to Latch Box 202272 2 CAPSCREW -- 1/2-13-NC x 1 1/2 Lg. - (St.) CAPSCREW -- 1/2-13-NC x 3 Lg. - (St.) 3 5 LOCKWASHER -- 1/2 SAE Reg. - - (St.) 6 6 PIN - Housing to Latch Box Dowel C-7950Ll 1/2 2 C-7950 HALF NUT -- 3/8-24-NF-Hex. -- (St.) COTTER PIN -- 3/32 x 3/4 Lg. - (St.) 9 COVER - Control Housing Top 202232 10 5 GASKET - Cover to Housing 11 202233 CAPSCREW -- 3/8-16-NC x 1 Lg. - (St.) 12 LOCKWASHER -- 3/8 SAE Reg. -- (St.) 13 4 PLATE - Control Handle Latch W-1811 14 C-8477L1 1/16 SPACER - Plate to Housing 15 C-8477 CAPSCREW -- 1/2-13-NC x 2 Lg. - (St.) 2 16 LOCKWASHER -- 1/2 SAE Reg. -- (St.) 17 2 PLATE - Engine Control Indicator 18 W-1810 CAPSCREW(Ind. Plate to Latch Plate) -- 3/8-16-NC 19 x 3/4 Lg. - (St. 20 SPACER - Latch Plate to Housing C-8477L1 //6 21 C-8477 2 CAPSCREW (Ind. & Latch Plate to Hous.) -22 1/2-13-NC x 4 1/4 Lg.-(St. 23 PLATE - Direction (Ahead) 24 10 202220 PLATE - Direction (Astern) 25 11 202221 MACHINE SCREW--10-24 x 1/2 Lg.-Flat Hd.-(Brass) 26 T-1247-E PLATE - Name 1 DRIVE SCREW -- Parker-Kalon #6 x 3/8 Lg. -Hardened - - (St.) VALVE ASSEM. - Air Cyl. & Brake Control X3274 13 VALVE ASSEM. -Air Start. & Cylinder Control X3275 1 GASKET - Valve to Control Housing 14 202273 CAPSCREW -- 3/8-16-NC x 1 Lg. - (St.) VALVE - Air Valve Bleeder 15 202198 3 36 16 202225 SPRING - Bleeder Valve 39 COVER - Eng. Control Housing Side 202332 40 GASKET - Cover to Housing 41 18 202337 CAPSCREW -- 3/8-16-NC x 3/4 Lg. - (St.) 42 LOCKWASHER -- 3/8 SAE Reg. - - (St.) 76 17 48 49 30 OPP. HAND SEE NAME ENGINE CONTROL HOUSING COVERS & AIR VALVE GROUP 2L1245 ORIGINALLY 6 CYL. 13x16 MAKINE - R.H. COPP. NOT. SEE FOR TOTAL REQUIREMENTS PER ENGINE MULTIFLY NO. REQ'D GIVEN ABOVE BY NO. REQ'D FOR THIS GROUP GIVEN ON INDEX SHEET ATLAS IMPERIAL DIESEL ENGINE CO. OAKLAND, CALIF MATTOC

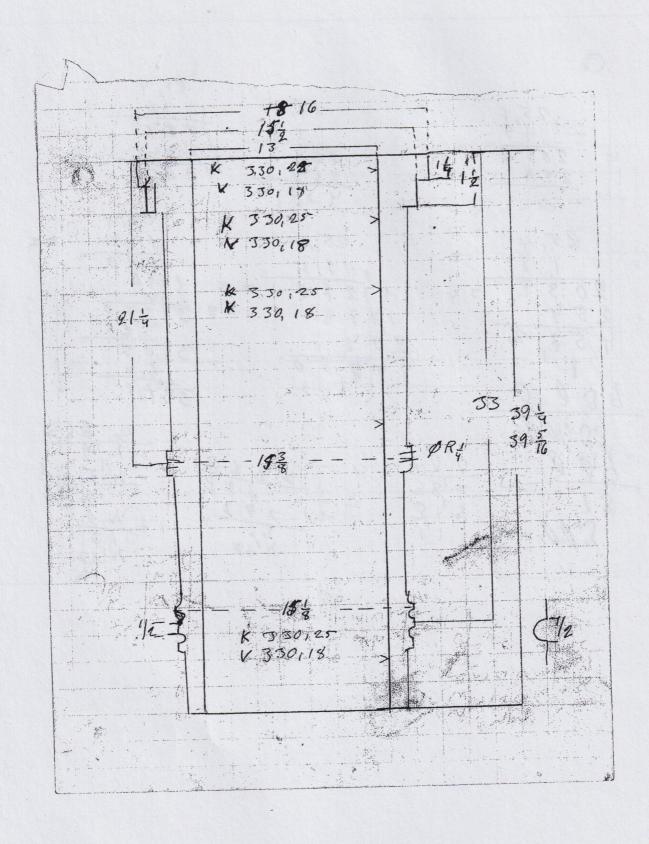
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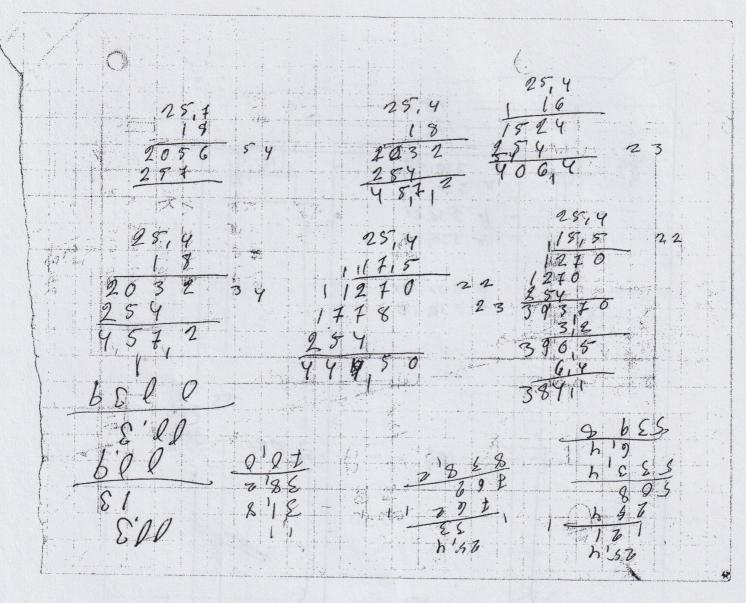




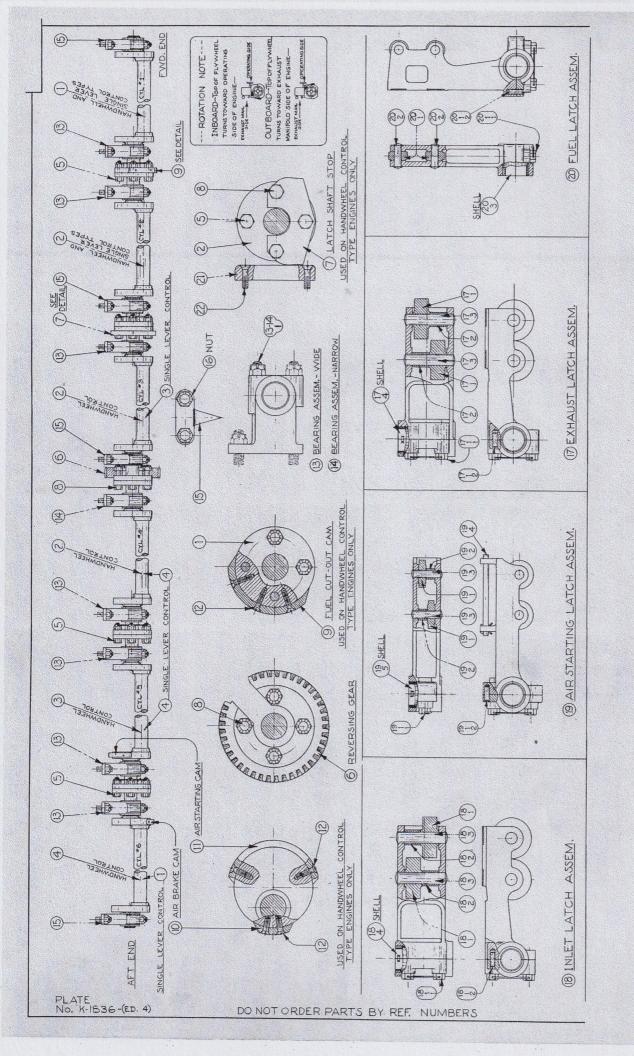
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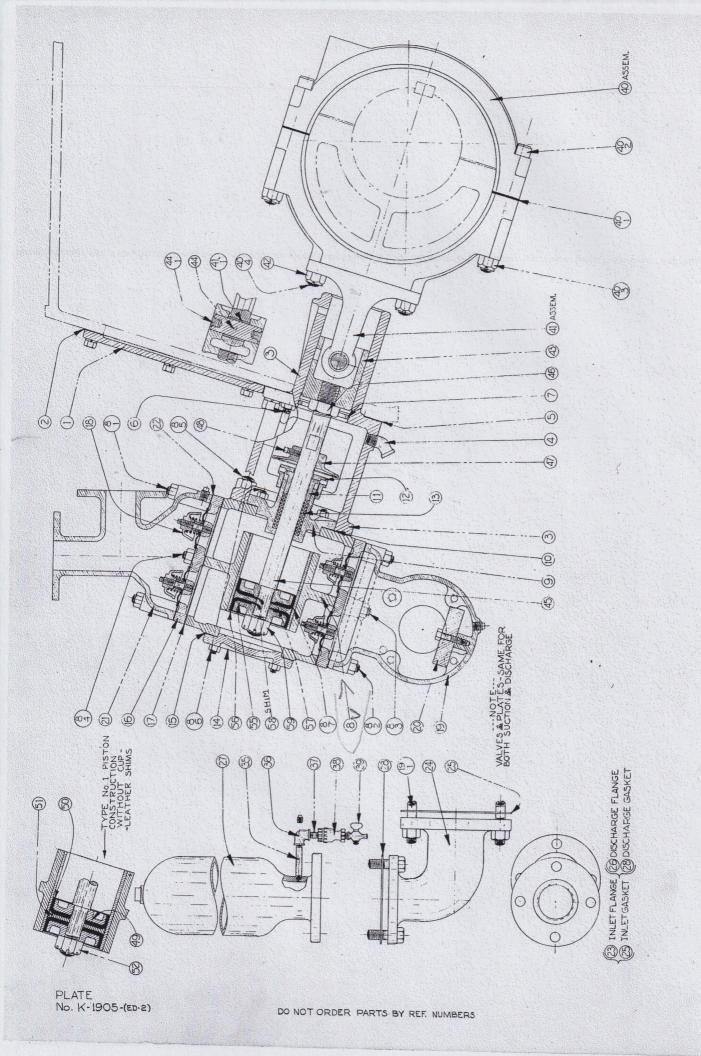




BY MED DATE 3-31-41 ISSUED BY Revised & Retyped From Sheet Dated 3-4-41 8-31-43 Line 23 Fart No. was C-9453 ALWAYS GIVE PART NUMBER-PART NAME-ENGINE NUMBER FOR STD. HARDWARE WITHOUT PART NUMBER GIVE DESCRIPTION AND SIZE * INDICATES PART NOT SERVICED INDIVIDUALLY LINE DRWG. NO. PART NO. DRWG. NO PART NAME REQU NO. SHAFT - Latch Shaft Interlock Control 202254 2 GEAR - Latch Shaft Interlock Drive 202231 KEY - Gear to Shaft C=7104 C-7104L1 1/4 SLOTTED NUT -- S/4-10-NC-Tex. -- (St.) 5 COTTER PIN -- 1/8 x 1 1/2 Lg. - (St.) CRANK - Latch Shaft Interlock Drive 6 202253 CAPSCREW -- 1/2-13-NC x 1 1/2 Lg. - (St.) TAPLE PIN -- No. 4 x 2 Lg. - (St.) 16 9 202192 LINK - Interlock Control 10 18 K-1974 BRACKET - Latch Shaft Interlock 11 9 GASKET - Bracket to Latch Box 202338 12 CAPSCREW -- 1/2-13-NC x 1 1/2 Lg. - (St.) 6 13 6 LOCKWASHER -- 1/2 SAE Rec. - - (St.) 14 0 - 7950C-7950Ll 3/4 2 PIN - Bracket to Latch Box Dowel 15 HALF NUT as as 3/8 as 24 as NF as Hex. as as (St. 2 16 COTTER PIN -- 3/32 x 3/4 Lg. - (St.) 11 17 202334 ROCKER - Interlock Plunger 18 12 WOODRUFF KEY -- 1/4 x 1 Std. - (St.) SHAFT - Interlock Plunger Rocker 202335 19 13 ROCKER - Interlock Plunger (Clamped) 20 14 202333 1 21 CAPSCREW -- 1/2-13-NC x 1 1/2 Lg. - (St.) 22 TAPER PIN -- #4 x 2 Lg. - - (St.) 2C3712L1 3/4 203712 23 16: PIN - Link to Plunger & Rocker 24 COTTER PIN -- 1/8 x 1 1/2 Lg. - (St.) 202257 202257Ll 5/8; 25 PIN - Rocker to Plunger 26 COTTER PIN -- 1/8 x 1 Lg. - - (St.) 27 18 202194 FORK - Letch Interlock Plunger 28 HALF NUT - 1/2-20-NF-Hex. - - (St.) 29 19 202193 PLUNGER - Latch Interlock 30 31 32 33 34 35 36 37 38 39 40 41 42 43 21516 45 46 47 48 49 50 OPP. HAND SEE NAME LATCH SHAFT INTERLOCK GROUP 211247 ORIGINALLY 6 CYL. 13 x 16 MARINE - R.H. PP. ROT. SEE FOR TOTAL REQUIREMENTS PER ENGINE MULTIPLY NO. REQ'D GIVEN ABOVE BY NO. REQ'D FOR THIS GROUP GIVEN ON INDEX SHEET ATLAS IMPERIAL DIESEL ENGINE CO. OAKLAND, CALLE. MATTOON, ILL. M NO. 240



	Re	etyped Fr	om 3	17FED 87 -5-41 - Crank	MEI	Op Gul	o
	1	& 6 Cons	solid	-5-41 - Crank ated into one	It	em ,	
_						Z	
L			H		``		Section of the sectio
			ALWA	YS GIVE PART NUMBER	R-PAI	RT NAME-ENGINE NUMBER 2L517	
	LINE	3	FOR S	INDICATES PART NO	NO.	The state of the s	PERSONAL PROPERTY OF THE PROPE
	NO.	DRWG. NO.	NO. *	F-2342	REQU	CRANK - Latch Shaft (Cyl. #1 Fwd #6 Aft)	
		1	2	F-6508	1	CRANK - Latch Shaft (Cyl. #2)	MANUAL CO. STATE OF THE PART OF T
	3	F-2344	3	F-6535		CRANK - Latch Shaft (Cyl. #3)	AND A MARK AND A SAME
	5		5	1692-062 C-3045		CRANK - Latch Shaft (Cyl. #4-5) CAPSCREW - Latch Crank	entrante en referent entrante
	6					CASTLE NUT 5/8-18-NF-Hex (St.)	
	8		6	C-9724	4	WIRE #16 Ga. x 16 Lg (St.) GEAR - Latch Shaft	
		C-2610			4	BOLT - Gear & Latch Cranks	Mark Market Special
	10				4.	CASTLE NUT 5/8-18-NF-Hex (St.) WIRE #16 Ga. x 16 Lg (St.)	a supreme to a supreme
	12				ah .	WIRE #10 Ga. X 10 Lg (St.)	
1		F-3698 F-3699	13	X376		BEARING ASSEM Latch Shaft (Wide)	
	15		14	х377	4 12	BEARING ASSEM Latch Shaft (Narrow) CASTLE NUT 5/8-18-NF-Hex (St.)	erent growing the Sageria
	16				24	COTTER PIN 1/8 x 1 1/4 Lg (St.)	
1	17		15	201891 0-9321		POINTER - Latch Shaft NUT - Latch Shaft Brg. Cap (& Pointer)	-
	19	ļ	-Ja ()	V	. 60	not - Lacen Share Drg. Cap (& Fornter)	
L	20	F-3671	17	X345	G	TARROLL ACCION TO-L-	
		F-3672	18:	X347	6	LATCH ASSEM Exhaust LATCH ASSEM Inlet	•
1		F-3673	19	X349		LATCH ASSEM Air Starting	
	25	F-3677	20	X357		LATCH ASSEM Fuel Spray Valve WIRE #16 Ga. x 8 Lg (St.)	
	26					H 20 300 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	
1	27		1				
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F	SI,	1243	NAME_	LATCH SHAFT O	HOU	JP (INBOARD ROTATION) GRIGINALLY 6 CYT., 13 x 16 MARINE - RaHa	
(حب	. RO	T. SEE	FOR TO	OTAL REQUIREMENTS PER ENGIN	IE MUL	130CO TOP TOP TO THE PARTY OF T	
N P	0. 2	10.19	F	PARTS	Description of the last of the	ST ATLAS IMPERIAL DIESEL ENGINE CO. OAKLAND. CALIF. MATTOON, ILL.	
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A		TYPED	MED	DATE 3 6 41 BY DATE - CHKD. APRVD. 7	_
L 10-20-41	Line 2	8 Part No. W	las F	DATE 3-6-41 PATE - CHED. 7. OF 28 #4 12-18-45 Line 3 & 4 was 1/2	
) 1 (co) , with 2 1	LINE O	Length of Ca	paor	ews b	
Was 1 1/	ine 36	Part No. wa	s C-	9391-14	
line 40 -	Part 1	Vo. was 2050	m P	Ö	
				21525 SHEET I	
	ALWAYS	S GIVE PART NUMBER	R-PART	NAME-ENGINE NUMBER NAME-ENGINE NUMBER REPORTED TO THE PLATE OF THE PLA	
		D. HARDWARE WITHO		CED INDIVIDUALLY	
NO. DRWG. NO	REF.	PART NO.	NO. REQD.	PART NAME ASSEM. DRWG. NO.	
1 0	7	C-3274	1 (COVER - Centerframe Pump Opening Top	.3
2:	2	C-3275	7 (ASKET - Cover to Centerframe	No.
<u></u>		the majory start class of the first of the start of the first of the start of the s	8 (CAPSCREW 5/8-11-NC x 1 1/4 Lg (St.)	
4	<u> </u>	P2 * 5	8	LOCKWASHER 5/8 SAE Reg (St.)	
5	3	W-518	-	GUIDE - Water Pump Cross-head STREET ELL 1/2 - 45° Std (Brass)	
6 7	4	C-3244	7	CASKET - Guide to Centerframe	
8	5	O.000.2.2	7	CAPSCREW 3/4-10-NC x 2 Lg (St.)	
9		de-springense at 1,000 months in provide for a participa provides at 1,000 months.	17	LOCKWASHER 3/4 SAE Reg (St.)	
L 10 C-6633	6	C-6633L2	2	PTN - Guide to Centerframe Dowel	
11			2.	HALF NUT 1/2-13-NC-Hex (St.)	c. day.
12			2	COTTER PIN 1/16 x 1 Lg (St.)	
13	7	C-3245	1	RING - Water Pump Piston Rod Oil	
14 W-477	- 18 V	X1372	1	BODY ASSEM Water Pump NUT 3/4-10-NC-Hex (Brass)	- 1. 1
15 16		n 2023	4	BOX - Piston Rod Stuffing	
10	9	F-3761 C-3269	7	GASKET - Stuffing Box to Body	
L 17/8	10	0-0200	6	NUT 3/8-16-NC-Hex (Brass)	1
19 >	11	C-3247	1	GLAND - Piston Rod Packing	
20	12	S-3066	1	Num - Piston Rod Packing Gland	
21	13	To the same Andrewson of April 2014 April 2014 (Sept. 2014) April 2014 (Sept. 2014)	10	PACKING5/16 Sq. x 5 Lg(Flax - Belmont #552)
	14	C-3268	1	COVER - Pump Body End	
23	15	C-3269	1	GASKET - Cover to Pump Body	
24		a ra ca	6	NUT 3/8-16-NC-Hex (Brass) PLATE - Water Pump Valve	
25	16	W-473 F-4419	2	GASKET - Valve Plate to Pump Body	
26 27	L(I Lastita	14	NUT 1/2-13-NC-Hex (Brass)	
L 28 20150	18	· 20150-P	12	VALVE - Water Pump Suction & Discharge	
29	19	X1373	1	COVER ASSEM Water Pump Body (Bottom)	
30	20	C-3258	1	BLOCK - Zinc (Progs)	
31			1	CAPSCREW 3/8-16-NC x 1 1/2 Lg (Brass)	
32	21	W-474	1	COVER - Water Pump Body (Top)	
33	22	F-4418	12	GASKET - Top & Bottom Cover to Pump Body NUT 1/2-13-NC-Hex (Brass)	
34			20	PIPE PLUG (Top & Bottom Cover) 1/4 Std. (Brass	3
for any and a second second	0 23	203070-P3	17	FLANGE - Water Pump Suction Pipe	444
37 C=939		C-9392-P	1	RABOW - Pump Suction Air Chamber	*****
38	25	C-3448	2	GASKET - Flange & Elbow to Pump Body	-
39			8	NUT == 5/8=11=NC=Hex. == (Brass)	
□ 20307		203070-P2	11	FLANGE - Water Pump Discharge	
41	27	C-3276	2	CHAMBER - Air - (Pump Suct. & Disch.)	
42			1 60	PIPE PLUG 1 Std (Brass) PIPE PLUG(Suct. Chamber) 1/8 Std (Brass)	1
43	7 00	C-9393-P	3		
44 C-939	3 28	1-9033-P	10	GAPSCREW 5/8-11-NC x 2 Lg (Brass)	3
46			12		
47					7
48					U
7 49			600	CONTINUED ON SHEET NO. 2 CONTINUED	
50			1	MED DIMP CROUP	,
OR OPP. HAND SEE	NAME	CIRCULATIN	G WA	TER PUMP GROUP ORIGINALLY 6 CYL. 13 x 16 MARINE - R.H.	
2L526		TOTAL REQUIREMENTS DES E	NGINE M	JULTIPLY NO. REQ'D GIVEN ABOVE BY NO. REQ'D FOR THIS GROUP GIVEN ON INDEX SHEET	0
	FOR	manuse. The Manusche Michigans and Nicola	, m	ATLAS IMPERIAL DIESEL ENGINE CO.	
ORM NO. 240 10-38		PARTS) L.	OAKLAND, CALIF. MATTOON, ILL.	
				/ · · · · · · · · · · · · · · · · · · ·	

RA:			TYPED BY	MED	DATE 3 = 6 = 41 ISSUEU DATE CHKD. APRVD. Y	
4	-25-41 Ad	ided .	Line 29		Sag	
					CH A N	٠.
				on and the second secon	2L525 SHEET	2
		ALWA FOR S	YS GIVE PART NUMBER TD. HARDWARE WITHOUT INDICATES PART NO	IIIT PA	T NAME - ENGINE NUMBER REPORTED AND SIZE PLATE K-1905 (ED 2)	
LIN	DRWG. NO.	REF.	PART NO.	NO. REQD.	PART NAME ASSEM. DRWG. NO. CONTINUED FROM SHEET NO. 1	
	2			9		a c
	4	35 36		1	NIPPLE (Snift. Valve) 1/8 x 2 1/2 Lg (Brase ELBOW (Snift. Valve) 1/8 Std (Brass)	2.9
****	5 c=9066	37	C-9066-P 1/8	1	CLOSE NIPPLE 1/8 Std (Brass) VALVE - Vertical Check	
	7 C-9045	39	C-9045-P 1/8	1	COCK - Air	
	8					name della d
1	1	10	7/5/27	7	STRAP ASSEM Water Pump Eccentric	
_ 1	² F-3757	40 41	X531 X544	1	ROD ASSEM Water Pump Connecting	processing the second
***	15	42		2	CASTLE NUT 3/4-16-NF-Hex (St.) COTTER PIN 1/8 x 1 1/4 Lg (St.)	And address;
****	16	43	F-3760 X545	1	CROSS-HEAD - Water Pump PIN ASSEM Water Pump Cross-head	
	18	45	C=3266	1	ROD - Water Pump Piston	
	20	46	C=3246	1	HALF NUT(Piston Rod Lock) 1 1/4-7-NC-Hex(S GUARD - Piston Rod Splash	t.
	22	47	U=0240	1	SETSCREW 3/8-16-NC x 7/8 Lg Sq. Hd Cup Point - (St.)	
	23 24	55_	202120	2	PISTON - Water Pump	
	25 26	56	202121 C-3265	12	CUP-LEATHER - Water Pump Piston SPACER - Piston Cup-Leather	
- C. C	27 28	58 59	202122	10	WASHER - Piston Cup-Leather Spacer NUT - Water Pump Piston Retainer	
	29			1	COTTER PIN 1/8 x 1 3/4 Lg (Bronze)	
	31 32					
	33					
	34 35			1		A. 100 to
	36 37					
	38					
	40					
E	42					N
	44 45					72
[46					Z
L	47 48					C
	49 50			CX 122.4	mile Strate CDONE	0
	P. HAND BEE 526 P. ROT, SEE	NAM			ORIGINALLY 6 CYL. 130 x 16 MARTNE - R.H.	N
		FO	PARTS	-	ULTIPLY NO. REQ'D GIVEN ABOVE BY NO. REQ'D FOR THIS GROUP GIVEN ON INDEX SHEET ATLAS IMPERIAL DIESEL ENGINE CO. DAKLAND, CALIF. MATTOON, ILL.	
RM P	NO. 240 10-39		1 / 11 7 1 ~	flages	participation of the second of	

BY EJU DAYE 0/4/52 ped from copy dated 12/31/48. No changes. 2L37 ALWAYS GIVE PART NUMBER -K-1979 FOR STD. HARDWARE WITHOUT PART, NUMBER GIVE DESCRIPTION AND SIZE PART NO DRWG NO HOUSING ASSEM. - Fuel Pump 2C1228 1 X2787 1 GASKET - Housing to Centerframe 201226 CAPSCREW - 5/8-11-NC x 2 Lg. (St.) 3 CAPSCREW - 5/8-11-NC x 4 Lg. (St.) 4 LOCKWASHER - 5/8 SAE Reg. (St.) G CAPSCREW - 1/2-13-NC x 2 3/4 Lg. LOCKWASHER - 1/2 SAE Reg. (St.) 7 PLATE - Fuel Pump Mounting 8 F-6108 5 GASKET - Mounting Plate to Housing 9 201209 PIPE PLUG - 1/4 Std. (C.I.) .0 NUT - 1/2 - 13 NC - Hex. (St.)6 11 LOCKWASHER - 1/2 SAE Reg. - (St.) 2 COVER - Fuel Pump Mtg. Plate Top W-1492 GASKET - Cover to Mounting Plate CAPSCREW - 3/8-16-NC x 3 1/4 Lg. 10 201207 4 15 CAPSCREW - 3/8-16-NC x 2 Lg. (St. G 4 GASKET - Capscrew C-5919 17 PIPE PLUG - 1/2 Std. (C't's'k. Hd. (C.I. .8 PLUG - Mtg. Plate cover By-Pass COVER - Fuel Pump Housing Side GASKET - Cover to Housing 17 C-9512 19 201227 1 30 14 21 15 201208 1 CAPSCREW - 1/2-13-NC x 1 Lg. (St.) 19 4 LOCKWASHER - 1/2 SAE Reg. (St.) 23 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 H.P. FUEL PUMP HOUSING & COVERS GROUP ORIGINALLY 6 CYL. 13 x 16 MARINE PP. ROT. SEE FOR TOTAL REQUIREMENTS PER ENGINE MULTIFLY NO. NEO D'GIVEN ABOVE BY NO. REO D FOR GROUP GIVEN ON INDEX SHEET THE NATIONAL SUPPLY CO. PARTS ENGINE DIVISION SPRINGFIELD, OHIO

DATE 0/4/06 typed from copy dated 3/4/52. No changes. 2L 534 ALWAYS GIVE PART NUMBER - PART NAME - ENGINE NUMBER
FOR STD. HARDWARE WITHOUT PART NUMBER GIVE DESCRIPTION AND SIZE PLATE K-1979 REF. PART NAME DRWG. NO. PART NO HEAD ASSEMBLY - H.P. Fuel Pump X3251 1 51 PLUG - Pump Head (Priming Pump Hole) 52 202160 2 2C2119 GASKET - Plug to Head 53 3 GASKET - Head to Mtg. Plate 54 C-8109 4 CAPSCREW - 1/2-20-NF x 1 1/2 Lg. (St.) 10 55 5 10 LOCKWASHER - 1/2 SAE Reg. - (St.) 6 X2163 VAINE ASSEM. - Fuel Pump Suction 7 56 C-8098 GASKET - Suct. Valve to Pump Head 2 C-8116 8 57 2 RETAINER - Pump Suction Valve C-8118 9 58 2 10 C-8122 59 X2164 PUMP ASSEMBLY - H.P. Fuel 2 GASKET - Pump Body to Head C-8117 11 60 2 NUT - Pump Body to Head 12 C-8119 61 SPRING - Fuel Pump Blunger 2 13 C+8124 62 RETAINER - Pump Plunger Spring 141 2 63 C-8123 CAGE ASSEM. - Fuel Pump Discharge Valve 15 201225 64 X2789 2 2 VALVE - Fuel Pump Discharge 16 C-9225 65 2C1222 2 TEE - Fuel Pump Discharge 17 66 2 PLUG - Discharge Tee Retainer & Bleeder 2C1223 18 67 STEEL BALL - 1/4 Dia. Std. (St.) 2 19 68 20 69 C-6073 PLUG - Discharge Valve Bleeder 21 22 23 PUMP ASSEM. - Fuel Priming X3227 70 24 71 202119 GASKET - Priming Pump to Head COLLAR - Priming Pump Plunger 25 72 1279-BXB3 0 - 7546NUT - 7/16-20-NF-Hex. (St.) 26 73 SHAFT - Priming Pump Lever 27 74 C-8088 LEVER - Priming Pump 28 75 F-6144 KEY - Lever to Shaft 29 76 5-3137 5127 30 77 SETSCREW - 1/4-20-NC x 1/2 Lg. (Sq. Hd. -Cup Pt. (St.) 31 \$2 2 GUIDE - Fuel Pump Cross head 78 C-8084 23 2 GASKET - Guide to Centerframe 34 79 C-8108 CAPSCREW - 1/2-13-NC x 1, 1/2 Lg. 35 6 80 LOCKWASHER - 1/2 SAE Reg. (St.) 36 6 ROD ASSEMBLY - Fuel Pump Connect. X2790 2 37 F-6103 38 82 201188 2 PIN - Connect. Rod & Crosshead 2 CROSSHEAD - Fuel Pump 39 83 2C1187 SIEEVE - Fuel Pump Crosshead GUARD - Crosshead Oil 2 40 C - 55384 831C-RB3 41 S-878 85 831D-RB31 2 42 PLUG - Fuel Pump Crosshead C-8126 86 43 N 44 45 46

PP HAND SEE NAME HIGH PRESSUR

47

48 49 50

ORIGINALLY 6 CYL. 13 x 16 MARINE

FOR TOTAL REQUIREMENTS PER ENGINE MULTIPLY NO. BEO'D GIVEN ABOVE BY NO. REG'D FOR GROUP GIVEN ON INDEX SHEET

FUEL PUMP GROUP

PARTS LIST

THE NATIONAL SUPPLY CO. ENGINE DIVISION SPRINGFIELD, OHIO

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W

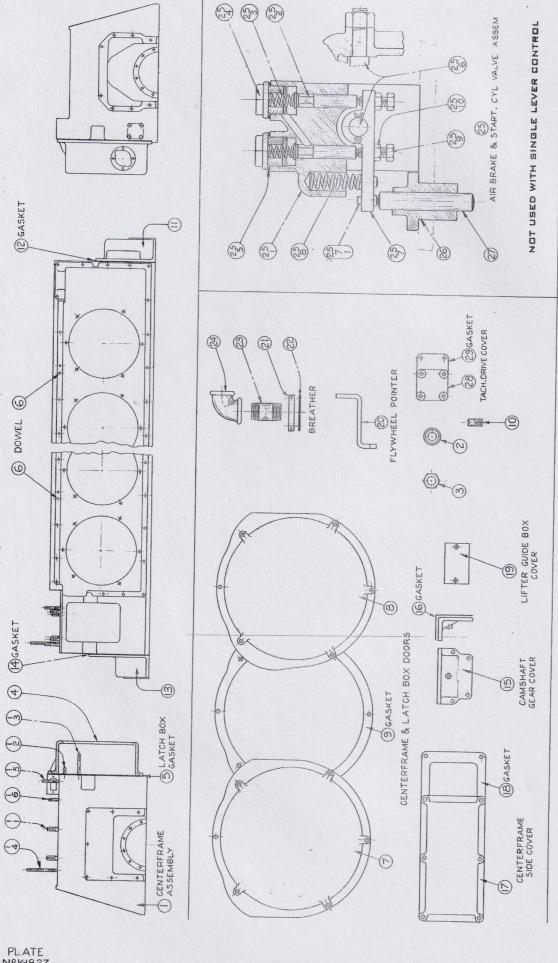


PLATE NºK1827

PA.		TYPE	MED	DATE 4-17-41 ISSUED DATE CHKD. APRVD.
-5-28-41 Li	ne 8	Part No. Wa	s S-9	75
(9 9-4-41 Li 1-7-42 Li	nes 9	& 10 No. Wa	eq'd.	Was 9
11 % 1 Re	SD.			
Added Line	moved es 44.	Part No. F -45-46	-000T	· · ·
		The second secon		2 577
	FOR ST	D HARDWARE WITH	HOUT PAR	NAME - ENGINE NUMBER IT NUMBER GIVE DESCRIPTION AND SIZE OFFI INDIVIDUALLY NO. 1827
INE	* REE	INDICATES PART N	NO.	CED INDIVIDUALLY NO. 12 2001
NO. DRWG. NO.	NO. *	PART NO.	REQD.	ENTERFRAME ASSEMBLY
	2	X2780 S-2707		ASHER - Base to Centerframe Stud
	3	S M V		UT 1 1/4-7-NC-Hex (St.)
4	4	K-1959	1 E	BOX - Latch
5	0 .		. 70 7	CAPSCREW 1/2-13-NC x 1 1/4 Lg (St.)
6	 		39 (OCKWASHER 1/2 SAE Reg (St.)
8,	6		2 1	APER PIN (Dowel) #7 x l Lg (St.)
F-6578	7	692-03	10 1	OOOR - Centerframe & Latch Box (Round)
101	8	C-1074	2 1	DOOR - Centerframe (Round) (Exh. Side - Ends)
11 S-1126	9	692A-03	12 (GASKET - Round Door to Centerframe & Latch Box CAPSCREW 1/2-13-NC x 1 1/4 Lg (St.)
12	10	S-3183		PIN - Dowel (Round Door)
14	11	W=3		COVER - Centerframe Fwd. End (& Crank. Brg.)
15	12	W-9	1 (GASKET - Cover to Centerframe & Base
16	13	W-7	1 (COVER - Centerframe Aft. End (& Crank. Brg.)
17	14	W-10		HASKET - Cover to Centerframe & Base CAPSCREW 1/2-13-NC x 1 1/4 Lg (St.)
18		t mark consistency or . May of the color of	24	LOCKWASHER 1/2 SAE Reg (St.)
$\frac{10}{20}$	15	F-3762		COVER - Camshaft Gear
21	16	C-3249		GASKET - Cover to Centerframe
22		and the company of the contract of the contrac	6	DAPSCREW 1/2-13-NC x 1 1/4 Lg (St.)
23	3.01	COC 07	6 1	JOCKWASHER 1/2 SAE Reg (St.) COVER - Centerframe Side (Ex. Side - Fwd.)
24 F-2954 25	17	696-03 F-2955	1	GASKET - Cover to Centerframe
26		1 0000	6	CAPSCREW 1/2-13-NC x 1 1/2 Lg (St.)
27			6	LOCKWASHER 1/2 SAE Reg (St.)
28	19	C-9155	1	COVER - Centerframe End (Lifter Guide Box) MACHINE SCREW5/16-18 x 5/8 LgFlat Hd(St.)
29 30	20	201288	2	POINTER - Flywheel
31	20	SOIZOO	2	CAPSCREW 1/2-13-NC x 1 1/4 Lg (St.)
32			2	LOCKWASHER 1/2 SAE Reg (St.)
33 C-460	21	779		FLANGE - Breather Pipe
34	22	S-2336		GASKET - Flange to Centerframe CAPSCREW 1/2-13-NC x 1 1/2 Lg (St.)
35 36 .	+		man and the state of the state	CAPSCREW 1/2-13-NC x 1 1/2 Lg (St.) LOCKWASHER 1/2 SAE Reg (St.)
37	23			NIPPLE 2 x 6 Lg (W.I.)
38	24		1	ELBOW 2 Std (M.I.)
39	28	C-8979	1	COVER - Tachometer Drive Hole
40	29	C-7527	1	GASKET - Tachometer Drive Hole Cover CAPSCREW 3/8-16-NC x 7/8 Lg (St.)
41			4	LOCKWASHER 3/8 SAE Reg (St.)
43		1		
-14	5A	F-6928	1	GASKET - Latch Box (Aft End Sect.) GASKET - Latch Box (Gov. End Sect.)
45.	5B	F-6929		CHARLEST L. L. D Thomas U. T. arrange Mary Transport
46	5C	F-6930	2	Strips)
48	+			U
2 49			1	
50				VERS GROUP (SINGLE LEVER CONTROL)
ROPP. HAND SEE	NAME.	CENTERFRAME	& CO	ORIGINALLY & CVI. 13 x 16 MARINE - R.H.
ROPP, ROT, SEE	FOR T	OTAL REQUIREMENTS PER	ENGINE MUL	TIPLY NO, REQ'D GIVEN ABOVE BY NO, REQ'D FOR THIS GROUP GIVEN ON INDEX SHEET
Comment of the second s		DADTE	\$ 10 mm	ATLAS IMPERIAL DIESEL ENGINE CO.
RM NO. 2-0 16.59			Burners I	OAKLAND, CALIF. MATTOON, ILL.
		<u> </u>		The property of the property o

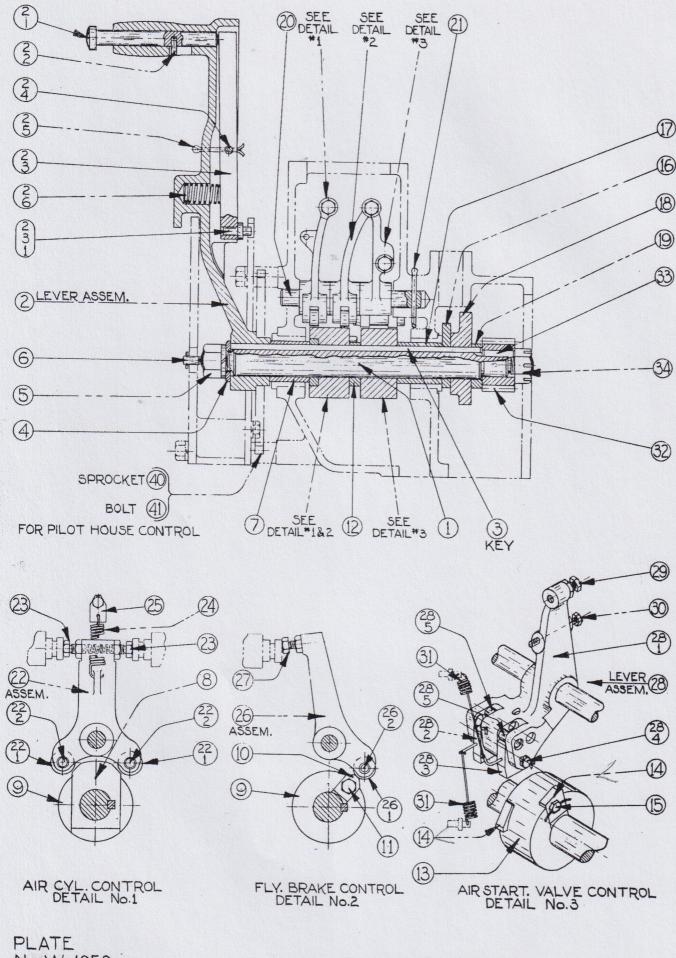
] `		FOR STD. HARDWARE WITHOU	PART NAME—ENGINE NUMBER T PART NUMBER GIVE DESCRIPTION AND SIZE PLATE PLATE PLATE NO.
LINE NO.	DRWG. NO.		NO. PART NAME TRUE DRWG. NO. A-238W-1506
1			Base to Sump Pump (Suct. Line)
2			
3,			NIPPLE 1 x 2 1/2 Lg (W.I.)
4	20160	2C160-P1	
$\frac{5}{6}$:	00100	00100 73	PIPE 1 x 17 Lg. (Thr'd. 2 Ends) - (W.I.) UNION ELBOW
7	20160	2C160-Pl	NIPPLE 1 x 4 1/2 Lg (W.I.)
8		,	TEE 1 Std (M.I.)
9	Cuffichers are as as as the blacks as as as	AMERICAN OF THE PROPERTY OF TH	PIPE PLUG 1 Std (C.I.)
10		A MATERIA CONTINUES OF THE PROPERTY OF THE PRO	CLOSE NIPPLE 1 Std (W.I.)
11		***************************************	Press. Pump to Four Way Cock (At Cooler)
12	·		L CLOSE NIPPLE 1 Std (W.I.)
13			1 ELBOW 1 Std 450 - (M.I.)
14	DATES	20165-Pl	1 NIPPLE 1 x 2 1/2 Lg (W.I.) 1 UNION TEE
1.6	20165	AULUU-FI	1 PIPE PLUG 1 Std (C.I.)
17	The control of the second of the supplementary and the second of the sec		1 PIPE 1 x 38 Lg. (Thr'd. 2 Ends) - (W.I.)
18	10 - 100 to 10 - 10 - 10 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 - 100 -		1 TEE 1 1/4 x 3/4 x 1 Std. Reducing - (M.I.)
19			1 CLOSE NIPPLE 3/4 Std (W.I.)
20			1 TEE 3/4 x 3/4 x 1/2 Std. Reducing - (M.I.)
21			1 CLOSE NIPPLE 3/4 Std (W.I.)
22 23		PG21L 3/4	RELIEF VALVE
24	OCTCO	2C160-P1 1/4	1 PIPE 1 1/4 x 22 Lg. (Thr'd. 2 Ends) - (W.I.) 1 UNION ELBOW
25	20160	ECTOO-LT T.E	1 CLOSE NIPPLE 1 1/4 Std (W.I.)
26	C-9055	C-9055-P1 1/2	1 COCK - Four Way
27	0=0000		4 REDUCING BUSHING 1 1/2 x 1 1/4 Std (C.I.)
28			Four Way Cock to Man. Connect. at Base
29			1 CLOSE NIPPLE 1 1/4 Std (W.I.)
30	20160	2C160-P1 1/4	
32			1 NIPPLE 1 1/4 x 4 Lg (W.I.) 1 ELBOW 1 1/4 Std (M.I.)
33		TO THE RESIDENCE AND ADDRESS OF THE PARTY OF	1 PIPE 1 1/4 x 48 Lg. (Thr'd. 2 Ends)-(W.I.)
34	20160	2C160-P1 1/4	1 UNION ELBOW
35			1 PIPE1 1/4 x 34 1/2 Lg(Thr'ds 2 Ends)(W.I.)
36			1 STREET ELL 1 1/4 Std(M.I.)
37	20160	2C160-Pl 1/4	1 UNION ELBOW
$-\frac{38}{39}$			Four Way Cock to Cooler (Cool. In.) 1 PIPE 1 1/4 x 18 Lg(Thr'ds. 2 Ends)-(W.I.)
40			1 PIPE 1 1/4 x 18 Lg(Thr'ds. 2 Ends)-(W.I.) 1 ELBOW 1 1/4 Std(M.I.)
41			1 NIPPLE 1 1/4 x 2 1/2 Lg(W.I.)
42	20160	2C160-P1 1/4	1 UNION ELBOW
43	~~~~	100 May 100 Ma	1 CLOSE NIPPLE 1 1/4 Std. (W.I.)
44			1 REDUCING BUSHING1 1/2 x 1 1/4 Std. (C.I.)
45		200 400 (000	- Four Way Cock to Cooler (Cool. Out.)
46			1 CLOSE NIPPLE 1 1/4 Std (W.I.)
47 Y	20160	2C160-Pl 1/4	1 UNION ELBOW 1 CLOSE NIPPLE 1 1/4 Std (W.I.)
49			1 REDUCING BUSHING 1 1/2 x 1 1/4 Std. (C.I.)
50			CONTINUED ON SHEET NO. 2
OPP.HAN	ID SEE	NAME LUBE OIL PIR	ING GROUP
DPF.RO	T. SEE		ORIGINALLY 6 CYL. 13 x 16 MARINE
7		FOR TOTAL REQUIREMENTS PER	ENGINE MULTIPLY NO. REG'D GIVEN ABOVE BY NO. REG'D FOR GROUP GIVEN ON INDEX SHEET
240 RE	V. S-42 IM TRANS	PARIS	LIST ATLAS IMPERIAL DIESEL ENGINE CO. OAKLAND, CALIF. MATTOON, ILL.
		IIX	

TRA STORY BW DATE 10-24-44 CHKD M ELBATE 10-24-44

73 Revised and Retyped from 12-11-43 4 4-22-49 Line 24 was PG42

INE	DRWG. NO.	REF.	DICATES PART NOT S	NO.	
0.	DRWG. NO.	NO.	PART NO.	REQD.	PART NAME . ASSEM. No. A-238 W-1506
2				 	CONTINUED FROM SHEET NO. 1
3					Lube Man. Inlet Pipe to Fwd. Cam Brg
1	C-9801		C-9801-P 1/4	***	
5	O-SOOT	1-1-	Casonial TV	7	CONNECTOR - Tube TUBE 1/4 O.D. x .030 x 120 Lg(S.D. Cop.)
6	C-9809		C-9809-P 1/4	1	TEE - Tube
7	V-0000		0-0000-1 1/3	1	TUBE 1/4 O.D. x .030 x 13 Lg(S.D. Cop.)
8	C-9801		C-9801-P 1/4	1	CONNECTOR - Tube
9			40 5		Sam. Brg. Line Tee to Gov. Body
0				1	TUBE 1/4 O.D. x .030 x 17 Lg(S.D. Cop.)
1	C-9804		C-9804-P 1/4	1	ELBOW - Tube
2	C-9832	42 4	C-9832-P 1/4		ELBOW - Tube
3		4		1	TUBE 1/4 O.D. x .030 x 12 Lg(S.D. Cop.)
4	C-9830		C-9830-P 1/4	1	CONNECTOR - Tube
5				-	Lube Man. Inlet Pipe to Press. Gage
6.	C-9804		C-9804-P 1/4	1	ELBOW - Tube
7				1	TUBE 1/4 O.D. x .030 x 60 Lg(S.D. Cop.)
8	C-9801	L	C-9801-P 1/4	1	CONNECTOR - Tube
9	<u> </u>				Reduc. Tee to Relief Valve to Filter
0	C-9801	1	C-9801-P 5/8	3 1	CONNECTOR - Tube
1			0 0000 7 5 //	1	TUBE 5/8 0.D. x .049 x 42 Lg (H.D. Cop.
22	C-9801		C-9801-P 5/8	3 1	CONNECTOR - Tube
4		-	7.2000	179	REDUCING BUSHING 1 x 1/2 Std(C.I.)
5			3A1872	2	OIL FILTER CAPSCREW 1/2-13-NC x 1 1/4 Lg (St.)
26				2	LOCKWASHER 1/2 SAE Reg (St.)
27		W. Y.			Filter to Camshaft Aft Brg.
28				1	REDUCING BUSHING 1 x 3/8 Std (C.I.)
29	C-9804		C-9804-P 1/9	2 7	ELBOW - Tube
30		1	7	1	TUBE 1/2 0.D. x .049 x 11 Lg(H.D.Cop.)
31	G-9801		C-9801-P 1/	3 1	CONNECTOR - Tube
32				1	TEE 3/8 Std (M.I.)
33				1	REDUCING BUSHING 3/8 x 1/8 Std (C.I.)
34	C-9801		C-9801-P 1/	4 1	CONNECTOR - Tube
35	(-		1	TUBE 1/4 0.D. x .030 x 29 Lg(S.D. Cop.)
36	C-9804	 	C-9804-P 1/	4 1	ELBOW - Tube
37					Pipe Tee to Transfer Pump Bearing
38		#	a anno = = /	4	REDUCING BUSHING 3/8 x 1/8 Std (C.I.)
10	C+9808	#	C-9808-P 1/	2 1	TEE - Tube TUBE 1/4 O.D. x .030 x 4 Lg (S.D. Cop.)
41	a anaa	-	0000 5 3 /	4 2	TEE - Tube
12	C-9808	#	C-9808-P 1/	7	COUPLING 1/8 Std. Pipe (M.I.)
13		1		3	CLOSE NIPPLE 1/8 Std (W.I.)
44		1			OBOSE WITTING TO A / O MOUSE THE OWNER OF THE OWNER OWNER OF THE OWNER
15					
16		100			
47					
48				- 1	CONTINUED ON SHEET NO, 3
49	12/14/11	1			
50	M.A.		100		
.HA	ND SEE	NA	LUBE OIL P	IPI	IG GROUP
	Braud Line	1		No.	ORIGINALLY 6 CYL. 13 x 16 MARINE

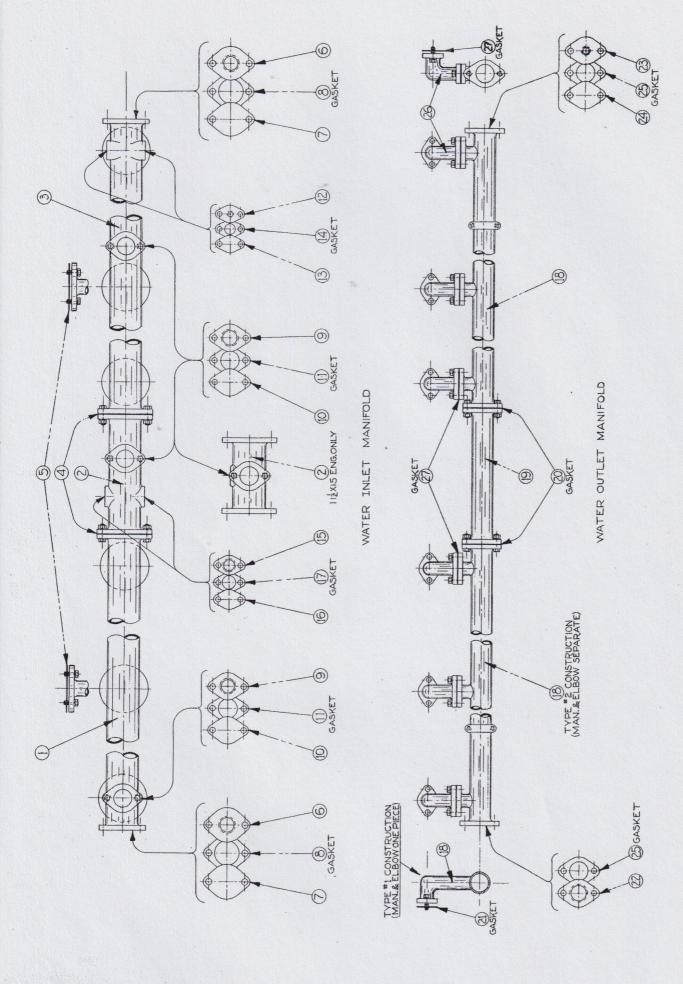
DATE 10-24-44 CHKD. MED DATE 10-24-44 CHANGE 3 OF ALWAYS GIVE PART NUMBER—PART NAME—ENGINE NUMBER
FOR STD. HARDWARE WITHOUT PART NUMBER GIVE DESCRIPTION AND SIZE
* INDICATES PART NOT SERVICED INDIVIDUALLY ASSEM. DRWG. NO. DRWG. NO PART NO PART NAME A-238 -- W-1506 1 ---- CONTINUED FROM SHEET NO. 2 ----2 3 ---- Tube Tee at Trans. Pump to Pump Housing and Press. Pump ----TUBE -- 1/4 0.D. x .030 x 5 Lg. -- (S.D.Cop.) C-9808 C-9808-P 1/4 1 TEE - Tube 6 TUBE(To Press, Pump-Outside)-1/4 O.D. x .030 x 8 Lg. -- (S.D. Cop.) 8 CONNECTOR - Tube C-9801 C-9801-P 1/4 1 Pump Housing (Inside) to Sump Pump ------- Bottom of C-9808 C-9808-P 1/4 1 TEE - Tube 11 TUBE -- 1/4 O.D. x .030 x 12 Lg. -- (S.D. Cop. C-9804-P 1/4 C-9804 ELBOW - Tube 13 Tube Tee to Press. Pump Bearing (Inside) ----14 TUBE -- 1/4 O.D. x .030 x 7 Lg. -- (S.D. Cop.) 15 C-9801 C-9801-P 1/4 CONNECTOR - Tube Tube Tee (at 3/8 Pipe Tee) to Fuel Pump Crank Bearing ---- 1 TUBE -- 3/8 O.D. x .030 x 8 Lg. -- (S.D. Cop. 16 17 C-9804-P 1/4 18 C-9804 ELBOW - Tube 19 20 21 22 23 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 LUBE OIL PIPING GROUP 13 x 16 MARINE OPF. ROT. BEE OF REO'D GIVEN ABOVE BY NO. REO'D FOR GROUP GIVEN ON INDEX SHEET ATLAS IMPERIAL DIESEL ENGINE CO. W 4 240 REV. 12-43 IN TRANS. OAKLAND, CALIF. MATTOON, ILL.



No. W-1858

DO NOT ORDER PARTS BY REF. No.

Tell No					
PART NO	2L601	PART NA	YS GIVE PART NUMBER	ALWA	
1			STD. HARDWARE WITHOU	FOR	
F-6507 2 X3268 1 LEVER ASSEM Engine Control Hand C-6706 3 C-6706L10		NO. REQD.	PART NÓ.		DRWG. NO.
F-6507 2 X3268 1 LEVER ASSEM Engine Control Hand C-6706 3 C-6706L10 4	Control Lever & Cam	1 SHA	F-6548	1	
4		1 LEV	х3268	2	F-6507
5 1 NUT 3/4-10-NC-Hex (St.) 1 LOCKWASHER 3/4 SAE Reg (St.) 1 ALEMITE FITTING #A-336 7 202238 1 SPACER - Hand Lever to Air Cyl. Cam 8 202239 1 CAM - Air Cylinder Control 9 202212 1 HUB - Air Brake Cam 10 202241 1 TOE - Air Starting Cam to Air Start. 12 202265 1 SPACER - AIr Cyl. Cam to Air Start. 13 202213 1 HUB - Air Starting Cam 14 202242 2 TOE - Air Starting Cam 16 202240 2 CAPSCREW - Toe to Hub 2 WIRE #16 Ga. x 6 Lg (St.) 17 202264 1 SPACER - Air Start. Cam to Fuel Cut 16 202240 1 CAM - Fuel Cut-out 18 202191 1 CAM - Fuel Cut-out 18 202191 1 CAM - Governor Control 19 202265 1 SPACER - Gov. Control Cam to Gear 20 202210 1 SHAFT - Air Valve Control Lever 21				3	C-6706
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13	. x 6 Lg (St.)	1 WIR			The state of the s
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2 WIRE #16 Ga. x 6 Lg (St.) 17					nee and and these some a war trapper and the
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40 F-6545 1 SPROCKET - Remote Control	ote Control	1 SPR	F-6545	40	
C-2708 41 C-2708L2 1/4 2 BOLT - Sprocket to Hand Lever		and the second of the second			C-2708
2 NUT 1/2-13-NC-Hex (St.)				-	× 38.1.3.8.9
2 LOCKWASHER 1/2 SAE Reg (St.					
		to the state of th	1	1	



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		á	FOR S	'S GIVE PART NUM I'D. HARDWARE WI' INDICATES PART		ert name-engine number part number give description and size plate K-1924 (ED)	2)
	NO.	DRWG. NO.	REF.	PART NO.	NO REQ		
1	1		1	F-2995	:1	MANIFOLD - Water Inlet (Fwd. Sect.)	
	2	C-424	2	783-06	1	MANIFOLD - Water Inlet (Center Sect.)	
	3		3	F-2996	1	MANIFOLD - Water Inlet (Aft Sect.)	
	1		4	C-443	2	GASKET - Center to End Section	of control and department of a company
	5				4	CAPSCREW 5/8-11-NC x 2 1/4 Lg (St.)	
_	6		-		4	NUT ~ 5/8 ~ 11 ~ NC ~ Hex. ~ (St.)	
	7		4	Total participation of the contract of the con	4	LOCKWASHER 5/8 SAE Reg (St.)	
-	8	tool and to the felt	5	605A∞N	, 6	GASKET - Manifold to Cylinder	
1	9				124	CAPSCREW 1/2-13-NC x 1 1/4 Lg (St.)	
-	10		+		24	LOCKWASHER 1/2 SAE Reg (St.)	
	11	***************************************	6	202062	2	FLANGE - Man. End - (Bilge &Circ. Pump Pine	es)
	12	**************************************	8	S-924	2	GASKET - Flange to Manifold	
	13			Annual plan material segment and materials are not all the segments are unit advanced to a segment	4	CAPSCREW 5/8-11-NC x 1 1/2 Lg (St.)	
T		C-5135	9	787-B	4	LOCKWASHER 5/8 SAE Reg (St.)	. The second of the second
	16	C=1118	10	787 - B	1	FLANGE - Manifold Water Inlet. (Center)	
	17		11	S-1005	3	FLANGE - Manifold Water Inlet (Blind)	
L	18		ollo eda	2-1000		GASKET - Flange to Manifold	
	19	\$100° -00' 10' 10' 10' 10' 10' 10' 10' 10' 10'	<u> </u>	end a divirus per hambororia i resperantario successivo successivo di bere de e confere per una red divirus se	6	CAPSCREW 1/2-13-NC x 1 1/2 Lg (St.)	· · · · · · · · · · · · · · · · · · ·
	20	The same of the sa	12	C-1051	7	LOCKWASHER 1/2 SAE Reg (St.)	
			13	784	+	FLANGE - Air Comp. Pipe	
	22	0.70740	14	S-994	-1-1	FLANGE - Air Comp. Pipe (Blind)	
	23		TE	0-00-5	4	GASKET - Flange to Manifold	
	24			The second section of the second section and the second se	4	CAPSCREW 1/2-13-NC x 1 1/4 Lg (St.) LOCKWASHER 1/2 SAE Reg (St.)	
	25	C-817	15	785-B	i	FLANGE - Spray Valve Cooling Pipe	
L		C-488	16.	785	î	FLANGE - Spray Valve Cooling Pipe (Blind)	
	27		17	S-2334	2	GASKET - Flange to Manifold	
	28	7-7-10 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1		,	4	CAPSCREW 1/2-13-NC x 1 1/4 Lg (St.)	···
	29	100 Mil (100 Mil)			4	LOCKWASHER 1/2 SAE Reg (St.)	
	30			The second secon		Land House Lives	B ANDRES STOTE ON THE STOP
1	31						
	32		18	F-6562	2	MANIFOLD - Water Outlet (End Sect.)	
	33		19	202395	1	MANIFOLD - Water Outlet (Center Sect.)	
_	34		20	S-1005	2	GASKET - Center to End Section	
1	35				4	CAPSCREW 1/2-13-NC x 1 1/4 Lg (St.)	
_	36	A [] []	100	Pd (1) Pd	4	LOCKWASHER 1/2 SAE Reg (St.)	Alabar to William Labor.
	37	C-5135	22	787-B].	FLANGE - Manifold Outlet Pipe	No. of State 2 of To. Advance and Associate
_	38		23	C-5268	1	FLANGE - Man. End - (Air Comp. Pipe)	*** **** *** ****
	39 40		25	S-1005	2	GASKET - Flange to Manifold	
-	41			TATO CONTRACTOR STATE OF THE ST	4	CAPSCREW 1/2-13-NC x 1 1/2 Lg (St.)	and the second second
1	42		06	000706	4	LOCKWASHER 1/2 SAE Reg (St.)	
	43		26	202396	6	ELBOW - Cyl. Head Out. to Manifold	T
(4.1	<u>-</u>	61	S-2334	12	GASKET - Elbow to Head & Manifold .	-
-	45	a matematical from the first production of the second seco			24	CAPSCREW 1/2-13-NC x 1 1/4 Lg (St.)	
11	46	***************************************			Eng Si	LOCKWASHER 1/2 SAE Reg (St.)	N
	47		 				
	48			1877 E.S. 107 (A. 100) A SPECIAL			1
7	49			THE RESIDENCE OF THE PARTY OF T			0
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OP		O SEE	NAME	WATER MANI	FOLD	GROUP	N
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L		*	Control	APTC	A COLUMN TO THE PERSON TO THE	ATLAS, IMPERIAL DIESEL ENGINE CO.	
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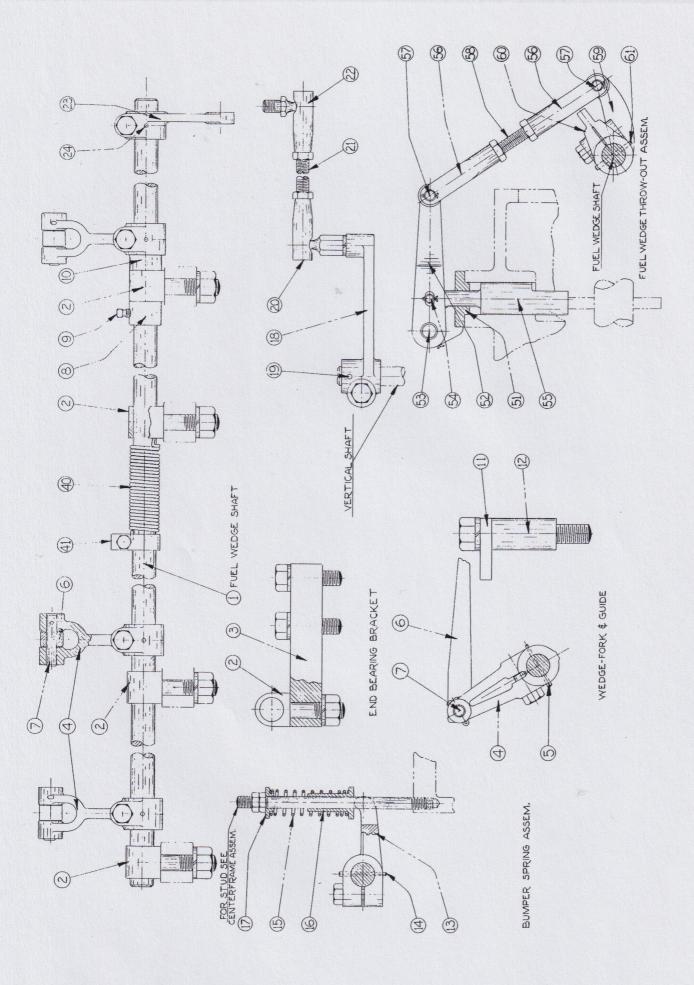
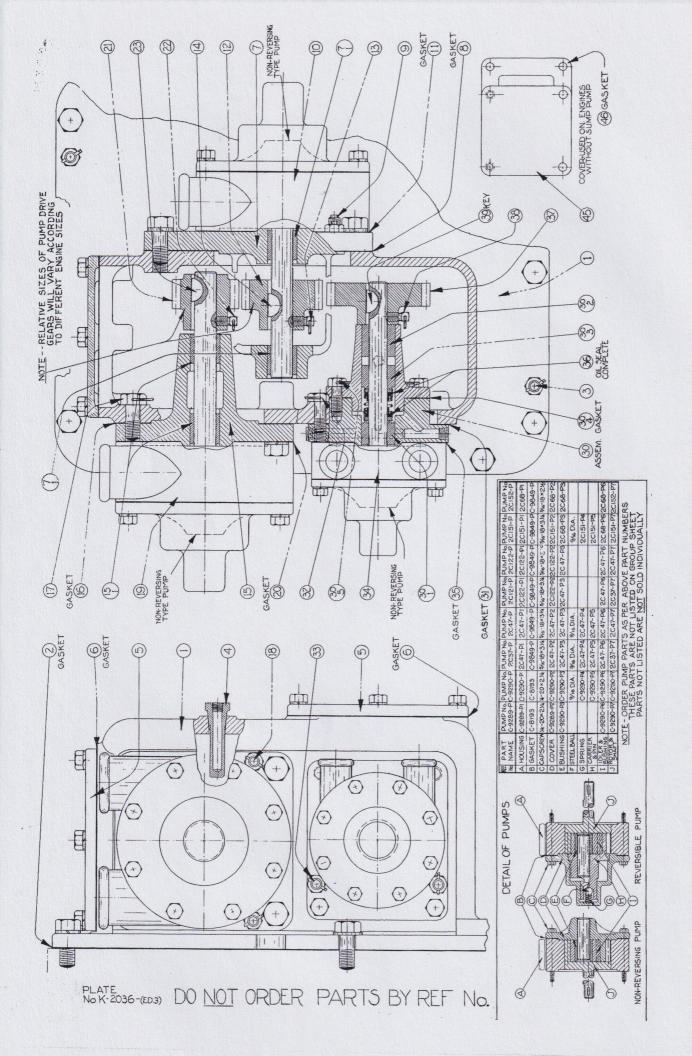


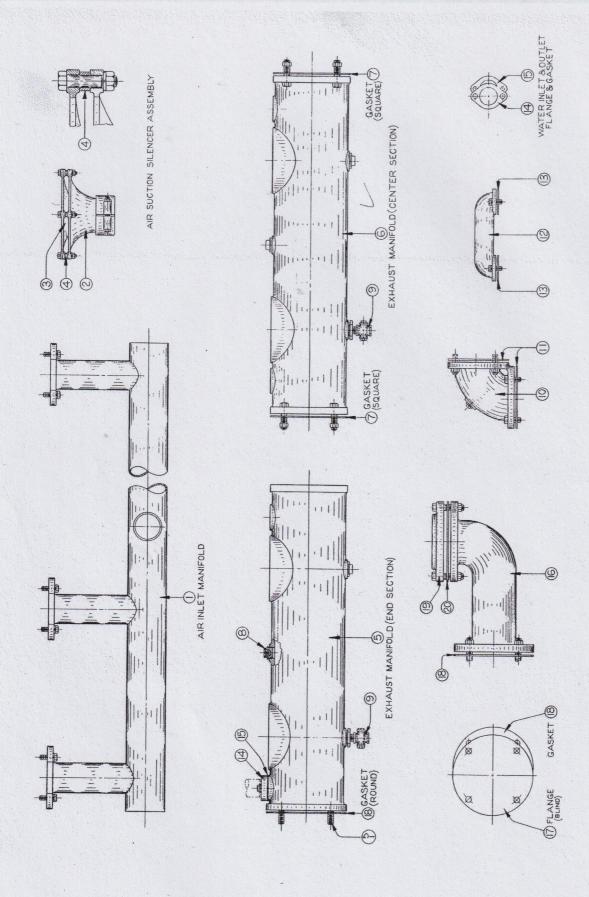
PLATE No. K-2043

DO NOT ORDER PARTS BY REF. NUMBERS

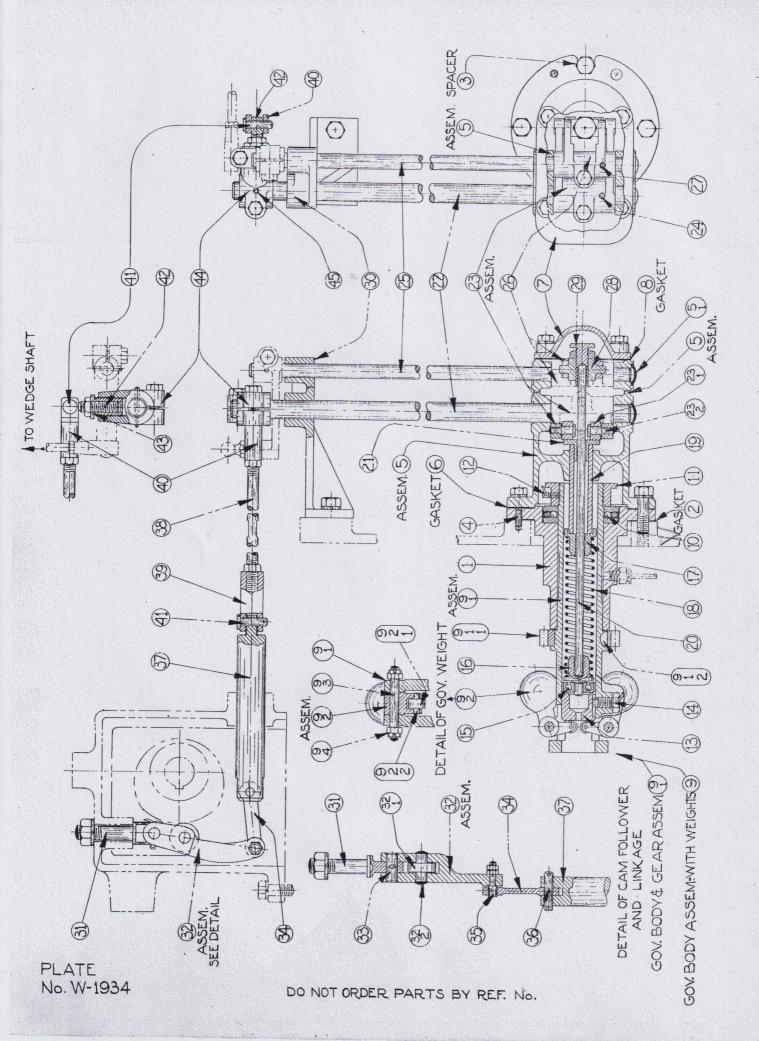
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	FOR S		DUT PA	RT NUMBER GIVE DESCRIPTION AND SIZE PLATE V COAT
LINE DRWG NO	REP		NO.	PART NAME ASSEM.
1	51	202188	REQD.	BRACKET - Wedge Throw-out Lever
2	4-7-1		2	CAPSCREW 3/8-16-NC x 7/8 Lg (St.)
3 - A	60	F-6547	2	LOCKWASHER 3/8 SAE Reg (St.)
5	53	202208	$\frac{1}{1}$	LEVER - Wedge Throw-out PIN - Lever to Bracket
6			ī	COTTER PIN 1/8 x 1 1/4 lg (St.)
7 202260 8	54	ECSS6011 2/8	1	PIN - Lever to Plunger
9	55	202214	2	COTTER PIN 3/32 x 5/8 Lg (St.) PLUNGER - Wedge Throw-out
10	56		2	ROD-END 3/8 SAE Std Adjustable (St.)
11 12	57		2	PIN - Rod-End 3/8 SAE Std (St.)
$\frac{12}{13}$	58	202250	2	COTTER PIN 3/32 x 5/8 Lg (St.) ROD - Wedge Throw-out
14,			2	HALF NUT 3/8-24-NF-Hex (St.)
15	59	202590	1	LEVER - Wedge Throw-out - (Floating)
17	60	202589	1	LEVER - Wedge Throw-out - (Clamped) CAPSCREW 3/8-16-NC x 1 1/4 Lg (St.)
18	61		ī	TAPER PIN #3 x 1 1/2 Lg (St.)
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50	- Page 7	. FUEL WEDGI	TO THE	ROW-OUT GROUP
DU P,HAMD SEE	NAN	AE FURIL WELLIN	u II	ORIGINALLY 6 CVI. 13 × 16 MARINE



TYPEOHJC DATE 3/4/52 CHKD. Tetyped from copy dated 10/10/41. No changes. 2L 705 PLATE K-2036 (Ed 2) FOR STD. HARDWARE WITHOUT PART NUMBER GIVE DESCRIPTION AND SIZE DRWG. NO. PART NO. ADAPTOR ASSEM. - Fuel Transfer Pump X3362 GASKET - Adaptor to Housing CAPSCREW - Adaptor to Housing C2406Ll 1/4 C-2406 WIRE - #16 Ga. x 10 Lg. (St.) CAPSCREW - 3/8 -16-NC x 1 1/4 Lg. (St.) LOCKWASHER - 3/8 SAE Reg. (St.) PIPE PLUG - 1/8 Std. (C.I.) PIN - Adaptor to Housing Dowel C-8265L1 C-8265 PUMP - FuelTransfer C9290-P 0-9290 GASKET - Pump to Adaptor 35 C-8193 CAPSCREW - 1/4-20-NC x 2 Lg. (St.) LOCKWASHER - 1/4 SAE Reg. (St.) OIL SEAL 202478-P GEAR - Transfer Pump Drive SETSCREW - Gear to Pump Shaft WOODRUFF KEY - 1/8 x 3/4 Std. (St.) WIRE - #16 Ga. x 7 Lg. (St.) -50 FUEL TRANSFER PUMP GROUP 13 x 16 A. HAND SEE ORIGINALLY 6 CYL. 11 1/2 x 15 MARINE PP. ROT. SEE FOR TOTAL REQUIREMENTS PER ENGINE MULTIPLY NO. REO'D GIVEN ABOVE BY NO. REO'D FOR GROUP GIVEN ON INDEX SHEET THE NATIONAL SUPPLY CO. PARTS ENGINE DIVISION SPRINGFIELD, OHIO



RA	TO	19-42 T	ine 2º	TYPED BY 7 No. Reg ca.	MED	DATE 10-17-41 SSUED ATE 10-70-41 CHKD APRVD.	
53%	Re	moved L	ine 28	3	98 Ca 60	W W U	
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1						21719	
			FOR ST	'S GIVE PART NUMBER TD. HARDWARE WITHO INDICATES PART NO	UT PA	T NAME-ENGINE NUMBER ART NUMBER GIVE DESCRIPTION AND SIZE PLATE NO. K-1883	
4	LINE NO.	DRWG, NO.	REF. *	PART NO.	NO. REQD	[ASSEM.	district days again, being 4
1	1 2	W-1935	1	X3373		MANIFOLD ASSEM Air Inlet CAPSCREW 5/8-11-NC x 1 3/4 Lg (St.)	
	3				24	LOCKWASHER 5/8 SAE Reg (St.)	
	4 5		3	F-3861 F-2207		SILENCER - Air Suction CONE - Air Suction Silencer.	*** **** *** **
L	6		4	. 201330	8	SPACER - Silencer Cone	
	7 8					CAPSCREW 3/8-16-NC x 1 3/4 Lg (St.) NUT 3/8-16-NC-Hex (St.)	
	9				8	LOCKWASHER 3/8 SAE Reg (St.)	
_	10				2	CAPSCREW(Clamp)1/2-13-NC x 4 1/4 Lg(St.) NUT 1/2-13-NC-Hex (St.)	The same of the sa
	12					A NOTE OF THE PROPERTY OF THE	and the second second second
U	13	**************************************	5	X2418	2	MANIFOLD ASSEM Exhaust (End Section)	
	15		6	F-1280	1	MANIFOLD - Exhaust (Center Section)	
	16		17	C-393	8	GASKET - Manifold Center to End Section CAPSCREW 3/4-10-NC x 3 Lg (St.)	and the second
L	18	emperorand and the status distribution of the state of th	18	C-3288	8	NUT 3/4-10-NC-Hex (St.)	
	20	AND THE RESERVE OF THE PROPERTY OF THE PROPERT		C=3200	2 4	PLUG - Pipe (Water Header Support) PIPE PLUG 1 1/2 Std (C.I.)	
j	21 22				3	REDUCING BUSHING 1 1/2 x 1/2 Std (C.I. CLOSE NIPPLE 1/2 Std (Brass)	.)
	23	C-9053	9	C-9053-P 1/2		COCK - Exhaust Manifold Drain	
	24	F-2975	10	398-R10	6	ELBOW - Cyl. Head Exhaust Outlet PIPE PLUG 1/2 Std (C.I.)	-
	26	S-919	11	760A-R10	12	GASKET - Elbow to Manifold & Cyl. Head	
	27			· ·	48	CAPSCREW 5/8-11-NC x 1 3/4 Lg(St.)	
1	29	C-385	12	4095	2	PIPE - Water By-Pass	
	30		13	S-1005	8	GASKET - By-Pass Pipe to Manifold CAPSCREW 1/2-13-NC x 1 1/4 Lg (St.)	
	32	0 5385	3.4	Ha Cha Lo	8	LOCKWASHER 1/2 SAE Reg (St.)	
	33	C-5135	14	787-B S-1005	2	FLANGE - Exh. Man. Water Inlet & Outlet GASKET - Flange to Manifold	-
	35 36				4	CAPSCREW 1/2-13-NC x 1 1/2 Lg (St.) LOCKWASHER 1/2 SAE Reg (St.)	
	37		16	S-2328	1	ELBOW - Exh. Manifold Exhaust Outlet	
	38		17	C-1104 C-391	1	FLANGE - Exhaust Manifold End (Blind) GASKET - Elbow & Flange to Manifold	×.
	40				8	NUT - 3/4-10-NC-Hex (St.)	
{	41		19	C-6412 C-391	1	FLANGE - Exhaust Outlet Pipe GASKET - Flange to Elbow	
	43				4	CAPSCREW 3/4-10-NC x 3 Lg (St.)	
	45		-	. v	4_	NUT 3/4-10-NC-Hex (St.)	
L	16		1	1			V
	47		1	i ·	1		F
1	-19				!		7
ROF	50) P. HA	NO SEE	NAME	INLET & EAH	AUS	T MANIFOLD GROUP	
ROF	PP. RO	Y. SEE	1	OTAL REQUIREMENTS PER ENG		ORIGINALLY 6 CYL. 13 x 16 MARINE	V
			i j	PARTS	H	ATLAS IMPERIAL DIESEL ENGINE CO.	
AW.	NO. 2	(5 10-59	il I		Beame 24	OAKLAND, CALIF. MATTOON, ILL.	. 4



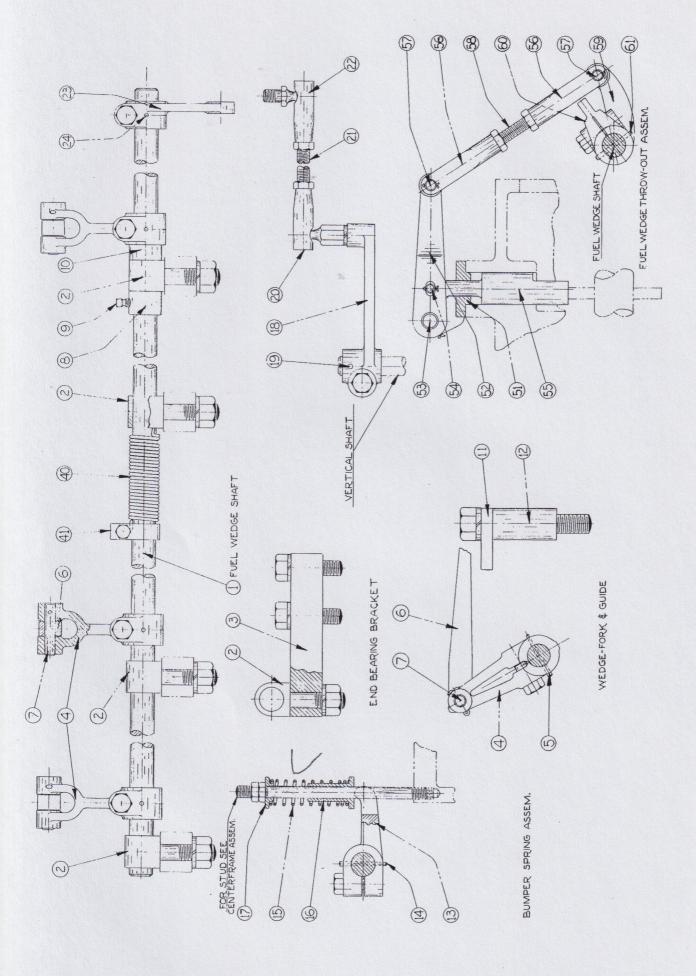
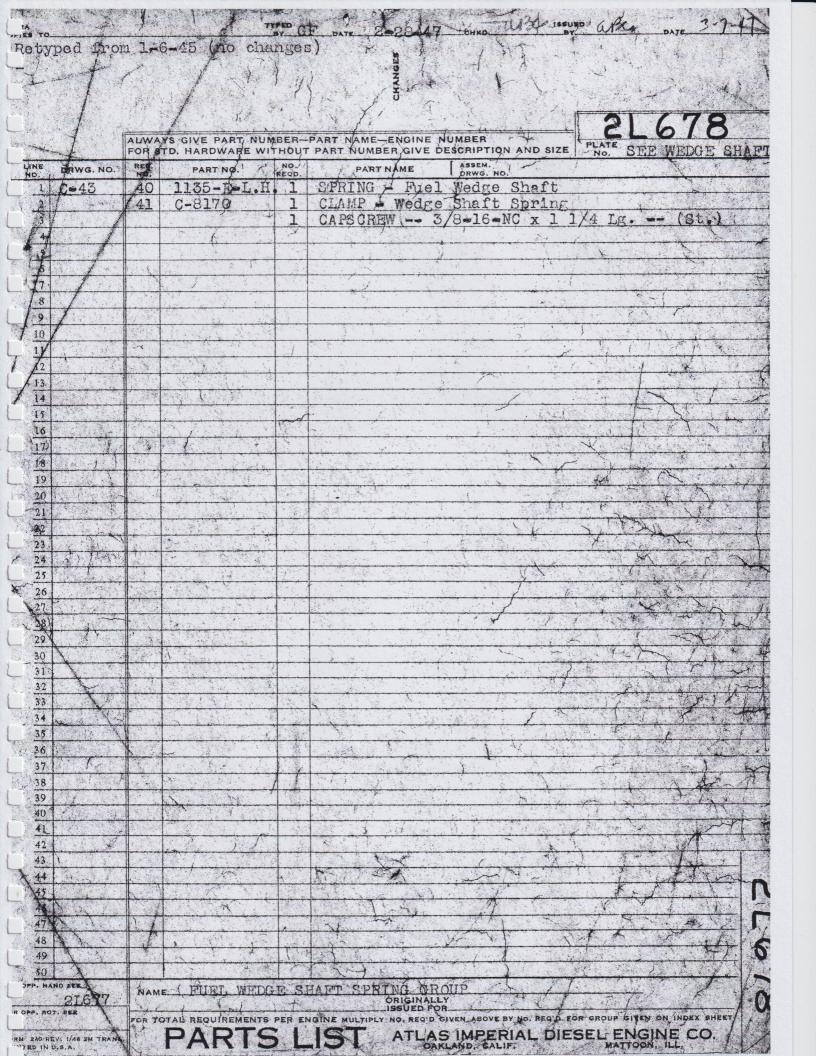
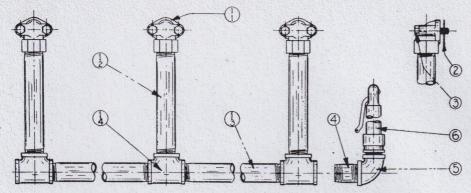


PLATE No. K-2043

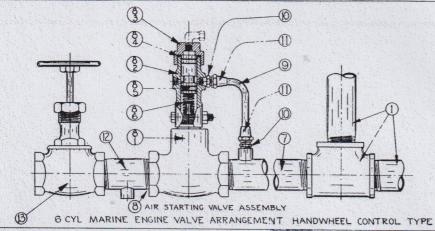
DO NOT ORDER PARTS BY REF. NUMBERS

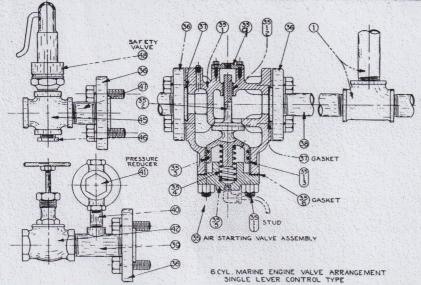
### 1				TYPED	MET	DATE 10-29 0041 ISSUED DATE //-4-6 CHKD. APRVD.					
7-29-42 Lines 19 2 20 No. Rec'd. was a second control of the contr	#1 4	-28-42	Revis	ed.							
The Dawns No	700	7-29-42 Lines 19 & 20 No. Reg'd. was 2									
The Dawns No	, 0										
The Dawn, No											
The Dawn, No						21734					
1	_		ALWA FOR S	YS GIVE PART NUMBER	-PAR	T NAME-ENGINE NUMBER RT NUMBER GIVE DESCRIPTION AND SIZE PLATE TO COAZ					
	LINE		*	INDICATES PART NOT	SER	VICED INDIVIDUALLY NO. N=2040					
2		DRWG, NO.				PART NAME DRWG. NO.					
1	L 1	202069	1				··· •				
1	3	A MINERAL POLICE OF THE PARTY AND	6	0.4004	7	NUT 1/2-13-NC-Hex (St.)	Sept 100 France				
CAPSCREW - 1/2-13-NC x 1 1/2 Lg (St.)	-1	PROFESSION 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1			7	LOCKWASHER 1/2 SAE Reg (St.)	•				
2 LOCKWASHER 1/2 SAE Reg (St.)	5	MOTOR CONTRACTOR OF THE PROPERTY OF THE PROPER	3	0~3385	1		, 40)				
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10 F-897 6 1132-E 6 WEDGE - Fuel 12 S-752 7 1132A-E 6 PIN - Fuel Wedge to Fork 13 14 15 15 15 15 15 15 15	*********	ang pagangan kerangan salah	1 2	ECECTO	6	CAPSCREW 3/8-16-NC x 1 Lg (St.)					
12 S-752 7	-		5			TAPER PIN #3 x 1 1/2 Lg (St.)					
18	Man or the		6	The state of the s							
15			17	1132A-E							
1 SETSGREW1/4-20-NC x 1/2 lgSq.HdCup Pt(St)	-	CONTRACTOR OF THE PARTY OF THE	O	C-7540	ן						
10				1 0-1049	1		t)				
18	16			202587	1	SPACER - Fuel Wedge Shaft					
10 S-2004 12 1141-E 7 SPACER - Fuel Wedge Shaft Guard 7 CAPSCREW 5/8-11-NC x 4 1/2 Lg (St.) 13 2C2583 1 FORK - Wedge Shaft Bumper Spring 1 CAPSCREW 3/8-16-NC x 1 1/4 Lg (St.) 1 TAPER PIN #3 x 1 1/2 Lg (St.) 15 S-2632 1 SPRING - Wedge Shaft Bumper Spring 16 S-2631 1 GUIDE - Wedge Shaft Bumper Spring 17 C-97 1 WASHER - Bumper Spring Retainer 27 2 HALF NUT 3/6-24-NF-Hex (St.) 28 29 20 20 20 20 20 20 20					1						
7 CAPSCREW 5/8-11-NC x 4 1/2 Lg (St.) 21		a			1						
13		S-2004	112	141001	7	CAPSCREW 5/8-11-NC v 4 1/2 Lg (St.)					
1 CAPSCREW - 3/8-16-NC x 1 1/4 Lg (St.)		Canada de la composição d	13	202588	7	FORK - Wedge Shaft Bumper Spring					
1	22		- LO		ī	CAPSCREW 3/8-16-NC x 1 1/4 Lg (St.)					
16		A RESIDENCE MINISTER CONTRACTOR C			1	TAPER PIN #3 x 1 1/2 Lg (St.)					
17	\$100mm 11.148				1						
2					7						
28 29 30		MARKET STREET, MARKET STREET, ST. ST. ST. ST. ST. ST. ST.	- Ja f		2	HALF NUT 3/8-24-NF-Hex (St.)					
18 202636 LEVER - Wedge Shaft Lontrol (On Vert. Shaft) 18 202636 LEVER - Wedge Shaft Control (On Vert. Shaft) 19 1 TAPER PIN - #3 x 1 1/4 Lg (St.) 19 1 TAPER PIN - #3 x 1 1/4 Lg (St.) 19 1 TAPER PIN - #3 x 1 1/4 Lg (St.) 19 1 TAPER PIN - #3 x 1 1/4 Lg (St.) 19 10 INT - Ball & Socket 10 CKWASHER - 3/8 SAE Reg (St.) 10 CKWASHER -	-		1	The second secon							
18 2C2636 1 LEVER - Wedge Shaft Control (On Vert. Shaft) 1 CAPSCREW 3/8-16-NC x 1 1/4 Lg (St.) 1 TAPER PIN #3 x 1 1/4 Lg (St.) 33 19 1 TAPER PIN #3 x 1 1/4 Lg (St.) 34 20 C-8409 1 JOINT - Ball & Socket 35 1 LOCKWASHER 3/8 SAE Reg (St.) 36 21 C-4514 1 ROD - Wedge Shaft Control 2 HALF NUT 3/8-24-NF-Hex (St.) 38 22 C-8410 1 JOINT - Ball & Socket 39 40 1 LEVER - Wedge Shaft Control (On Wedge Shaft) 23 2C2808 1 LEVER - Wedge Shaft Control (On Wedge Shaft) 42 1 CAPSCREW 3/8-16-NC x 1 1/4 Lg (St.) 43 24 1 TAPER PIN #3 x 1 1/2 Lg (St.) 14 44 45 46 47 48 49 49 48 49 49 48 49 49					:						
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1 TAPER PIN - #3 x 1 1/4 Lg (St.)	****	1	178	202000	1	CAPSCREW 3/8-16-NC x 1 1/4 Lg (St.)	10.000				
34			19		1						
36	34			C-8409	1						
2 HALF NUT - 3/8-24-NF-Hex (St.) 22 C-8410 1 JOINT - Ball & Socket 1 LOCKWASHER - 3/8 SAE Reg (St.) 23 2C2808 1 LEVER - Wedge Shaft Control (On Wedge Shaft) 1 CAPSCREW - 3/8-16-NC x 1 1/4 Lg (St.) 24 1 TAPER PIN - #3 x 1 1/2 Lg (St.) 25 2C2808 1 TAPER PIN - #3 x 1 1/2 Lg (St.) 26 1 TAPER PIN - #3 x 1 1/2 Lg (St.) 27 18 19 10 10 10 10 10 10 10 10 10 10 10 10 10	-		1	0 4674	1		Marie Marie III				
1 LOCKWASHER 3/8 SAE Reg (St.) 1 LOCKWASHER 3/8 SAE Reg (St.) 23 202808 1 LEVER - Wedge Shaft Control (On Wedge Shaft) 1 CAPSCREW 3/8-16-NC x 1 1/4 Lg (St.) 1 TAPER PIN #3 x 1 1/2 Lg (St.)			21	· C=4514	1	HALP NUT - 3/8-24-NF-Hey - (St.)	er and a second				
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1 CAPSCREW 3/8=16=NC x 1 1/4 Lg (St.) 43 24 1 TAPER PIN #3 x 1 1/2 Lg (St.) 44 45 46 47 48 49 50	40	!			1		~				
13 24 1 TAPER PIN #3 x 1 1/2 Lg (St.) 43 45 46 56 6 77 48 49 50 6 6 Cyl. 13 x 16 MALINE OPP. ROT. SEE FOR TOTAL REQUIREMENTS PER ENGINE MULTIPLY NO. REO'D GIVEN ABOVE BY NO. REQ'D FOR THIS GROUP GIVEN ON INDEX SHEET ATLAS IMPERIAL DIESEL ENGINE CO.	L	1	23	202808	, ole	LEVER - Wedge Shaft Control (On Wedge Shaft)					
44 45 46 47 48 49 50 NAME FUEL WEDGE SHAFT & CONTROL GROUP—(SINGLE LEVER CONTROL) OPP. NOT. SEE FOR IDIAL REQUIREMENTS PER ENGINE MULTIPLY NO. REQ'D GIVEN ABOVE BY NO. REQ'D FOR THIS GROUP GIVEN ON INDEX SHEET PARTS IN PERIAL DIESEL ENGINE CO.		+	24		1	TAPER PIN - 43 v 1 1/2 Lo (St.)	-1				
15 46 47 48 49 50 NAME FUEL WEDGE SHAFT & CONTROL GROUP-(SINGLE LEVER CONTROL) OPP. HOT. SEE OPP. HOT. SEE FOR TOTAL REQUIREMENTS PER ENGINE MULTIPLY NO. REQ'D GIVEN ABOVE BY NO. REQ'D FOR THIS GROUP GIVEN ON INDEX SHEET PARTS IS ATLAS IMPERIAL DIESEL ENGINE CO.			LAT.		du		n .				
17 48 49 50 NAME FUEL WEDGE SHAFT & CONTROL GROUP-(SINGLE LEVER CONTROL) OPP. ROT. SEE OPP. ROT. SEE FOR TOTAL REQUIREMENTS PER ENGINE MULTIPLY NO. REQ'D GIVEN ABOVE BY NO. REQ'D FOR THIS GROUP GIVEN ON INDEX SHEET WEDGE ATLAS IMPERIAL DIESEL ENGINE CO.	45						O				
ANAME FUEL WEDGE SHAFT & CONTROL GROUP-(SINGLE LEVER CONTROL) OPP. ROT. SEE OPP. ROT. SEE FOR TOTAL REQUIREMENTS PER ENGINE MULTIPLY NO. REQ'D GIVEN ABOVE BY NO. REQ'D FOR THIS GROUP GIVEN ON INDEX SHEET PARTS STATUS IMPERIAL DIESEL ENGINE CO.					1	P					
NAME FUEL WEDGE SHAFT & CONTROL GROUP-(SINGLE LEVER CONTROL) OPP. ROT. SEE OPP. ROT. SEE NAME FUEL WEDGE SHAFT & CONTROL GROUP-(SINGLE LEVER CONTROL) OPP. ROT. SEE FOR TOTAL REQUIREMENTS PER ENGINE MULTIPLY NO. REO'D GIVEN ABOVE BY NO. REQ'D FOR THIS GROUP GIVEN ON INDEX SHEET WATTOON HE				<u> </u>	-		1				
NAME FUEL WEDGE SHAFT & CONTROL GROUP-(SINGLE LEVER CONTROL) OPP. ROT. SEE OPP. ROT. SEE NAME FUEL WEDGE SHAFT & CONTROL GROUP-(SINGLE LEVER CONTROL) OPP. ROT. SEE FOR TOTAL REQUIREMENTS PER ENGINE MULTIPLY NO. REO'D GIVEN ABOVE BY NO. REQ'D FOR THIS GROUP GIVEN ON INDEX SHEET PARTS STATEMENTS PER ENGINE CO.	/	4			·••		, ;				
OPP. NOT. SEE OPP. NOT. SEE FOR TOTAL REQUIREMENTS PER ENGINE MULTIPLY NO. REO'D GIVEN ABOVE BY NO. REQ'D FOR THIS GROUP GIVEN ON INDEX SHEET PARTS IST ATLAS IMPERIAL DIESEL ENGINE CO.						The state of the s					
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PARTS I IST ATLAS IMPERIAL DIESEL ENGINE CO.	OPF. R	OY. SEE	1	TOTAL DEQUIPMENTS ACR. PUR	INF						
CAMIAND CALLE MATTOON BL	L	modern comment of an indicated state of the contract parts		THE PARTY AND THE PARTY AND ADDRESS OF THE PAR	*	His medicine Managarine and the same of the same parts of the same bearing from it for the first of the factor of the same of	,				
	" NO.	249 16 55		LAKID	Bontons						

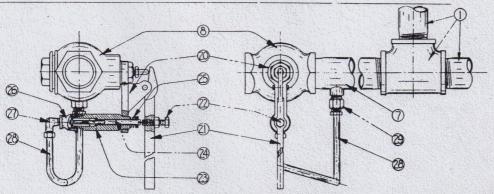




() MANIFOLD ASSEM. -(LESS VALVES)- MARINE & STAT. ENG.







VALVE ARRANGEMENT FOR ALL STAT AND 3 AND 4 CYL. MARINE ENGINES

	· · · · · · · · · · · · · · · · · · ·	TYPED MED DATE 7-25-42 CHKD STOATE 1-31-42 ISSUED APRVD.	
11	4-28-44 L	ine 3 Length was 31 Lo	
		THO O LIGHT WAS US LIGHT	
		211027	
		ALWAYS GIVE PART NUMBER—PART NAME—ENGINE NUMBER FOR STD. HARDWARE WITHOUT PART NUMBER GIVE DESCRIPTION AND SIZE * INDICATES BART NOT SERVICED INDIVIDUALLY NO. W=1624 (F.d. 2)	
	DRWG, NO.	* INDICATES PART NOT SERVICED INDIVIDUALLY REF. PART NO. NO. PART NAME DRWG. NO. REQD. PART NAME DRWG. NO.	
	1 F-6035	1 X1391 1 MANIFOLD ASSEM Air Starting	
Market State of the Control of the C	2:S=922 3 4	2 577A-J 6 GASKET - Manifold to Cyl. Head 3 12 CAPSCREW 5/8-11-NC x 3 1/4 Lg(St.)	
-	5 ,	1 CLOSE NIPPLE 1 1/2 Std (W.I.) 5 1 ELBOW 1 1/2 x 1 1/4 Std. Reducing - (M.I.)	
	6 C-9800	6 C-9800-P1 /4 1 SAFETY VALVE (350 Lbs)	
	7 : 8 :	35 X3358 1 VALVE ASSEM Air Starting	
-	9	36 202633 2 FLANGE - Start. Valve Inlet & Outlet	
	1 :	37 2C2634 2 GASKET - Flange to Valve 8 CAPSCREW 3/4-10-NC x 2 Lg(St.)	
	2 3 : OGF 3 FF7	38 1 NIPPLE(Valve to Man.) 1 1/2 x 6 1/2 Lg. (W.I.)	
1	3 2C3177 4 C-9046	39 X3573 NIPPLE ASSEM Start. Valve to Globe Valve 42 C-9046-Pl /2 GLOBE VALVE	
	5		
-	7 8		
-	9		
	10		
1 2	22		
33	23 24		
	25 26		
1 2	27		
-	9		
	30		
	31 32		
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1 8	85		
	36 : 37 ··		
	38		
1	10		
-	11		
1	13		
	14 145	N	
	16		
5	18		
1	19 50		
1 079	HAND SEE	NAME AIR STARTING MANIFOLD GROUP (SINGLE LEVER CONTROL) ORIGINALLY 6 CYL. 13 x 16 MARINE	
OPF	. ROT. SEE	FOR TOTAL REQUIREMENTS PER ENGINE MULTIPLY NO. REQ'D GIVEN ABOVE BY NO. REQ'D FOR GROUP GIVEN ON INDEX SHEET	
1M 24	D REV. 5-42 1M TRANS	PARTS LIST ATLAS IMPERIAL DIESEL ENGINE CO.	
-	. 1	I the state of the	

etyped from	om 7-25-42 (No	Chan	ges)	
			CHAN	
	FOR STO. HARDWARE WI'	THOUT PA	RT NAME-ENGINE NUMBER RT NUMBER GIVE DESCRIPTION AN	2LIO28
INE DRWG. NO.	REF PART NO.	NO.	PART NAME	ASSEM. DRWG. NO. A-250 RH F-7188 LH
1	CHARLESTON OF STREET CONTRACTOR CONTRACTOR STATES SHOW THE PROPERTY OF THE STATES OF T		Man. to Control Ho	Charles Charles the Same of any agency in Case of the
2 3 5 5		1	NIPPLE 3/8 x 3 L	g (W.I.)
3 0 0003	00003 7 3	1	ELBOW 3/8 Std	(M.I.)
4 C-9801	C-9801-P 1/	2 1	CONNECTOR - Tube	.049 x 130 Ig (H.D. Cop.)
6 C-9809	C-9809-P 1/	2 7	TEL - Tube	• Oda X Ton the . (uene cobe)
7	1,000,1,1,1		and the state of the companies the particular property of the companies of	.049 x 27 Ig(H.D. Cop.)
8		1	TUBE 1/2 0.D. x	.049 x 39 Lg(H.D. Cop.)
9 C-9804	C-9804-P 1/	2 2	ELBOW - Tube	
10	^-	77 - 7	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	A 3
12 C-9801	C-9801-P 1/		e to Fwd. End of Re	v. Cy1
(3 0.0001	A=8001=1 1/	7	CONNECTOR - Tube	.049 x 82 Ig(H.D. Cop.)
4 0-9804	C-9804-P 1/	2 1	ELBOW - Tube	OTO A OR THOU CODS!
15.		1		1/2 x 3/8 Std (C.I.)
16				
17			e to Aft. End of Re	v. Cyl
18 C-9801	¢-9801-P 1/	2 1	CONNECTOR - Tube	.049 x 87 Lg(H.D. Cop.)
0 C-9805	¢-9805-P 1/	2 1	ELBOW - Tube	• Octa X Ol Dis • (B*D* Cob*)
21	V-0000-1 1/	" i	NIPPLE 3/8 x 2 L	æ (W.I.)
22		1	REDUCING BUSHING	1/2 x 3/8 Std (C.I.)
23.		VIT 5		
24	Cont.	Val	e to Fly. Brake	w/o - 3/4 Ch2 /O T \
6 C-9801	C-9801-P 3/	2017	CONNECTOR - Tube	$3/8 \times 1/4 \text{ Std.} - (C.I.)$
27	0-3001-1 0/	1	TUBE 3/8 0.D. X	.035 x 155 Lg. (S.D. Cop.)
28 C-9804	C-9804-P 3/	81	ELBOW - Tube	
20				
30				Start. Man.
31 C-9804	C-9804-P 3/	8 1	ELBOW - Tube	.035 x 153 Lg(S.D. Cop.)
88 C-9804	¢-9804-P 3/	8 1	ELBOW - Tube	· OOO X TOO TR · (D.D. OOD ·)
34				
35	Start	. Mai	. Valve Bleeder	• •
36		1	CLOSE NIPPLE 3/4	Std (W.I.)
87 2C160	20160-P 3/	4 1	UNION EIROW	
39				
40	202413	1	CLAMP - Tube	
41	202402	13	CLAMP - Tube	
12	202403	4	CLAMP - Tube	
43	S-1495	1	CIAMP - Tube	
44		1	MACHINE SCREW1/4-	20 x 3/8 LgRnd.Hd. (St.)
46		1	NUT - 1/4-2U-NU-NE	X (Dto)
47				
48		1 y		
49	H			

OR OPP. HAND BEE

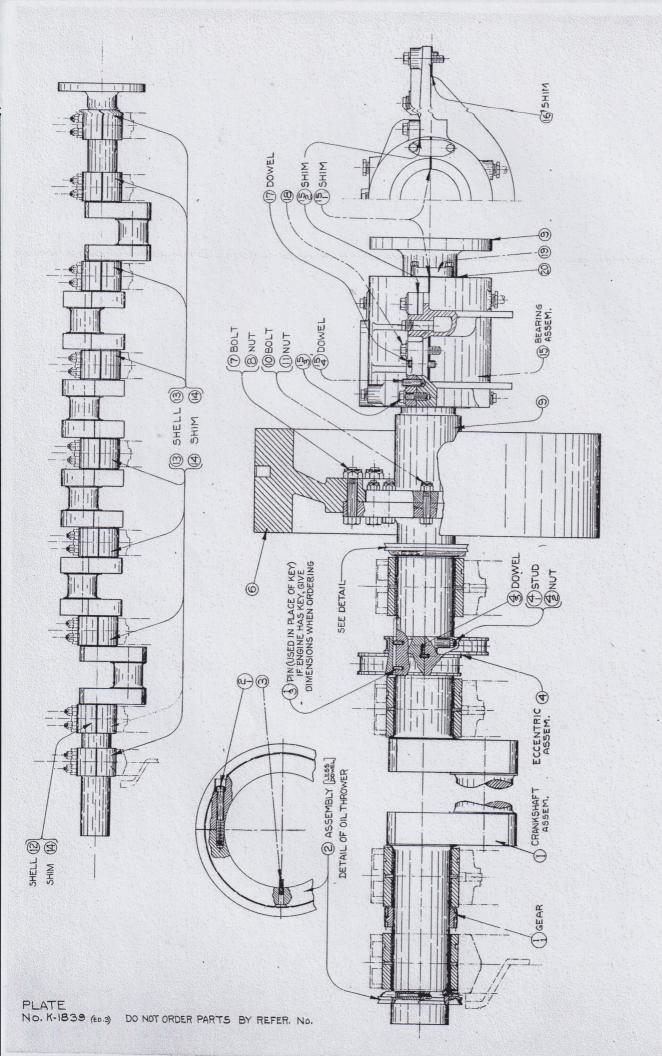
OR OPP. ROT. SEE

DRM 240 REVI 12-49 IN TRANS

ORIGINALLY 6 CYL. 13/x 16 MARINE

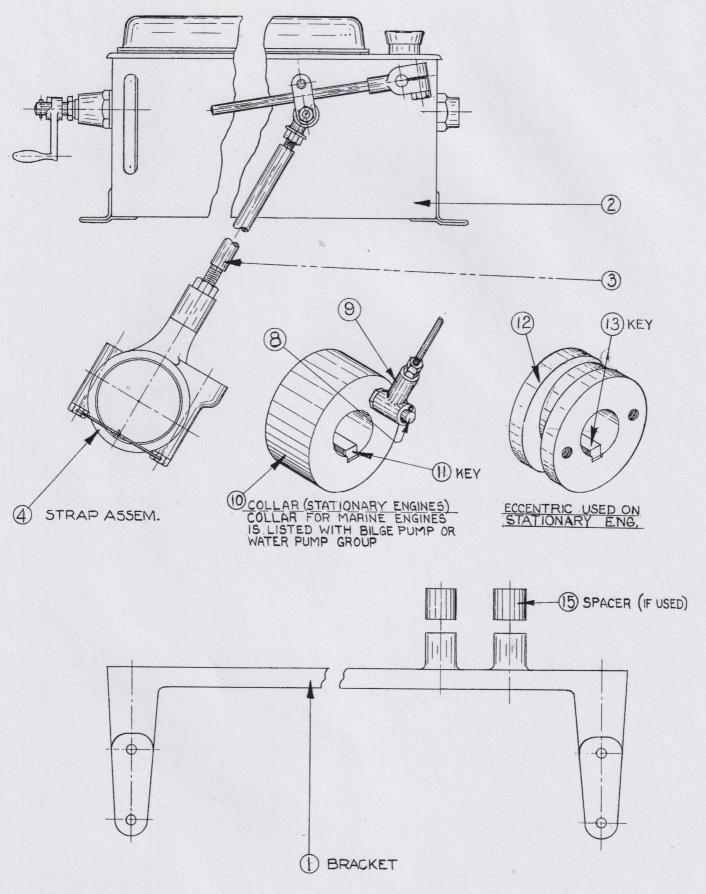
PARTS LIST ATLAS IMPERIAL DIESEL ENGINE CONCENTRATE ON ALLES ON AL

ATLAS IMPERIAL DIESEL ENGINE CO. MATTOON, ILE



4-29-49 Retyped from 9-21-42 (no changes) ALWAYS GIVE PART NUMBER-PART NAME-ENGINE NUMBER K-1839 (Ed 3) FOR STD. HARDWARE WITHOUT PART NUMBER GIVE DESCRIPTION AND SIZE ASSEM. DRWG. NO NO PARTNAME PART NO. NO. CRANKSHAFT ASSEMBLY X2779 1 THROWER ASSEM. - Crankshaft Oil 2 W-1373 X499 PIN - Oil Thrower to Crankshaft Dowel 3 S-2827 3 ECCENTRIC ASSEM. - Air Comp. & Water Pump 4 X530 4 W-314 5 FLYWHEEL 6 W-321 7 C-2620LG 1/2 BOLT - Flywheel to Crankshaft C-2620 CASTLE NUT -- 1 1/4-12-NF-Hex. - (St.)
COTTER PIN -- 3/16 x 2 1/4 Lg. - (St.) 8 9 10 9 W-1426 SHAFT - Thrust 11 BOET - Thrust Shaft to Crankshaft C-2616 10 C-2616L4 3/4 8 12 CASTLE NUT -- 1-14-NF-Hex.- (St.) 11 13 COTTER PIN -- 1/8 x 1 3/4 Lg. - (St.) 14 15 2 | SHELL - Crankshaft Bearing (Fwd. End.) 12 F-3746 16 16 AHELL - Crankshaft Bearing F-2532 13 646-03 17 18 SHIM - Crankshaft Bearing- (1/16) C-6370 14 720A-03-A 18 36 SHIM - Crankshaft Bearing - (1/32 720A-03-B 19 C-6370 14 90 SHIM - Crankshaft Bearing - (.010 C-6370 14 720A-03-D 20 72 SHIM - Crankshaft Bearing - (.003) C-6370 14 720A-03-E 21 22 1 BEARING - Thrust 15 20135P 20135 23 SHIM - Bearing to Base - (1/32) C-8699-B C-8699 16 24 C-8699 16 SHIM @ Bearing to Base - (C-8699-D 8 SHIM - Bearing to Base - (.003) C-8699-E C-8699 16 2 PIN - Thrust Brg. to Base Dowel C-6386L3 1/4 27 C-6386 17 6 | CAPSCREW -- 1-8-NC x 3 3/4 Lg. - (St.) 18 28 LOCKLASHER -- 1 SAE Reg. - (St.) 29 PACKING (Thrust Brg.) -- Garlock #90VS ((or Eq.) 3/8 Sq. x 24 Lg. 31 32 33 34 35 36 37 38 39 40 41 42 43 44 211072 45 47 49 50 CRANKSHAFT FLYWHEEL & THRUST BEARING GROUP - (KINGSBURY) OFP. HAND SEE ON OPP. ROY. SEE FOR TOTAL REQUIREMENTS PER ENGINE

ST ATLAS IMPERIAL DIESEL ENGINE CO.

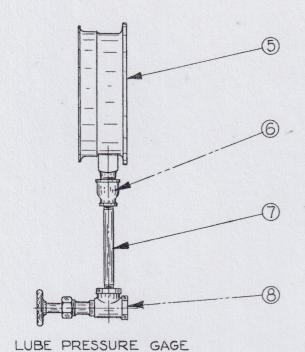


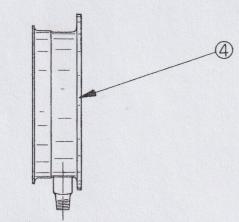
ISSUED M. E.A. APRVD I 6-21-43 Added Line 15 CHANGES Line 4 part number added 1-3-44 73 Line 13 Added Drwg. No. 4-2-46 ALWAYS GIVE PART NUMBER—PART NAME—ENGINE NUMBER FOR STD. HARDWARE WITHOUT PART NUMBER GIVE DESCRIPTION AND SIZE * INDICATES PART NOT SERVICED INDIVIDUALLY LINE DRWG. NO PART NO. PART NAME REQD NO 1 W-168 BRACKET - Lubricator 1061-P4 2 CAPSCREW -- 1/2-13-NC x 3 1/2 Lg. - (St.) 3 LOCKWASHER -- 1/2 SAE Reg. - - (St.) 4 F-7148 LUBRICATOR -- Madison Kipp - R.H. Side Drive 2 F-7148-P12 5 12 Feed 6 CAPSCREW -- 3/8-16-NC x 1 1/4 Lg. 7 NUT -- 3/8-16-NC-Hex. -- (St.) 8 LOCKWASHER -- 3/8 SAE Reg. - (St.) 9 PLAIN WASHER -- 3/8 SAE Std. - (St.) 10 202035 ROD - Lubricator Drive 11 NUT -- 1/2-20-NF-Hex. - (St. 12 NUT -- 3/8-16-NC-Hex. - (St.) 13 F-6940 X498 STRAP ASSEM. - Lub. Drive Eccentric 14 WIRE -- #16 Ga. x 9 Lg. - (St.) 15 C-8477Ll 1/4 4 SPACER - Lub. Bracket to Cyl. 15 C-8477 16 Piping - (Cam Side) -------- Lubricator 17 TUBE(Cyl #1)--1/4 ODx .030x 24 Lg.-(S.D. Cop. .18 TUBE(Cyl #2)--1/4 ODx .030x 46 Lg.-(S.D. Cop.) 19 TUBE(Cy1 #3)--1/4 ODx .030x 68 Lg.-(S.D. Cop. 20 TUBE(Cyl #4)--1/4 ODx .030x 90 Lg.-(S.D. Cop.) 21 TUBE(Cyl #5) -- 1/4 ODx .030x 112 Lg. - (S.D. Cop.) 22 TUBE(Cyl #6)--1/4 ODx .030x 134 Lg. - (S.D. Cop. 23 C-9832 C-9832-P 1/4 6 ELBOW - Tube 24 Lubricator Piping - (Exhaust Side) ----25 TUBE(Cyl #1) -- 1/4 ODx .030x 34 Lg. - (S.D. Cop. 26 TUBE(Cyl #2)--1/4 ODx .030x 56 Lg.-(S.D. Cop.) 27 TUBE(Cyl #3)--1/4 ODx .030x 78 Lg.-(S.D. Cop.) 28 TUBE(Cyl #4) -- 1/4 ODx .030x 100 Lg. - (S.D. Cop. 29 TUBE(Cyl #5)--1/4 ODx .030x 122 Lg.-(S.D. Cop. 30 TUBE(Cyl #6) -- 1/4 ODx .030x 144 Lg. - (S.D. Cop. 31 ELBOW - Tube C-9832-P 1/4 6 C=9832 32 33 ---- Lubricator Oil Tube Clamps 34 CLAMP - (2 Tube S-1492 35 S-1493 CLAMP -(3 Tube 36 CLAMP -S-1494 (4 Tube 37 S-1495 CLAMP -(5 Tube) 38 S-1496 CLAMP -(6 Tube) 39 MACHINE SCREW--1/4-20 x 5/8 Lg.-Rnd. Hd.-(St.) 40 23 NUT -- 1/4-20-NC-Hex. - (St.) 41 42 43 --- Governor Oil Tube ----44 TUBE--1/4 O.D. x .030 x 14 Lg. - (S.D. Cop.) 45 ELBOW - Tube C-9832 C-9832-P OIL CUP--1/8 Hinged Lid-Gits 802 or Eq. (St) 46 47 48 49. 50 OPP.HAND SEE GROUP LUBRICATIOR 311143 ORIGINALLY 6 CYL. 13 x 16 MARINE OPF. ROT. SEE FOR TOTAL REQUIREMENTS PER ENGINE MULTIPLY NO. REQ'D GIVEN ABOVE BY NO. REQ'D FOR GROUP GIVEN ON INDEX SE ATLAS IMPERIAL DIESEL ENGINE

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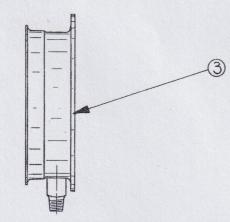
MATTOON II

OAKLAND, CALIF.

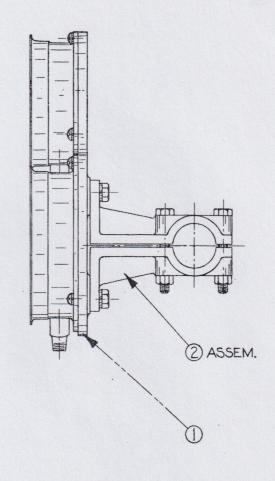


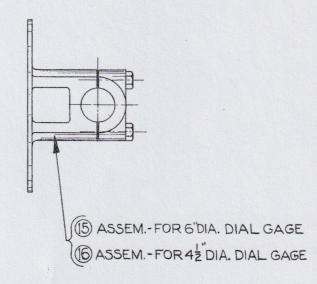


AIR PRESSURE GAGE



FUEL PRESSURE GAGE





PRESSURE GAGE GROUP

LINE

NO.

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OR OPF. HOT. SEE

IM BOND

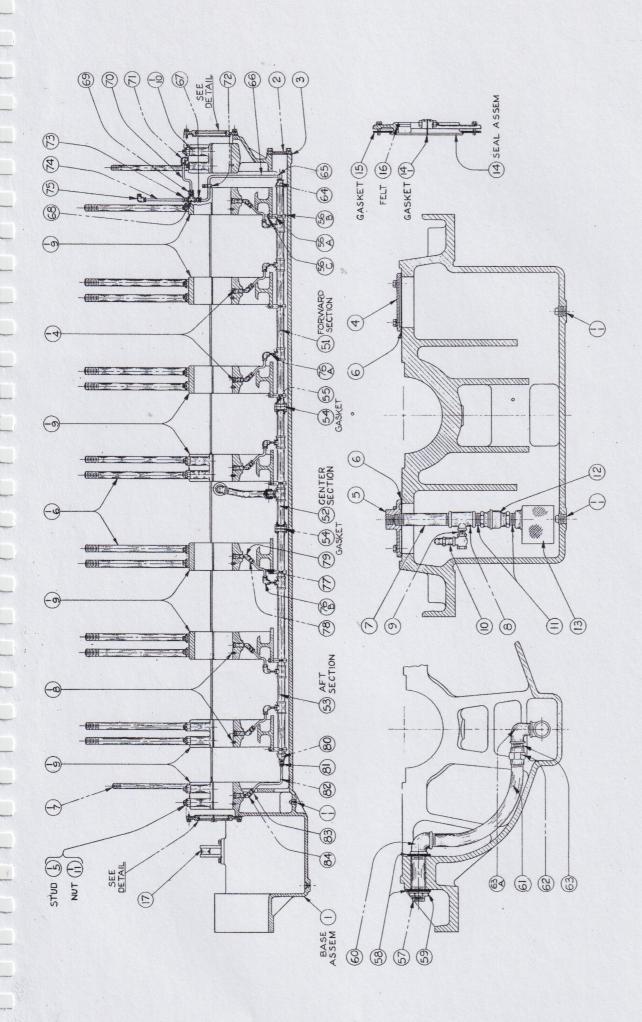
RM 240 REV

FOR TOTAL REQUIREMENTS PER ENGINE MULTIPLY NO. REQ'D GIVEN ABOVE BY NO. REQ'D FOR GROUP GIVEN ON INDEX SHEET

PART

ATLAS IMPERIAL DIESEL ENGINE CO. MATTOON, ILL. DAKLAND, CALIF.

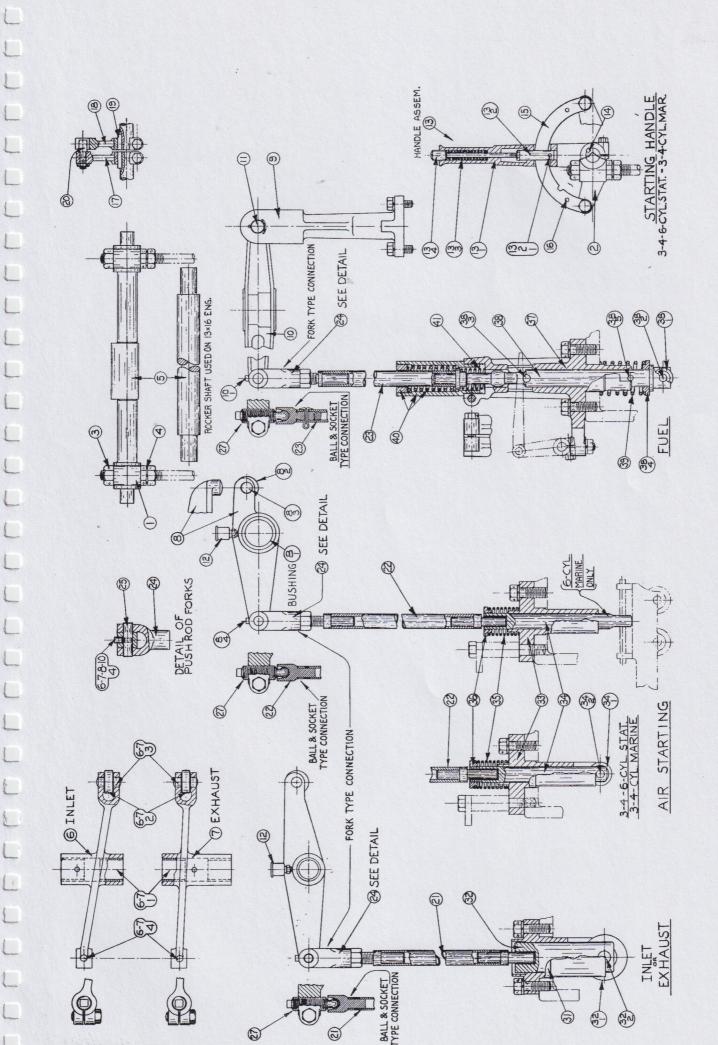
R		TY DIED DATE 9-21-42 PHKD/4.8.0 DATE 9-21-4 - ISSUED/4.8.0 APRVD	
4.1	5-12-43 C Galv.	hanged Mat'l. Brass to	•
	The Color of the	CHANGES	
		j	
		ALWAYS GIVE PART NUMBER—PART NAME—ENGINE NUMBER FOR STD. HARDWARE WITHOUT PART NUMBER GIVE DESCRIPTION AND SIZE PLATE	-
	LINE DRWG. NO.	* INDICATES PART NOT SERVICED INDIVIDUALLY NO.	-
	1	Bilge Pump to Water Inlet Man	_
	3	1 NIPPLE 2 x 5 1/2 Lg (Galv. Iron) 1 TEE 2 Std (M.I.)(Galv.)	<u>.</u>
	4	1 NIPPLE 2 x 2 1/2 Lg (Galv. Iron)	_
	5 C-5135	787-B 1 FLANGE - Air Chamber	
	7	F-2827 CHAMBER - Air 1 PIPE PLUG 1 Std (C.I.)(Galv.)	
	8	S-1005 1 GASKET - Flange to Air Chamber	·
	9	2 CAPSCREW 1/2-13-NC x 2 Lg (St.) 2 NUT 1/2-13-NC-Hex (St.)	
	11	2 LOCKWASHER 1/2 SAE Reg (St.)	
_	12	1 NIPPLE 2 x 3 1/2 Lg. (Gelv. Iron)	
	14	1 ELBOW 2 Std 45° - (M.I.)(Calv.) 1 CLOSE NIPPLE 2 1/2 Std (Galv. Iron)	-
	15 C=9054	C-9054-P2 1 COCK - Three Way	_
	17	1 NIPPLE 2 x 5 Lg (Galv. Iron)	-
	18		_
	20		-
	21		
	22		
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L	46		J
	47 ;	T,	
1	49		
BOI	50 ;	WATER PIPING GROUP	
1	PP. ROT. SEE	ORIGINALLY 6 CYL. 13 x 16 MARINE	:
1	1	FOR TOTAL REQUIREMENTS PER ENGINE MULTIPLY NO. REQ'D GIVEN ABOVE BY NO. REQ'D FOR GROUP GIVEN ON INDEX SHEET	
- mi	240 REV. 5-42 IM TRANS IM BOND	PARIS LIST ATLAS IMPERIAL DIESEL ENGINE CO.	1
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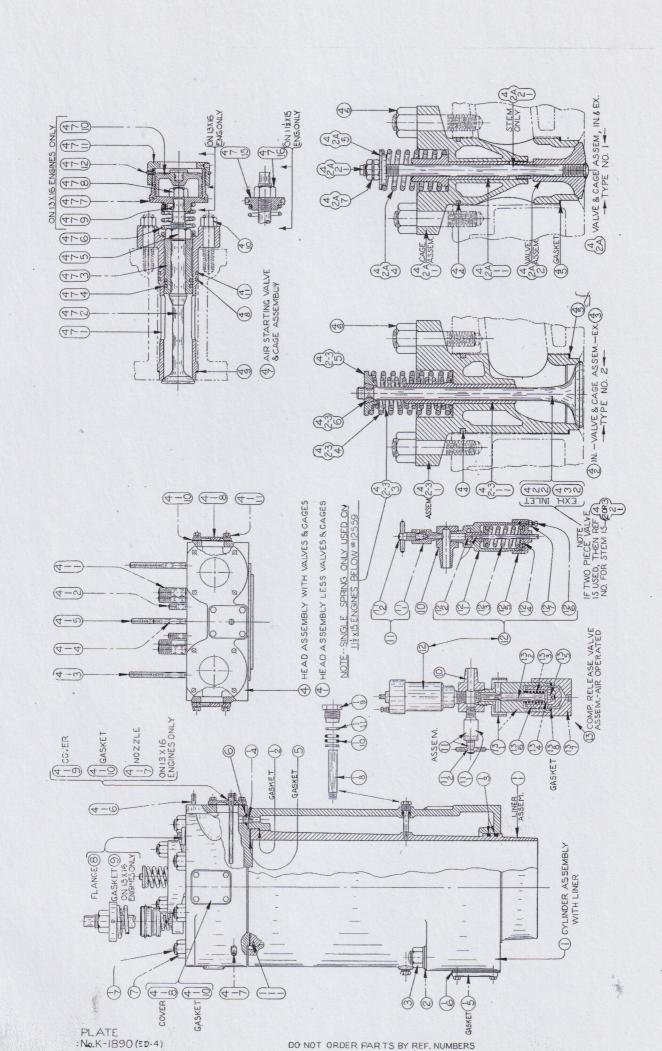
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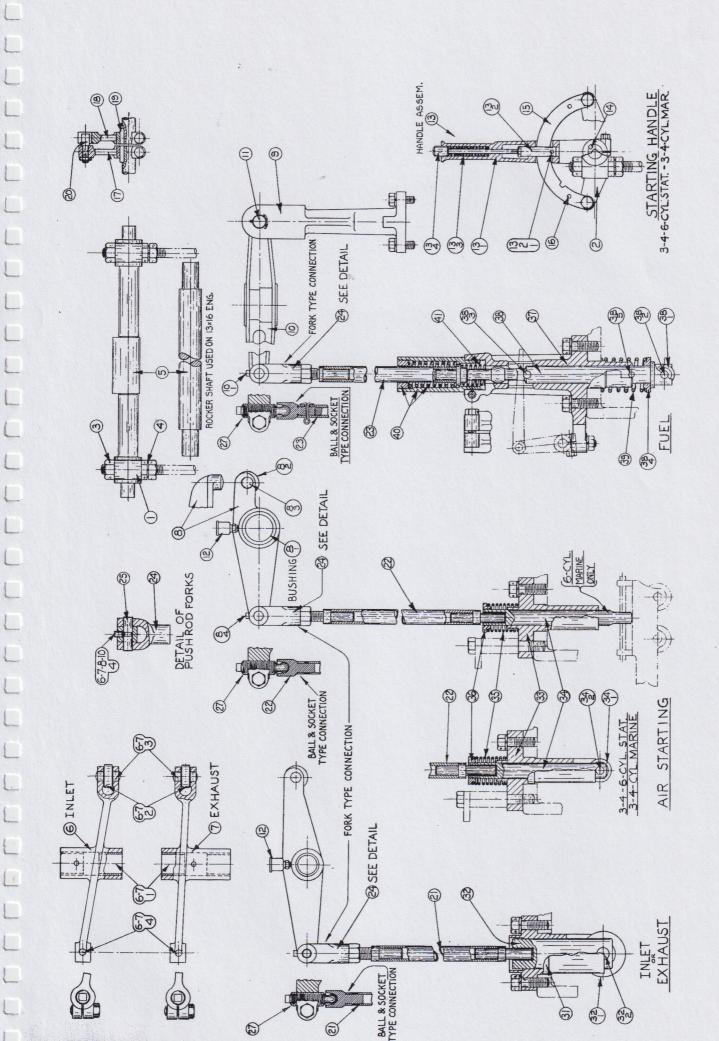
TYPED ABC NATE 5-21-46 CHKD 211 TO ISSUED									
styped from 12-17-42 (no change)									
	I								
The same of the same	ALWAYS GIVE PART NUMBER-	PART NAME ENGINE NUMBER							
	FOR OTD. HARDWARE WITHOU	PART NUMBER GIVE DESCRIPTION AND SIZE NO. K-2019							
LINE DRWG, NO.	PART NO. REGD.	PART NAME ASSEM. No. K-2001							
² F-6586	57 X3047 1 52 X3321 1	MAN IFOLD ASSEM Lube Oil (Fwd. End Sect.) MAN IFOLD ASSEM Lube Oil (Center Sect.)							
3 F-6132	53 X2776 1	MANIFOID ASSEM Lube Oil (Aft End Sect.)							
4 /	54 201299 2	GASKET - Manifold Flange							
5 C-2508/	55 C-2508I2 8	BOIT - Manifold Flange CASTLE NUT 1/2-20-NF-Hex (St.)							
7	2	WIRE #16 Ga. x 10 Lg (St.)							
8	56A 2C2484 7	SPACER - Lube Manifold							
10 C-2408	56B 202485 7 560 0-2408L4 14	CLAMP - Lube Manifold							
10 C-2408	560 C-2408I4 14	WIRE #16 Ga. x 6 Lg (St.)							
12	Base to Mar								
<u> 13</u>	57 C-6430 1	NIPPLE - Lube Oil Connect. (Thru Base)							
C-5145	58 C-8184 2 59 367-7 1	WASHER - Lube Oil Nipple Seal LOCKNUT - Lube Oil Nipple							
16.	60 1	ELBOW 1 1/4 Std (M.I.)							
17)	61	PIPE 1 1/4 x 18 1/2 Lg. (Thr'd. 2 Ends) (W.I.							
18 2C157	62 2C157P1 1/4 1	UNION							
19 /	63 1 63A 1	CLOSE NIPPLE 1 1/4 Std (W.I.) STREET ELL 1 1/4 Std (M.I.)							
21.	Manifold to								
3 22	64 1	REDUCER (Bell) 1 1/4 x 1/2 Sto (M.I.)							
23 C-9804	65 C-9804P 5/8 1	TUBE 5/8 0.D. x .049 x 30 Lg(H.D. Cop.)							
25 C-9801	67 d-9801P 578 1	TUBE 5/8 0.D. x .049 x 30 Lg(H.D. Cop.)							
26	68	TEE 1/2 x 3/8 x 3/8 Std. Reducing - (M.L.)							
27 0-9801	69 C-9801P 1/2 1	CONNECTOR - Tube							
29 C-9804	71 C-9804P 1/2 1	TUBE 1/2 0.D. x .049 x 18 Lg (H.D. Cop.)							
30	72 201332 1	CLAMP - Tube							
31 32		CAPSCREW 1/4-20-NC x 1/2 Lg (St.) LOCKWASHER 1/4 SAE Reg (St.)							
33.	Fwd. Beari	LOCKWASHER 1/4 SAE Reg (St.)							
34 C-9801	73 0-9801P 1/2 1	CONNECTOR - Tube							
36 C-9801	74 1 75 C-9801P 1/2 1	TUBE 1/2 O.D. x .049 x 14 Lg (H.D. Cop.) CONNECTOR - Tube							
37.	13 0-96011 1/2 1	TEE 3/8 Std (M.I.)							
38	1	CLOSE_NIPPLE 3/8 Std (W.I.)							
39.	76A Manifold t	NIPPIE 3/8 x 1 3/4 Lg (W.I.)							
41 C-9805	76B C-9805P 1/2 7	ELBOW - Tube							
42	77 7	TUBE 1/2 0.D. x .049 x 9 Lg (H.D. Cop.)							
43 0-9801	78 C-9801P 1/2 7	STREET ELL 3/8 Std 450 - (M.I.)							
45		o Aft. Crenk. Brg							
46	80 1	REDUCER (Bell) 1 1/4 x 3/8 Std. = (N.I.)							
47 C-9801	81 C-9801P 1/2 1	TUBE 1/2 0.D. x .049 x 14 Lg (B.D. Cop.)							
49 c-9801	82 0-9801P 1/2 1	CONNECTOR - Tube							
50	84 1	STREET ELL 3/8 Std 450 -AM.I.							
OPP. HAND BEE.	NAME LUBE OIL MANI	ORIGINALLY 6 CYL. 13 x 16 MARTNE							
OPP, HOT. SEE	FOR TOTAL REQUIREMENTS PER E	NGINE MULTIPLY NO. REQ'D GIVEN ABOVE BY NO. REG'D NOR GROUP GIVEN ON INDEX SHEET							
IN 240 REV. 1/48 EN TRANS	PARTS	IST ATLAS IMPERIAL DIESEL ENGINE CO.							

A S TO	-	1	TY	PEDA I	30 DATE 7-24-46 CHIP CONTYSSUED 000 DATE 7-29-				
The Board of	ped from	1/12.	-17-42' (no cl	nang	(08)				
				1	1 8				
		A 1.347A	Ve ove pape Mun	OFF	PART NAME-ENGINE NUMBER				
		FOR S	TD. HARDWARE WIT	HOU	PART NUMBER GIVE DESCRIPTION AND SIZE PLATE				
INE	DRWG. NO.	REF.	PART NO.	NO.	PART NAME ASSEM.				
1			F-6911	1	MANIFOLD - Latch Shaft Oil (Fwd. Sect.)				
_2		1.	F-6910	1	MANIFOLD - Latch Shaft 011 (Aft Sect.)				
_ 3			The state of the s	2	PIFE CAP 1/8 Std (M.I.)				
4	~ ~ ~ *		S-2810	5	CLAMP - Manifold				
6	C-2404		C-2404L 1/2	5	CAPSCREW Clamp to Latch Box LOCKWASHER 1/4 SAE Reg (St.)				
7				5	WIRE #16 Ga. x 6 Lg (St.)				
8	-3 5 1	, J			11 10 100 100 100 100 100 100 100 100 1				
9		1							
10	1	7	I	nt.	Gear Tee to Latch Shaft Fwd. Manifold				
11	1			1	REDUCING BUSHING - 3/8 x 1/8 Std (C.I.)				
2 2 7 7 6	C-9801		C-9801P 1/4	1	CONNECTOR - Tube				
13	c-9805		C-9805P 1/4	1	TUBE 1/4 O.D. x .030 x 32 Lg (S.D. Cop. ELBOW - Tube				
14	0-9000	7 18 34	0-2000r 1/4	1	Dubow - Tube				
16	7	1	- Lube Oil	Lin	(On Exh. Side of Eng.) to Aft Manifold				
17	1				ation of this connection to Lube Pressure Line				
18	X-2			on 1	xhaust Side of Engine will vary & therefore				
10	2: 200			rub	length given below is maximum that will be				
20	2			req	ired.				
21	0.000		a 000 to 2 /2	1	REDUCING BUSHING 1/2 x 1/8 std (C.I.)				
22 23	C-9804		C-9804P 1/4]	TUBE 1/4 0.D. x .030 x 50 Lg (S.D. Cop.				
	C-9805		C-9805P 1/4	1	ELBOW - Tube				
25	0-000		C-3865	1	NIPPLE (Thru Latch Box)				
26				1	LOCKNUT 1/8 Std. Pipe - (M.I.)				
27			C-5919	1	GASKET - Locknut				
28	 	,	7.50	1_	ELBOW 1/8 Std (M.I.)				
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50 P. H.	ND SEE	1 . 3	- LATCH SHAF	m o	IL PIPING GROUP				
		NAM	E DATON SHAP	7 0					
P. RC	TA, SEE	FOR TO	TAL REQUIREMENTS	PER E	ISBUED FOR 6 CYT 1.3 X 16 HARTING				
					IST ATLAS IMPERIAL DIESEL ENGINE CO.				



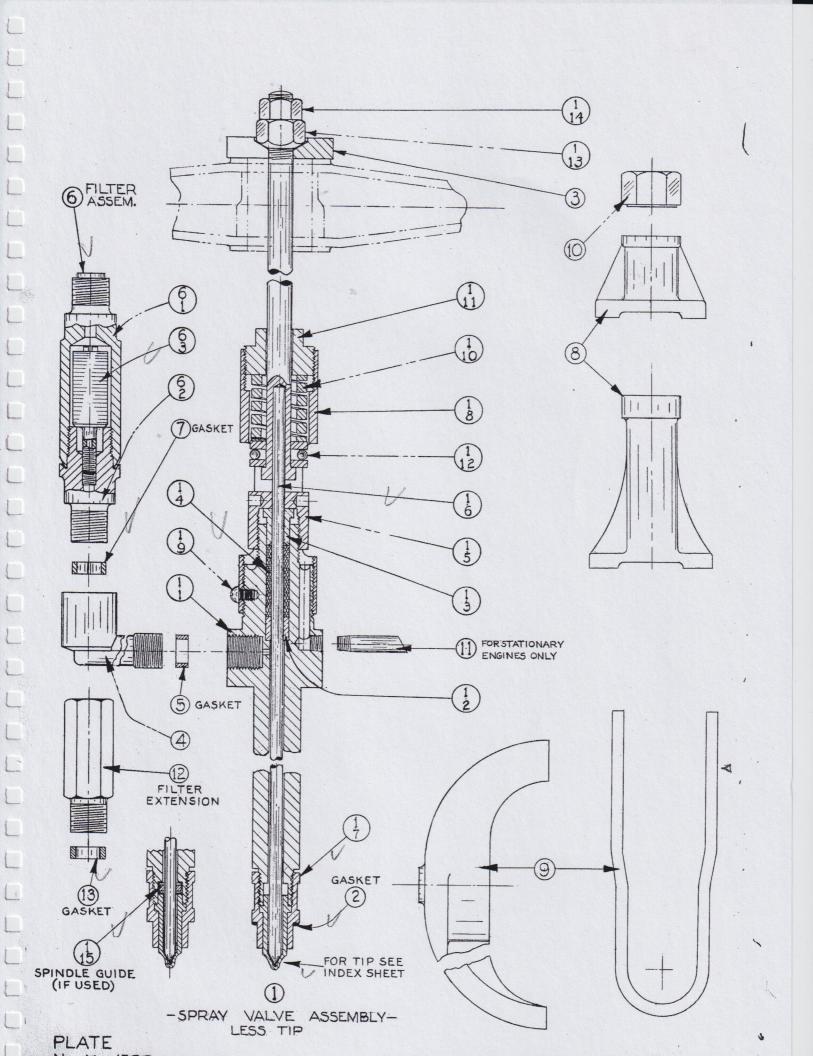
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· ' ' . \	1	1. 15 45	1.14	L-6919				
	ALWA	YE GIVE PART NU	MBER-	PATE PATE				
INE DRWG, NO.	REF.	PART NO.	NO.	I ANDM				
1 G-7988	31	529-C	REQD.	GUIDE - In. & Exh. Valve Lifter				
2			4	CAPSCREW 5/8-11-NC x 1 3/4 Lg (St.)				
40 0000	80	Cara mara	14	LOCKWASHER 5/8 SAE Reg (St.)				
4 C-8465	32	-/x1511	2	LIFTER ASSEM In. & Exh. Valve				
6 202536	33	599 E6	1	GUIDE - Air Start. Valve Lifter				
7			1_	CAPSCREW 5/8-11-NC x 1 3/4 Lg (St.)				
2 202535	34	594-E6	1	LOCKWASHER -+ 5/8 SAE Reg (St.) LIFTER - Air Start. Valve				
10	35	3A1738	1	SPRING - Air Start. Valve Lifter				
11 C-7987	361	594A-E	1	COLLAR - Valve Lifter Spring Retainer				
13	37	- W-140	1	GUIDE - Fuel Spray Valve Lifter				
14			2	CAPSCREW 15/8-11-NC x 1 3/4 Lg (St.)				
15			8	LOCKWASHER 5/8 SAE Reg (St.)				
17 R-3770	3.8	X 553	12	CAPSCREW (Clamp) 1/2-13-NC x 2 Lg (St.) LIFTER ASSEM Fuel Spray Valve				
18	39	0-3291	1	SPRING - Fuel Spray Valve Lifter				
19		1						
70 C-1932	40	X490 10-1983		SPRING ASSEM Spray Valve Push-Rod Buffer				
22	- 4			SPRING - Spray Valve Push Rod /				
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P. HAND SEE	NAME	VALVE T	LETR	3.8 GUIDE GROUP -				
P. NOT. SEE		5.4	1	ORIGINALLY 6 CYL / 7 x10 to 13x16 - 3. 4.				
**		PARTS		GINE MULTIPLY NO. HER D. GIVEN ABOVE BY NO. REQ.D. FOR GROUP BIVEN ON INDEX SHEET				





TYPED DLC ISSUED DATE 4-20-49 Retyped from 9-14-43 (No Changes) ALWAYS GIVE PART NUMBER-PART NAME-ENGINE NUMBER FOR STD. HARDWARE WITHOUT PART NUMBER GIVE DESCRIPTION AND SIZE K-1926 ASSEM. PART NO. PART NAME NO. C-3418 1 BEARING - Valve Rocker Shaft 2 3 NUT -- 3/4-10-NC-Hex. - (St.)DRAKE LOCKHUT -- 3/4-10-NC-Hex. - (St.) 4 3 4 5 C-1951 SHAFT - Valve Rocker 5 6 X520 ROCKER ASSEM. - Inlet Valve 7 X518 ROCKER ASSEM: - Exhaust Valve 6 7 ROCKER ASSEM. - Air Start Valve 8 X522 8 F-2919 STAND - Fuel Spray Valve Rocker 9 NUT -- 5/8-11-NC-Hex. -- (St.) LOCKWASHER -- 5/8 SAE Reg. --10 CAPSCREW -- $1/2-13-NC \times 1 \frac{1}{2} \text{ Lg.} - (St)$ 11 LOCKWASHER -- 1/2 SAE Reg. -- (St.)
ROCKER ASSEM. - Fuel Spray Valve 12 10 X494 13 S-2448 11 873-II PIN - Spray Valve Rocker to Stand 14 COTTER PIN -- 3/32 x 1 1/4 Lg. - (St.) 15 12 OIL CUP -- Bowen No. 5 - Hinged Lid-1/8 P.T. (St.) 16 17 18 19 C-3257 21 X535 20 PUSH-ROD ASSEM. - Inlet & Exhaust Valve 21 C-3256 22 X534 PUSH-ROD ASSEM. - Air Starting Valve C-3255 23 X536 PUSH-ROD ASSEM. - Fuel Spr ay Valve FORK - Push Rod to Rocker Connecting 0-281 24 526-R 23 NUT -- 3/4-16-NF-Hex/ - - (St.) 4 24 PIN - Push-Rod Fork to Valve Rocker 25 3-748 25 527-E1 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 P. HAND SEE & PUSH-ROD GROUP ORIGINALLY 6 CYL. 13 x 16 MARINE OTP. ROT. SEE FOR TOTAL REQUIREMENTS PER ENGINE MULTIPLY NO. HER'D GIVEN ABOVE BY NO. REQ'D FOR GROUP GIVEN ON INDEX SHEET ATLAS IMPERIAL DIESEL ENGINE CO.

OAKLAND, CALIF.



TRA PIES TO		TYPED DATE STAGE CHKO. 198UED DATE
Retyped from	n 9-10-43 (no of	reages)
	11113	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
	ALWAYS GWE PART NU	MBER-PART NAME-ENGINE NUMBER. ITHOUT PART NUMBER GIVE DESCRIPTION AND SIZE No. W-1596
DRWG. NO.	REF. PART NO.	NO. PART NAME ASSEM. PART NAME PROPERTY VALVE ASSEM Fuel Sprey
2 S=923	2 860-E 4 C-3231	1 GASKET - Spray Valve to Cyl, Head 1 CONNECTION - Spray Valve Fuel Filter
4 S=998	5 861A-E 12 C-3235	1 GASKET - Filter Connection to Spray Valve 1 EXTENSION - Spray Valve Filter Connection
6 S-628 7 F-1981 8 S-928	13 861A-E 6/ X71 7 861A-E	1 GASKET - Extension to Connection 1 FILTER ASSEM Spray Valve Fuel
9 6-287 10	855-FXC4 9 0-3230	1 GASKET - Filter to Extension 1 BRIDGE - Spray Valve Retainer 1 CLAMP - Spray Valve Bridge
1 0-278 2 0-179	10 855A=FXC4 3 877-E	1 NUT - Spray Valve Bridge Clamp Reteiner 1 COLLAR - Horseshoe (Spray Valve to Rocker)
13 14 15:		
16:	4 (1) (1) (1) (1) (1) (1) (1) (1) (1) (1)	
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MORP, ROT. 986	NAME FUEL SPRAY	ORIGINALLY 13 X 16 MAR.
DM 240 REV. MASIZM THANS.	PARTS	PER ENGINE MULTIPLY NO. REO'D GIVEN AROVE BY NO. REO'D FOR GROUP GIVEN ON INDEX SHEET - ATLAS IMPERIAL DIESEL ENGINE CO. NATIOON, ILL.

SIOUX VALVE SERVICE EQUIPMENT

Approved by

THE NATIONAL SUPPLY CO.
FOR SUPERIOR AND ATLAS ENGINES



Manufactured by

ALBERTSON & CO., INC.

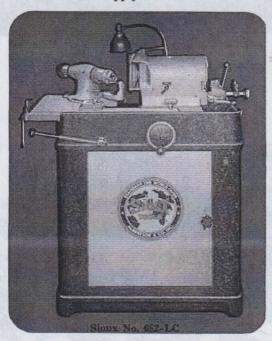
SIOUX CITY 2, IOWA, U.S.A.



STANDARD THE

Sioux Valve Face Wet Grinding Machine

National Supply No. BM-6476



Wet grinding built in. Reduces wheel dressing to a minimum. Eliminates heat and distortion, pro-

ducing finest finish and factory precision.
For valves with f_b" to 1¼" stem and up to 6" diameter, 15° to 90° angle.
Quick Acting Lever Operated Chuck, f_b" to ¾"

capacity.

Quick Acting Lever Operated Chuck fa" of 11/4" capacity.
Automatic Chuck Stop.

1 horsepower motor. Micrometer graduated feed.

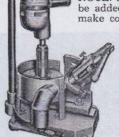
 8" grinding wheel for grinding valve face
 7" cup wheel for grinding valve end.
 Removable coolant tank for easy cleaning, 4 gallon capacity. Pump mounted in tank, selfpriming.

• Machine is 32" long and 19" wide. No. 641-B-Flexible Plastic Cover for No. 682.

Sioux Valve Seat Grinder

Basic Sets listed at right. Auxiliary Tool Kits on following page.

NOTE: Correct Auxiliary Tool Kit must be added to recommended basic set to make complete valve seat grinding set.





Dressing Grinding Wheel

Grinding Seat

Sioux Valve Seat Grinding Sets

For National Supply Co. Engines

Large valve seat grinding wheels require a slower driving unit than do the smaller wheels.

Listed here are three Basic Sets, to which special kits of pilots and grinding wheels must be added as recommended for the various engines. Note: See listings of engines on back page for proper set recommended.

HEAVY DUTY BASIC SET

Recommended for Valve Seats 3" and over

No. BM-6309-115 volt AC-DC No. BM-6309A-220 volt AC-DC

Sioux No. 1780 Includes:

–No. 1770—H. D. Driver, 4000 R.P.M. –No. 1772—Dressing Tool with 1772–B Pilot, Guard

and Driver Support, complete.

No. 1703-BB-5—Grinding Wheel Holders,

No. 1682-3—Holder Clamp.

No. X-826—Dial Indicator with 3½" finger.

-No. X-812-Pin.

-No. 1442—334" Special Lifting Spring. -No. 1442—532" Special Lifting Spring. -No. 1703-8—Spanner Wrench.

1-No. 1779-Metal Box.

HEAVY DUTY BASIC SET

Recommended for valve seats 2" to 3"

No. BM-6451—115 volt AC-DC, No. BM-6451A—220 volt AC-DC. No. BM-6451B—32 volt DC.

Sioux No. 1777 Includes:

No. 1705—Driver, 8000 R.P.M.

No. 1772—Dressing Tool with guard, with 1718-B

Pilot.

No. 1703-BB—Grinding Wheel Holders.

No. 1682-3—Holder Clamp.

No. X-826—Indicator with 3½" finger.

No. X-812—Pin.

-No. 1442—3½" Special Lifting Spring. -No. 1442—5½" Special Lifting Spring. -No. 1779—Metal Box.

BASIC SET

Recommended for valve seats under 2"

No. BM-6452-115 volt AC-DC

No. BM-6452A—220 volt AC-DC. No. BM-6452B—32 volt DC.

Sioux No. 1752 Includes:

No. 1710—High Speed Driver, 12000 R.P.M.
No. 1702-BB—Ball Bearing Wheel Holder.
No. 1713—Sioux Dressing Tool.

-No. X-811—Pin. -No. X-825—Indicator.

1-No. 1757-Metal Box.

Shipping weight 54 lbs.

Albertson & Company, Inc.

SIOUX CITY 2, IOWA, U.S.A.



SIOUX VALVE SERVICE TOOLS

For National Supply Co. Superior and Atlas Engines

No.	Price	No.	Price
BM-6308	\$ 35.10	BM-6463	\$ 43.50
BM-6309	258.95	BM-6464	59.00
BM-6309A	258.95	BM-6464A	59.00
BM-6451	218.30	BM-6464B	59.00
BM-6451A	218.30	BM-6465	30.00
BM-6451B	218.30	BM-6466	35.00
BM-6452	131.60	BM-6467	21.00
BM-6452A	131.60	BM-6468	27.80
BM-6452B	131.60	BM-6469	28.30
BM-6453	22.30	BM-6470	27.40
BM-6454	25.30	BM-6471	14.00
BM-6455	85.60	BM-6472	26.90
BM-6455A	85.60	BM-6473	29.00
BM-6455B	85.60	BM-6475	21.00
BM-6456	36.30	BM-6476	1185.00
BM-6457	24.40	BM-6477	27.80
BM-6458	37.30	BM-6478	39.00
BM-6459	59.00	BM-6479	32.40
BM-6459A	59.00		
BM-6459B	59.00		
BM-6460	20.90		
BM-6461	28.30		
BM-6462	39.30		

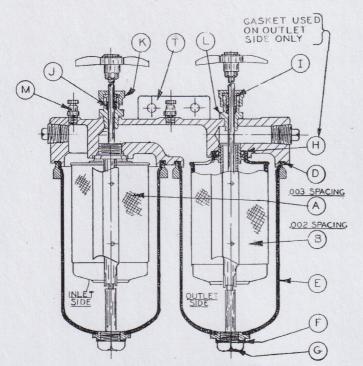
PRICES ARE NET TO USER AND SUBJECT TO CHANGE WITHOUT NOTICE

ALBERTSON & COMPANY, Inc.

Sioux City 2, Iowa, U. S. A.

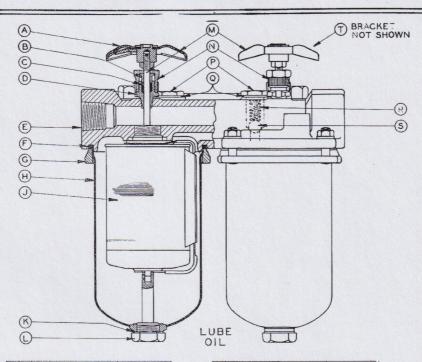
D.W.V.-FORM 198-PL-11-6-53-2M





REF.	REG	NAME	PART NO.
Α		ELEMENT& KNIFE ASSEM	F-6418 P1
В	1	ELEMENT & KNIFE ASSEM.	F-6418 P2
D	2	GASKET	F-6418 P3
Ε	2	SUMP TANK	F-6418 P4
F	2	GASKET	F 6418 P5
G	2	PLUG	F-6418 P6
14	1	GASKET	F-6418 P7
I	2	GLAND	F-6418 P8
J	2	PACKING	F-6418 P9
K	2	CAP	F-6418 P10
L	2	PLUG	F-6418 P11
М		VENT	F-6418 P13
Т	T	BRACKET	F 6418 P12

COMPLETE FILTER - PART No. F-6418P - FUEL OIL -



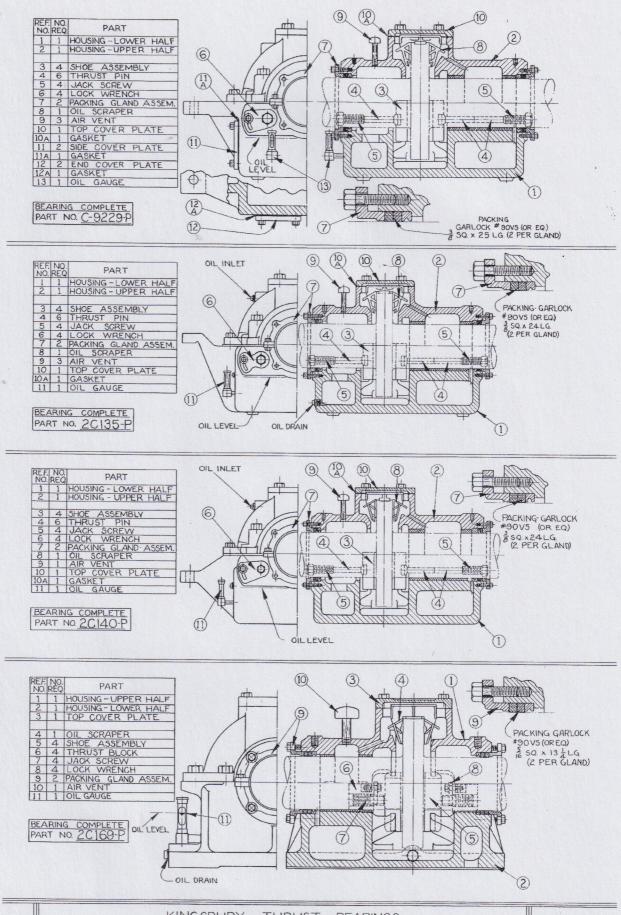
REF.	NO.	NAME	PART NO.
A	2	HANDLE ONLY	3A1872P1
В	2	GLAND	F 6418P8
C	2	PACKING	F-6418P9
D	2	PLUG	F 6418P11
E	1	HEAD	3A1872P5
F	2	GASKET	F-6418P3
G	2	RING	3AI872P7
H	2	SUMP TANK	F 6418P4
J	2	ELEMENT & NIFE ASSEM	F-6418Pi

REF.	NO.	NAME	A.I.D.E. CO.
K	2	GASKET	F-6418P5
L	2	PLUG	F-6418P6
M,	2	HANDLE & STEM	3A1872P12
N	2	PACKING NUT	F-6418P10
P	2	SCREW	3A1872P14
Q	2	GASKET	3A1872P15
R	2	SPRING	3A1872P16
S	2	BALL	3A1872917
T	1	MOUNT. BRACKET	F-6418P12

-COMPLETE FILTER PART No 3A1872-

-NOTE-

BOTH FILTERS SHOWN ABOVE MAY NOT NECESSARILY BE USED. CHECK INDEX SHEET OR GROUP LISTS FOR PART No. OF FILTERS.



KINGSBURY THRUST BEARINGS NOTE .

STANDARD THE WORLD OVER



SIOUX AUXILIARY TOOL KITS

The following auxiliary tool kits include grinding wheels and pilots as needed for each engine. Below is listed the number of each kit and what they contain. Also Kits for Air Starter valves. Note: See listings of engines on back page for proper kits recommended.

Kit No.	Pilots Grinding Wheels	
	TSA-751—12 "x5½" K- 57-WS K- 59-WS	3
BM-6308	TSA-753-12 "x51/2" K-117-WS K-119-WS	5
	TSA-755—12 "x5½" 3¼"-45° 3½"-45°	
\$4.000 mm market	TS-631—11½"x5½" K- 59-WS—3½"-45°	
BM-6453	TS-633—11½"x5½" K-119-WS— "	
	TS-635—11½"x5½"	
	TSA-688—13 "x7 " K- 59-WS—3½"-45°	
BM-6454	TSA-690—13 "x7 "K-119-WS—"	
DM-0494	TSA-692—13 "x7 "	
D34 0450	TSA-751—12 "x5½" K- 59-WS K- 61-WS	
BM-6456	TSA-753—12 "x5½" K-119-WS K-121-WS	5
	TSA-755—12 "x5½" 3½"-45° 3¾"-45°	
	TSB-688—12½"x6 "K- 55—3"-45°	
BM-6457	TSB-690—12½"x6 "K-115— "	
	TSB-692—12½"x6 "	
***************************************	TS-1001—10%"x5 "K- 59-WS—3½"-45°	
BM-6458	TS-1003—105%"x5 "K-119-WS—"	
	TS-1005—105%"x5 "	
	TSA-626—11 "x5 " K- 46-#3—2½"-45°	
BM-6460		
D141-0400		
	1011-000-11 AU	
	TSE-751—12½"x6 "K- 59-WS—3½"-45°	
BM-6461	TSE-753—12½"x6 "K-119-WS—"	
	TSE-755—12½"x6 "	
	TSC-876-12½"x6½" K- 59-WS K- 63-5-V	VS
BM-6462	TSC-878-1212"x61/2" K-119-WS K-123-5-V	VS
	TSC-880—12½"x6½" 3½"-45° 4"-45°	
***************************************	TS-1126—12 "x5 " K- 65-5-WS—41/4"-45	>
BM-6463	TS-1128—12 "x5 "K-125-5-WS "	
2212 0100	TS-1130—12 "x5 "	
	10 1100 10 10	
DR 0405	TSD-875—15 "x7 "K- 63-5-WS—4"-45°	
BM-6465	12D-011-19 XI V-159-9-MD-	
***************************************	TSD-879—15 "x7 "	
	TSD-875—15 "x7 "K- 68-5-WS—4¾"-45	2
BM-6466	TSD-877—15 "x7 "K-128-5-WS—"	
	TSD-879—15 "x7 "	
***************************************	TS-626—11½"x5½" K- 51—2¾"-45°	*******
BM-6467	TS-628—11½"x5½" K-111— "	
	TS-630—11½"x5½"	
***************************************	TSF-751—14½"×7¼" K- 57-WS—3¼"-45°	
BM-6468	TSF-75314½"x7¼" K-117-WS "	
D1V1-0400		
	TSF-755—14½"x7¼"	
	TSD-751—13½"x6¾" K- 59-WS—3½"-45°	
BM-6469	TSD-753—13½"x6¾" K-119-WS—"	
	TSD-755—13½"x6¾"	
	TSD-626—14 "x7 " K- 51 K- 55	
BM-6470	TSD-628-14 "x7 "K-111 K-115	
	TSD-630—14 "x7 "23/4"-45° 3"-45°	
	TS-313— 8%"x5 "SK- 3—156"-45°	
DIM GATT		
BM-6471	TS-314— 8%"x5 "SK-73— " TS-315— 8%"x5 "	
	15-315 X3/6"Y5 "	

Kit No.	Pilots			Grinding	Wheels
***************************************	TS-501-3-11	"x5	"	K- 46-#3,	K-111
BM-6472	TS-502-3-11	"x5	.11	K-106-#3,	K- 51
	TS-503-3-11	"x5	"	2½"-45°	23/4"-45
	TSA-751-12	"x51	2"	K- 61-WS-	-3¾"-45°
BM-6473	TSA-753—12	"x51	2"	K-121-WS-	_ "
	TSA-755—12	"x51	2"		
	TSD-626-14	"x7	"	K- 51-23/4"	-45°
BM-6475	TSD-628-14	"x7	"	K-111-	»
	TSD-630—14	"x7	,		
***************************************	TSA-751—12	"x51	2"	K- 57-WS-	-3¼"-45°
BM-6477	TSA-753-12	"x51	2"	K-117-WS	
	TSA-755—12	"x51	2"	T. B. H. C. V.	
***************************************	TSE-1001-141/	2"x61	2"	K- 65-5-WS	41/4"-45
BM-6478	TSE-1003-144	2"x61	2"	K-125-5-WS	<u>"</u>
	TSE-1005-141/	2"x61	2"		
	TS-563-11	"x5	"	K-455-3"-3	0°
BM-6479	TS-564-11	"x5	11	K-525 "	
	TS-565—11	"x5	"	K- 49-25%"	-45°
	TS-566-11	"x5	11	K-109-	,

Kits for Air Starter Valves

BM-6455—115 Volt.

BM-6455-A-220 Volt.

BM-6455-B-32 Volt.

Includes:

1-No. 1710 Driver, 12,000 R.P.M.

2-No. 1702-BB-Wheel Holders.

1-No. 1772-A-Pilot.

I-No. X-825-A-Sleeve.

1-No. X-811-Pin.

1-No. SK-5-1%"-45° Grinding Wheel

1-No. SK-75-1%"-45° Grinding Wheel.

1-No. TSG-750-2-Special Pilot.

BM-6459-115 Volt.

BM-6459-A-220 Volt.

BM-6459-B-32 Volt.

Includes:

1-No. 1710-Driver, 12,000 R.P.M.

1-No. K-17-3-134"-45° Grinding Wheel.

1-No. K-87-3-13/4"-45° Grinding Wheel

1-No. TSA-937-Special Pilot.

BM-6464-115 Volt.

BM-6464-A-220 Volt.

BM-6464-B-32 Volt.

Includes:

1-No. 1710-Driver, 12,000 R.P.M.

1-No. K-21-3-17/8"-45° Grinding Wheel.

1-No. K-91-3-1%"-45° Grinding Wheel.

1-No. TSF-1000-Special Pilot.

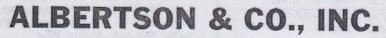


STANDARD THE WORLD OVER

Listing of Engines and Basic Sets with Auxiliary Kits needed for each Model Engine. Number.

(Note: Where there are no model numbers, bore and stroke are substituted for identification.)

Model No. Superior Engines	Basic Set Numbers Sioux National		For Regular Valves Auxiliary Kit No.	For Air Starter Valves Auxiliary Kit No.
6-G-510	1780	BM-6309	BM-6453	
PTD, 40	1780	BM-6309	BM-6454	BM-6455
PTG	1780	BM-6309	BM-6456	BM-6455
44	1780	BM-6309	BM-6456	Jan 0100
PTL, 40-LX	1780	BM-6309	BM-6457	BM-6455
LO, LOC, LP, LPC, KN, KNA, KNB, 60	1780	BM-6309	BM-6458	BM-6459
VDHA, GI,	1777	BM-6451	BM-6460	
VDMA, VDMB, VDMS,	1780	BM-6309	BM-6461	BM-6455
VDMD	1780	BM-6309	BM-6462	BM-6455
VDSS, VDST, 80, VDSB, VGST, VDSC,	1780	BM-6309	BM-6463	BM-6464
65	1780	BM-6309	BM-6478	
Model No. Atlas Engines			****	
1558, 58	1780	BM-6309	BM-6465	
2124, 75, 76 and 12½x16	1780	BM-6309	BM-6466	
327, 5¾x8 6x8 6¼x8 6½x8 282	1777	BM-6451	BM-6467	1 24 Charles - 12 Chil
763, 48 and 8½x12	1780	BM-6309	BM-6468	
1125, 55	1780	BM-6309	BM-6469	
464	1780	BM-6309	BM-6470	
Atlas Jr.	1752	BM-6452	BM-6471	
253	1777	BM-6451	BM-6472	
668, 45, 46	1780	BM-6309	BM-6473	
528, 38	1777	BM-6451	BM-6475	
8x9½, 8½x9½, 3" Int. Valve	1780	BM-6309	BM-6308	
8x9½, 8½x9½ 668 industrial	1780	BM-6309	BM-6477	A CANAL MANAGEMENT
35	1780	BM-6309	BM-6479	



SIOUX CITY 2, IOWA, U.S.A.

